Superstructure East Bay Crossing (Contract No. 04-7)

The as-built drawings, which are contained in these CDs, are scanned from drawings of the existing structure for the contractor and as a means to convey to the contractor the available information regarding the existing structure. It is to be understood that no claim is being made as to the accuracy or completeness of the said information and that the State of California or its officers or agents shall not be responsible for the manner in which the contractor interprets and uses this information or for the accuracy, currency or completeness of these scanned as-built drawings. The contractor shall be responsible to obtain, at the contractor's expense, any additional information that the contractor deems necessary for completely and accurately assessing the existing conditions of the structure. The contractor shall not be entitled to any compensation for any claim arising from inaccuracy or insufficiency of these as-built drawings or in anyway related to these drawings.

- 1. East Bay Crossing General Plan & Elevation
- 2. East Bay Crossing Stress Sheet Cantilever Arm and Suspended Span
- 3. East Bay Crossing Stress Sheet Anchor Arm
- 4. East Bay Crossing Stress Sheet 504-Ft. Spans
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- 23. East Bay Crossing 504 Ft. Span Panel Point U6
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- 33. East Bay Crossing Bents E2 & E3 Cap Details
- 34. East Bay Crossing Bents E2 & E3 Base Details

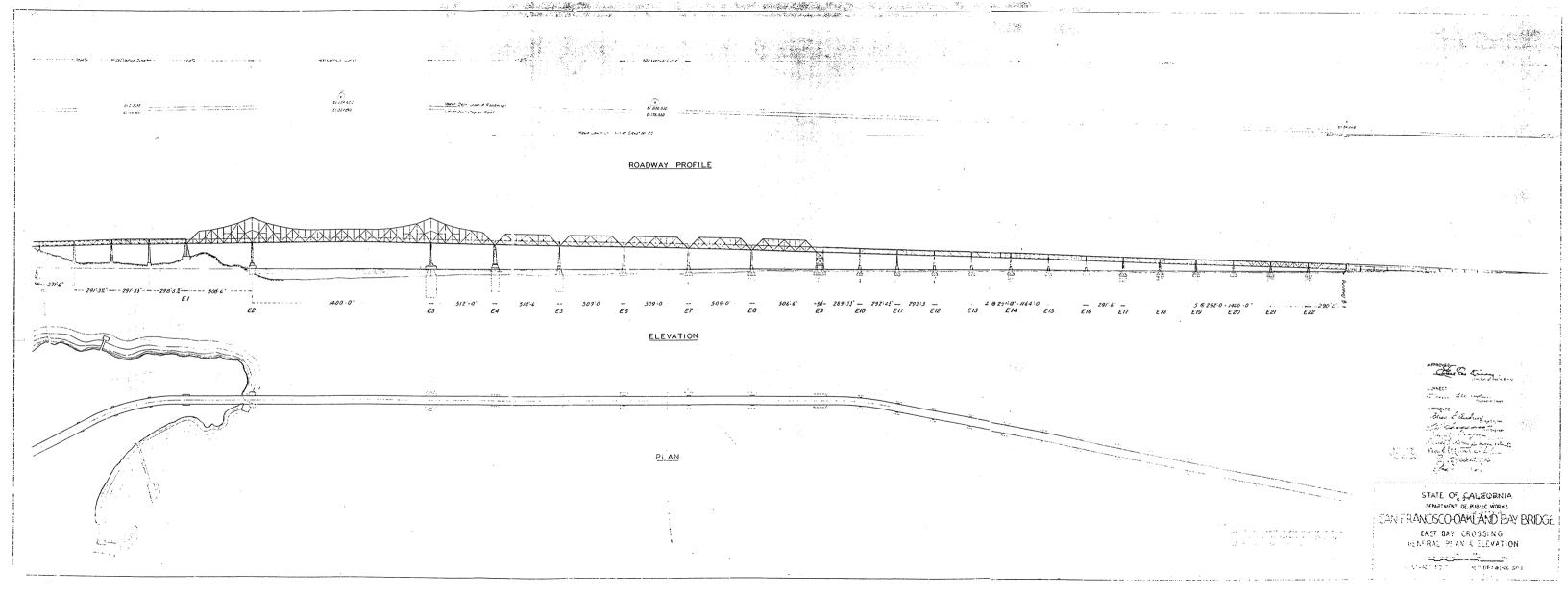
36. East Bay Crossing Bent E4 Details of Base

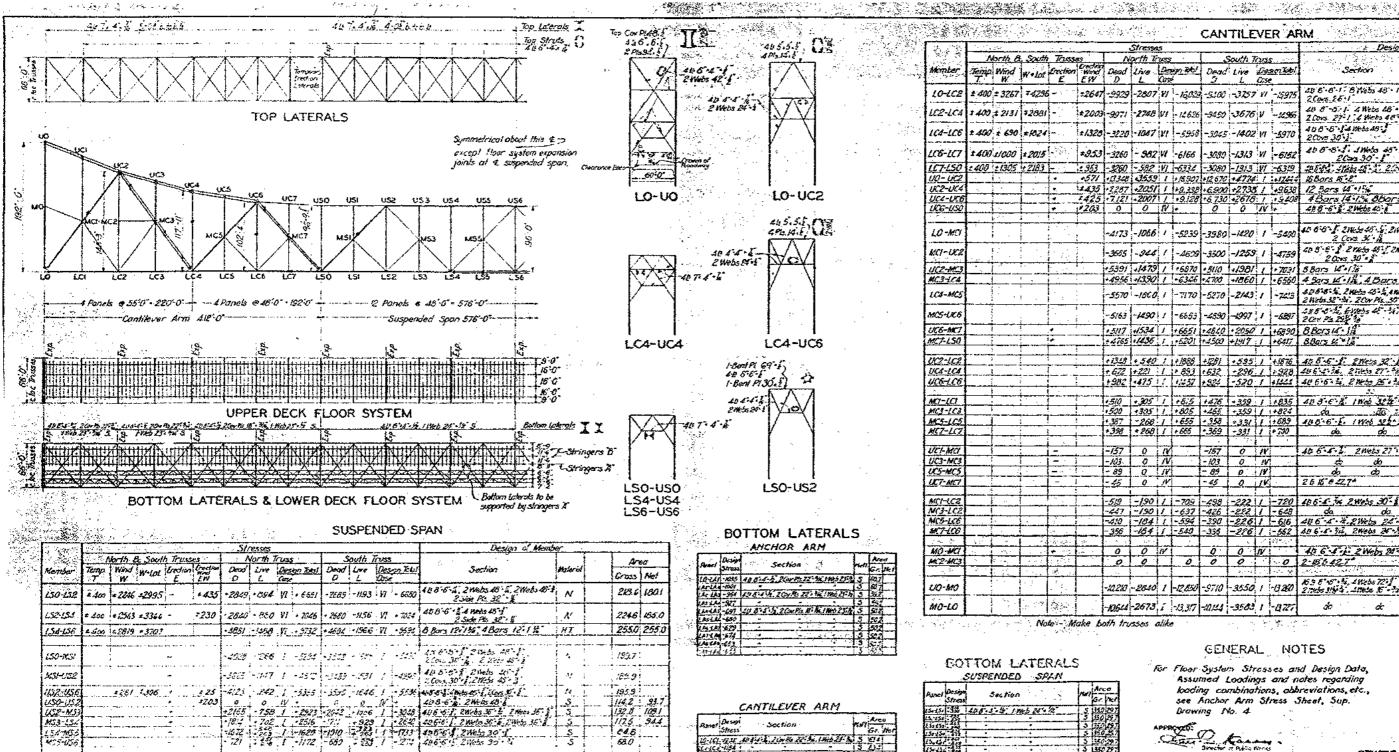
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CANTILEVER ARM

EOTTOM LATERALS SUSPENDED SPAN

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For Floor System Stresses and Design Data, Assumed Loadings and notes regarding loading combinations, abbreviations, etc., see Anchor Arm Stress Sheet, Sup. Drawing No. 4

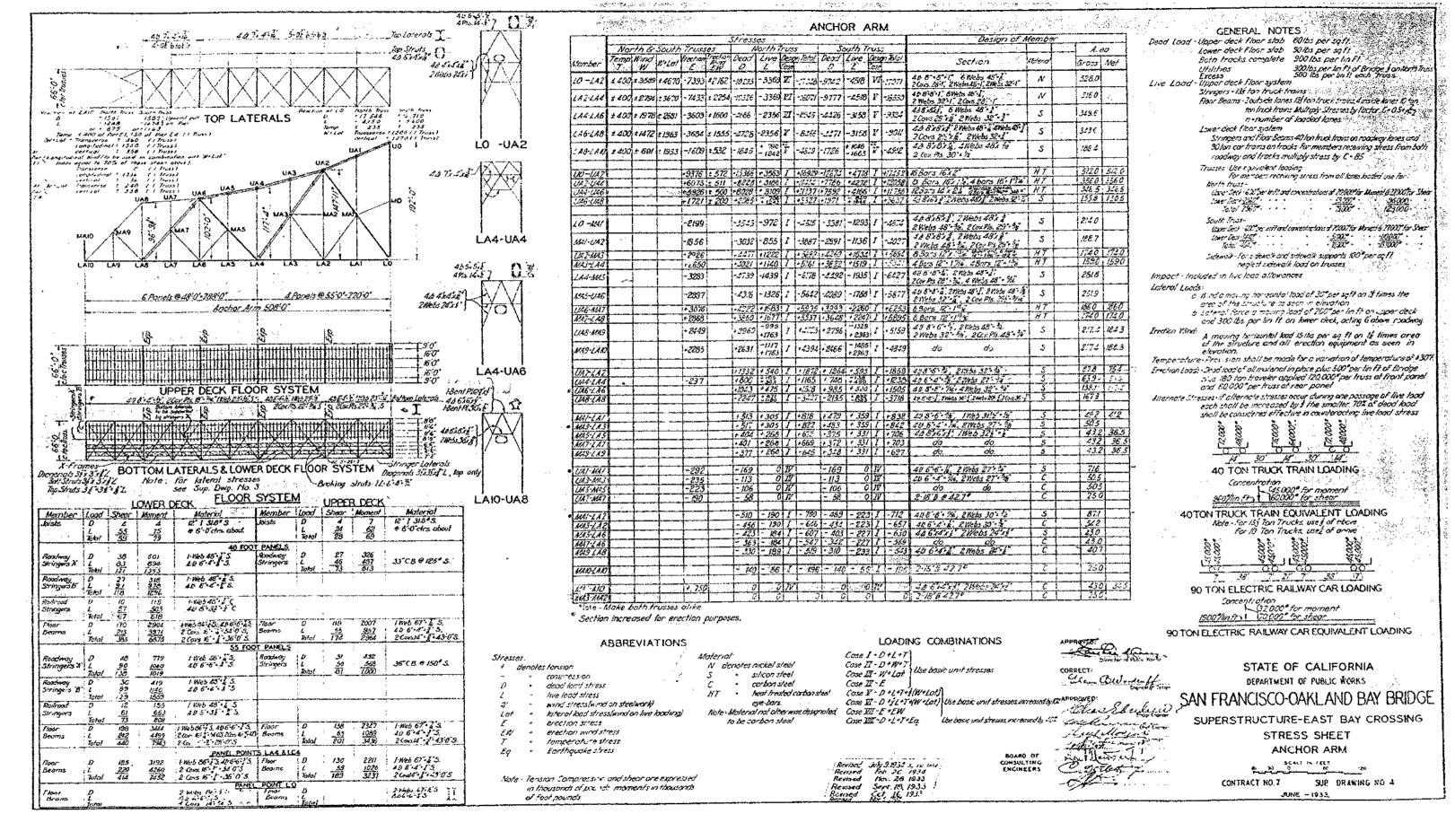
GENERAL NOTES

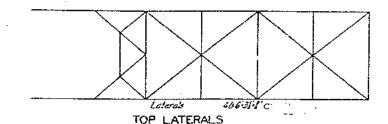
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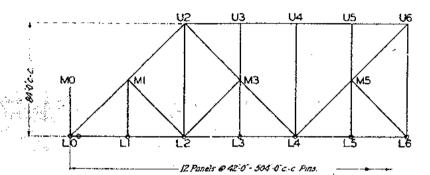
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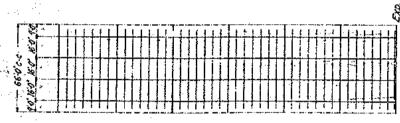
SAN FRANCISCO-OAKLAND BAY BRIDGE SUPERSTRUCTURE-EAST BAY

CANTILEVER ARM AND SUSPENDED SPAN

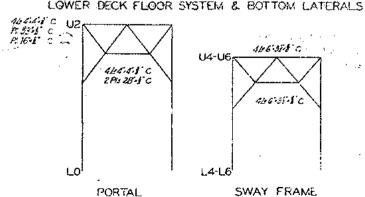








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BOTTOM LATERALS PANEL DESN AREA SECTION GROSS NET LO-L1 -675 2844, 228 40-8-4-8 20-44 22.8 L1-L2 +630 5 L2-L3 -521 23.0 185 40-8-6-5 5 L3-L4 1470 23.0 18.5 734 L4-L5 +470 23.0 230 185 5-16 438

GENERAL NOTES

for Design Data, Assumed Loading and more complete notes regarding loading combinations, obbreviations etc. see sep. Drawing No. 4

Denotes tension,

- Carbon Steel,
- Heat Treated Carbon Steel Eye-Bars.

Material not otherwise designated to be Carbon Stee

STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS

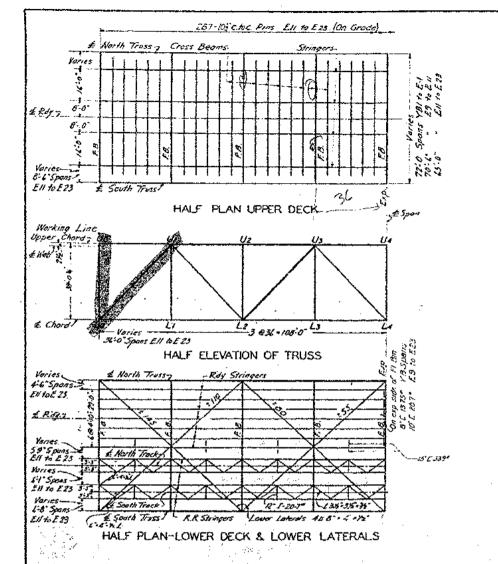
SUPERSTRUCTURE-EAST BAY CROSSING

STRESS SHEET 504-FT SPANS

CONTRACT NO.7 SUP DRAWING NO.5

Revised August II, 1933. Revised August 29, 1933 Revised Ockber 16, 1933

Revised January II 1934 Revised: December 4 1933 Revised: October 23 1933



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- € North Trass 5h 246-17597 241-09847 241-0047 241-91847 209-05847 259-05847 255-45347 256-57347 241-49347 241-49347 247-99347 259-25347 279-20587

LAYOUT SPANS
For Layout Spans YBI to E1 see Sep Brug. No. 79.
For Layout Spans E9 to E1 see Sep Brug. No. 79.
For Layout Spans E9 to E1 see Sep Brug. No. 78. No Scole.

applies for North and South Trusses Spons Ell to E 23 inc. South Trust YB2 to El and E9 to Ell. Opplies for North Trass Spens YOZ to El. E9 to Ell. moers not listed in Table II and Table II to be as listed in Table I combination · Case II See Sup Drg. Ho. 6

FLOOR SYSTEM LOWER DECK Cross Beams (210318"S. Flor Beams 10-6 c.toc Trusses.

1 Neb Pl. 47 T/2 }

AB L=6"+34" Ráy Stringer B to 30 Spon 21 CB e 13 S. M. D. 46 Sh. D. 7 <u>L. 208</u> <u>L. 42</u> Totol 254 Totol 40 M. D. 7 Sh. D. 3 <u>L. 62</u> <u>L. 25</u> Tota: 69 Total 28 41: 1-14-76. 2 CM: 14-76. 26.0 Long 2 CM: 14-76. 36.0 Long 2 CM: 14-76. 30.0 Long D. 2444. 5h. D. 137. M. D. 1733 St D. 88 50 ingers 26 to 30 5pm 21 (897) 1. 940 . 1. 47 Talia 2473 Talil 135 Rety, Stringer 30 to 31' Sport 24 CB 6743 Mr. D. 64 St. D. 10 N. D.104 55 D. 17 L 250 L 41 Floor Beam 45 0" ctoe Trustes 2.302 THE FLET WE SE 70 ES Stringers 301057 Spor-27CB 685 \$ Floor Beam To-4" e to: Trusses Rdy Stringer 31 to 40 Ston 2 CE 680. M. D. 198 Sh. D. 2/ M. D. 1472 St. D. Bb S4. D. 11 15. 2. 97 1. 364 1.42 Total 362 Total 63 L. 809 Total 2281 L 324 Tetal 421 1. 14 Total 55 R.R. Stringers 264030 Spon 24 CBerto. M. D. X Sh D. 4. Stringers 31 to 40 Span-77CB @ 1065 M. D. 272 Sh. D 22 M. D. 2344 D. 135 1 386 L 47 L 3871 Total 6220 Total 251 RR Stringer 30 to 37 Spor 30'CB & 108C Floor Beam 72-0 ctoc Trusses or Beart 65'0 choc Tresses M. D 35 SA D & 1 Web Pl. 67 17/6" 4 15 6 14 17/6" I NED DY BOX'S ∠ 334 40 626 7/2 I 44 2CH: 14. 14. 46-8 Tong 5 2CH: 14. 14. 35-0 Tong 2C Pk 14 1/4 46 6 long Total 369 M. D. 1800 St D. 89 1. 975 1 47. Total 2775 Tatal 134 M. D. 2040 Sh. D. 125 Total 5360 Tatal 308

For General Notes See Sup. Ding N.4

Bertsod - Dec. 21 1933 Revised Oct 18 1933 Revised Oct. 23 1933

> BOARD OF CONSULTING

STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS

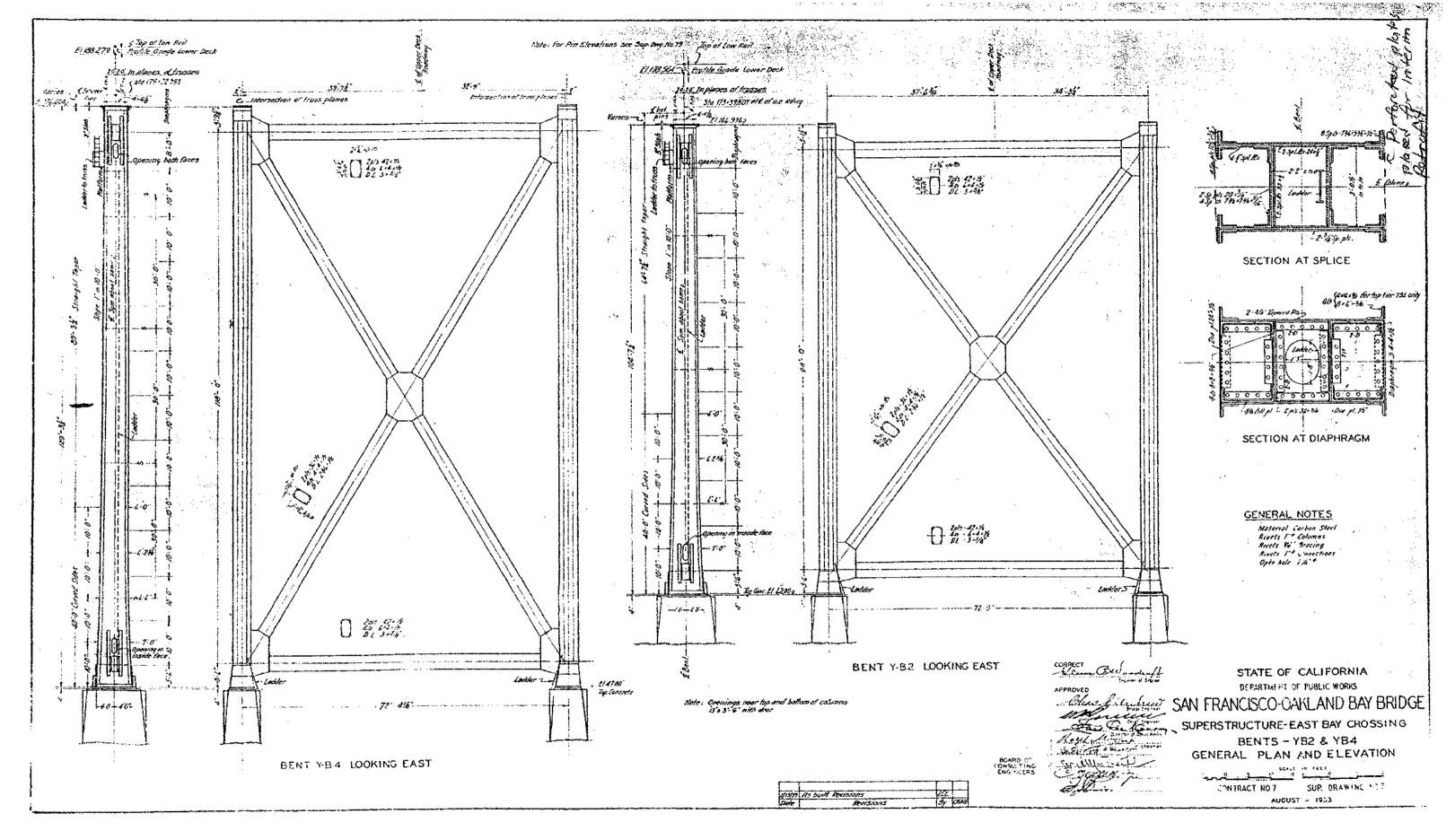
SAN FRANCISCO-OAKLAND BAY BRIDGE

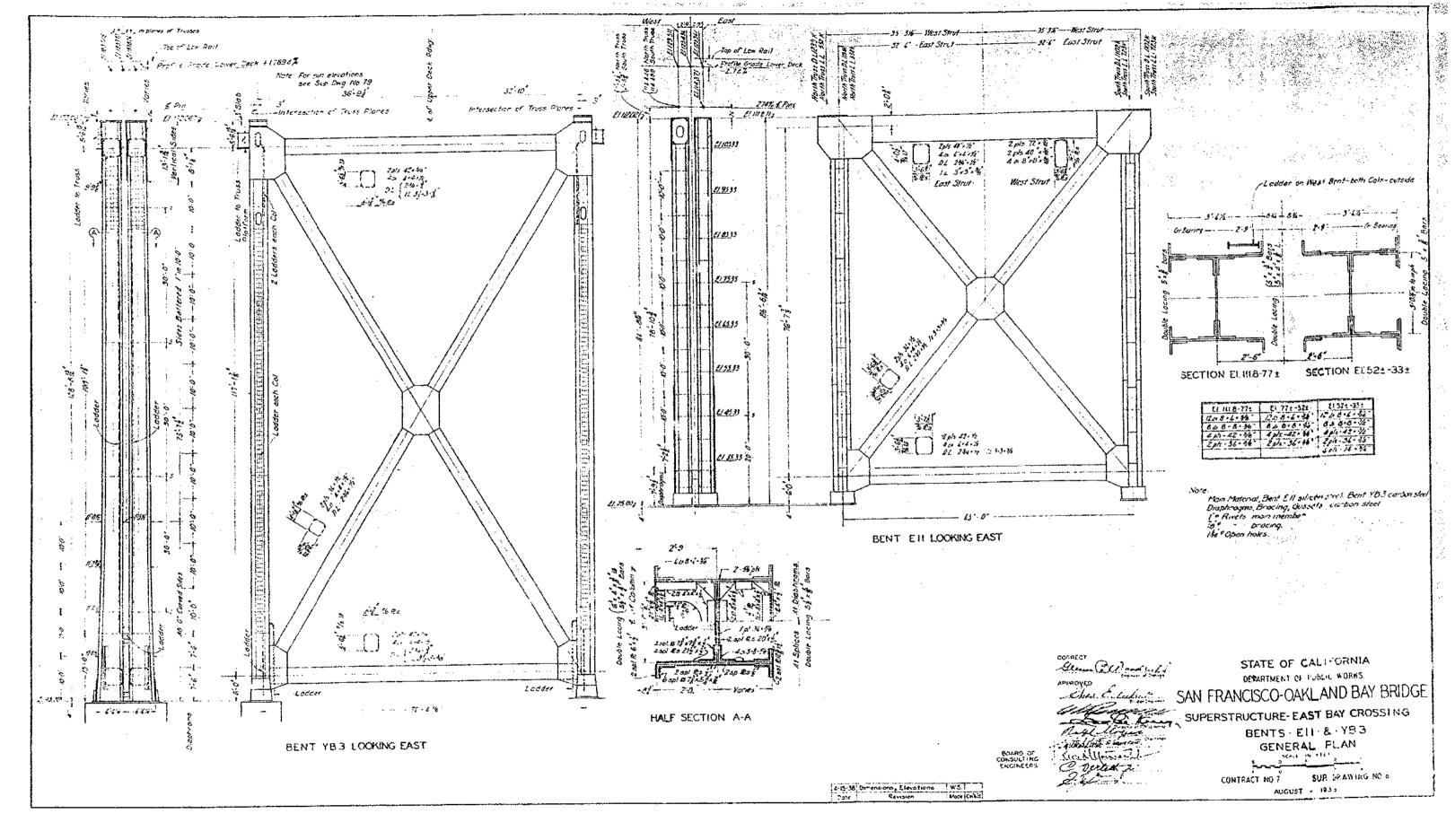
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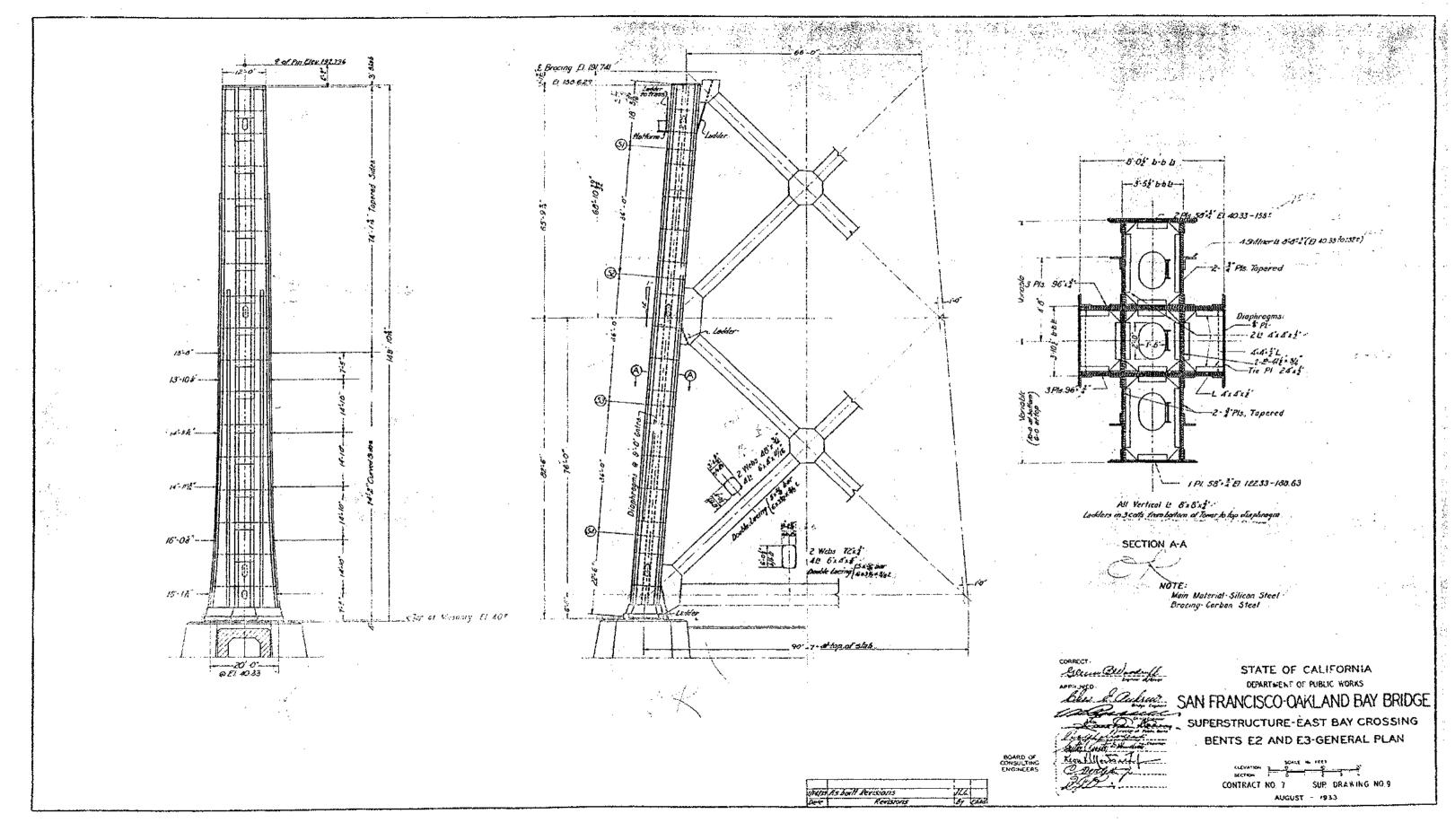
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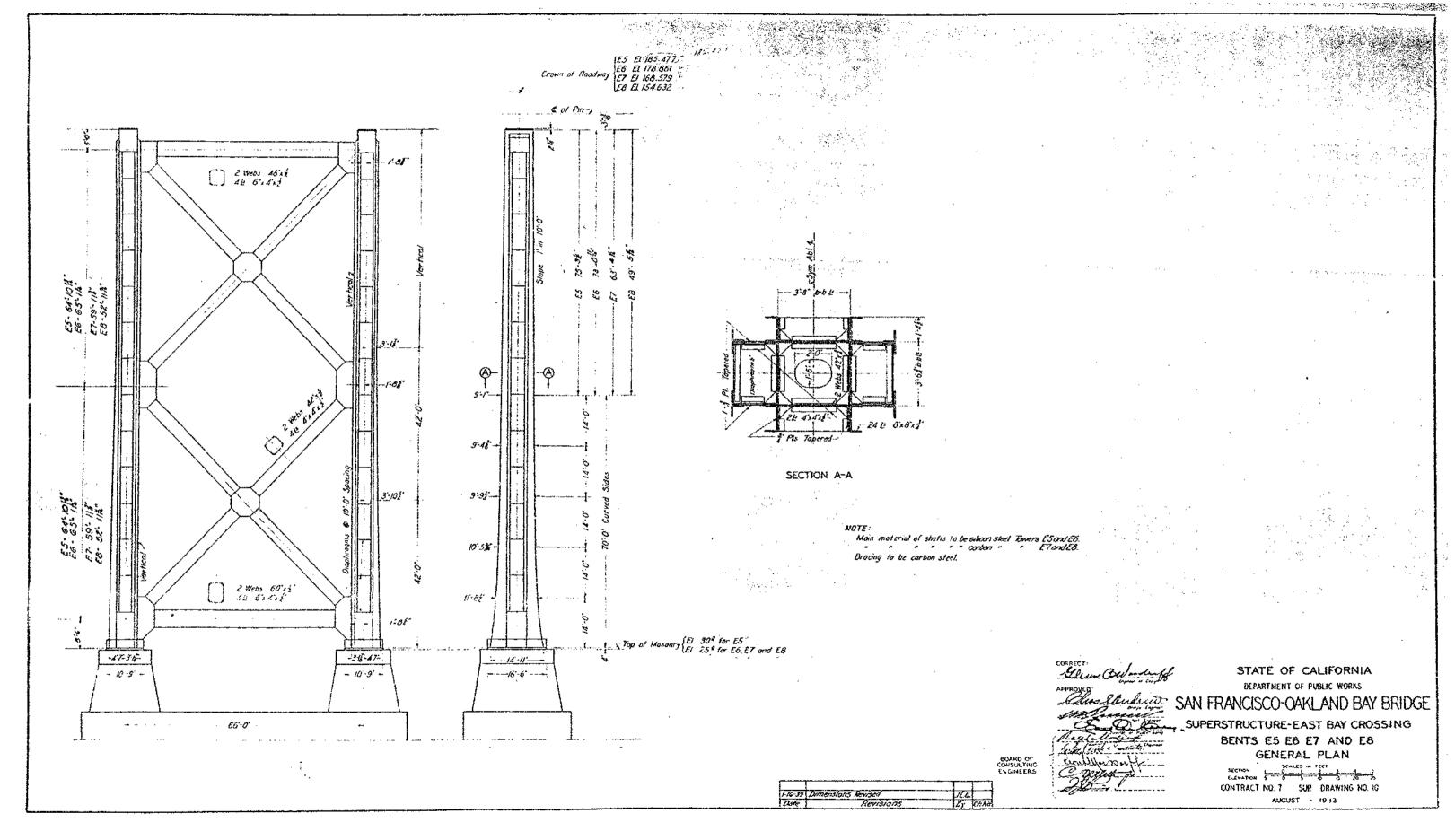
CONTRACT NO 7. SUP DRAWING NO. 6.

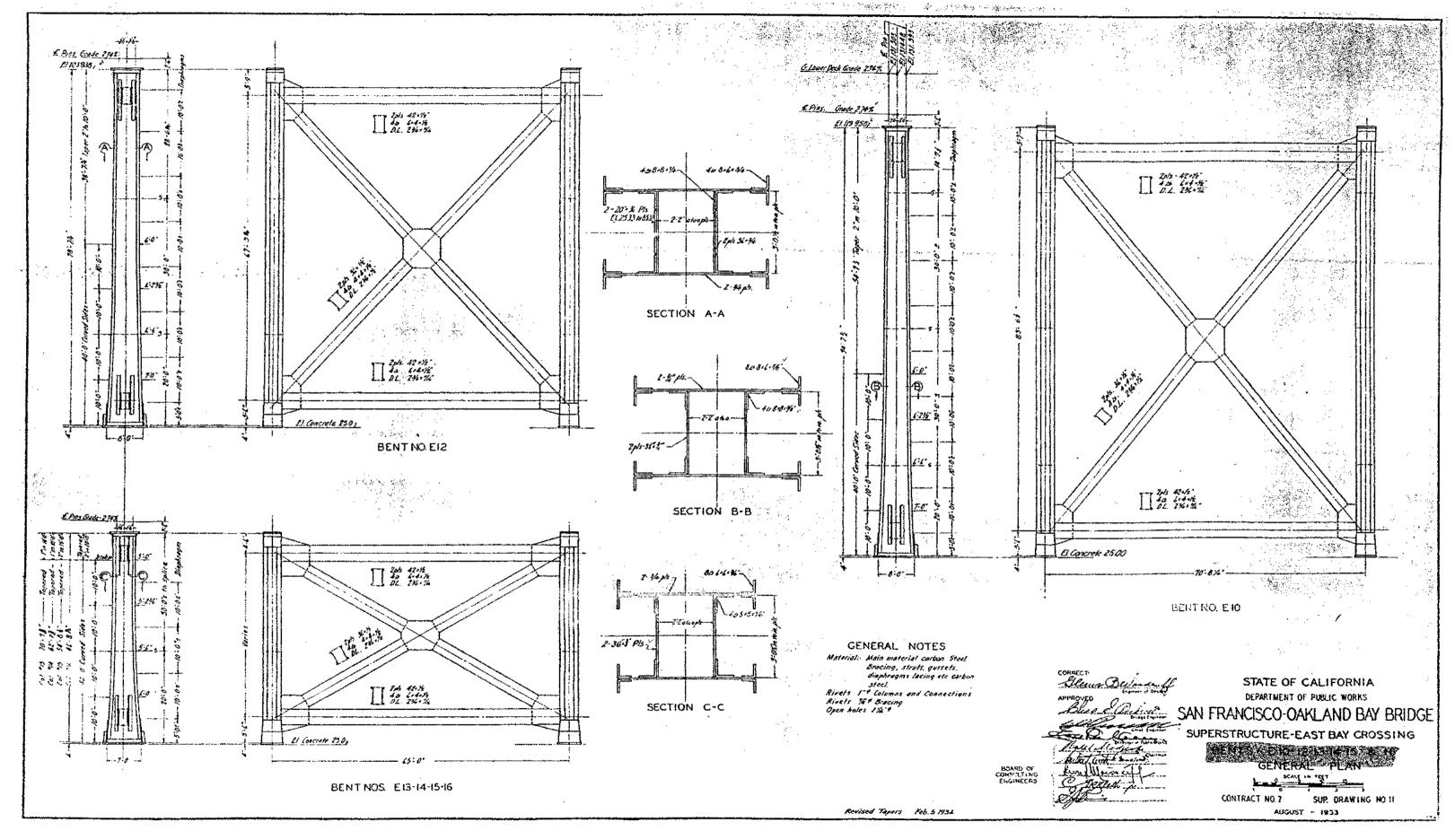
OCTOBER - 1933

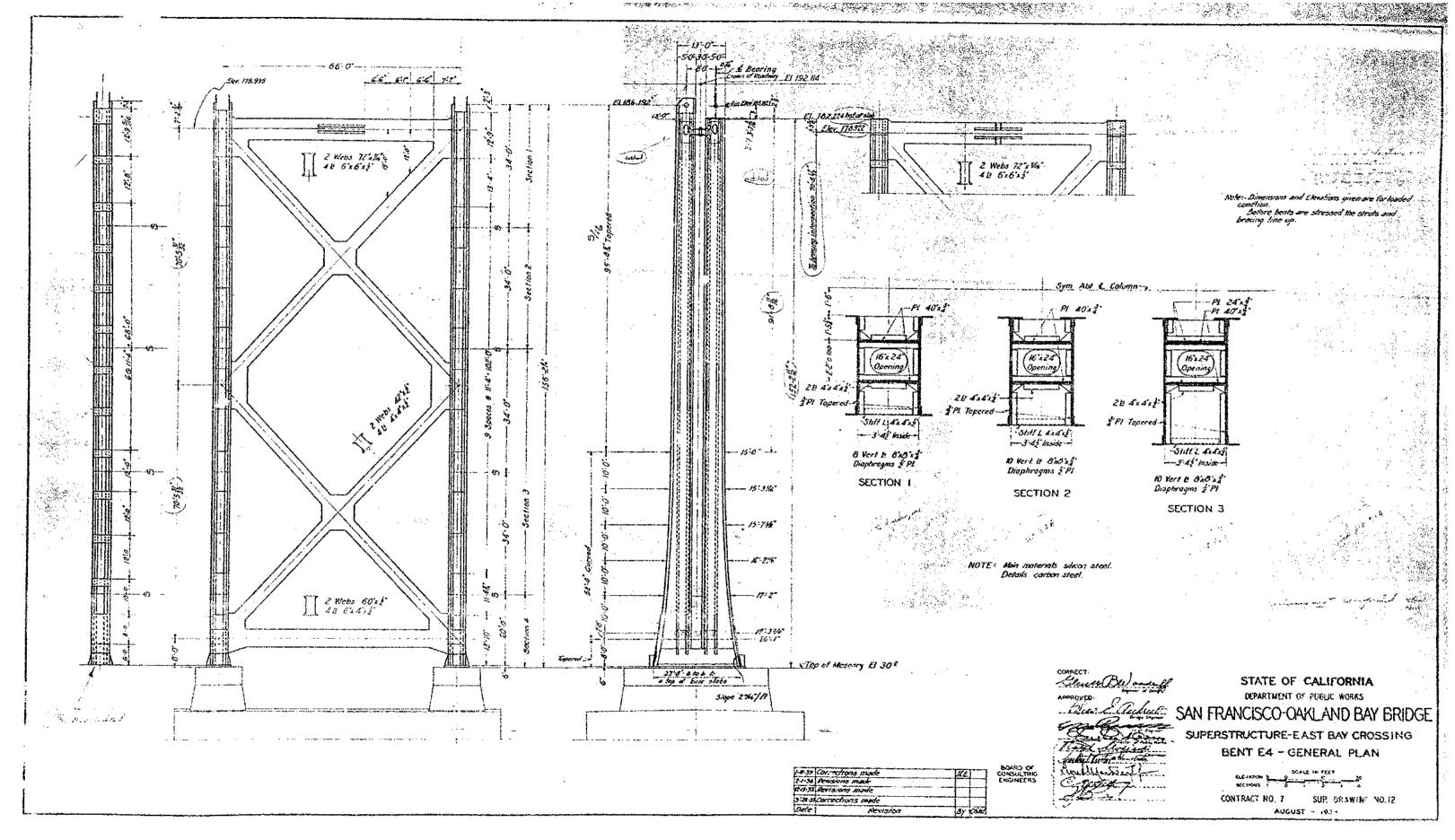


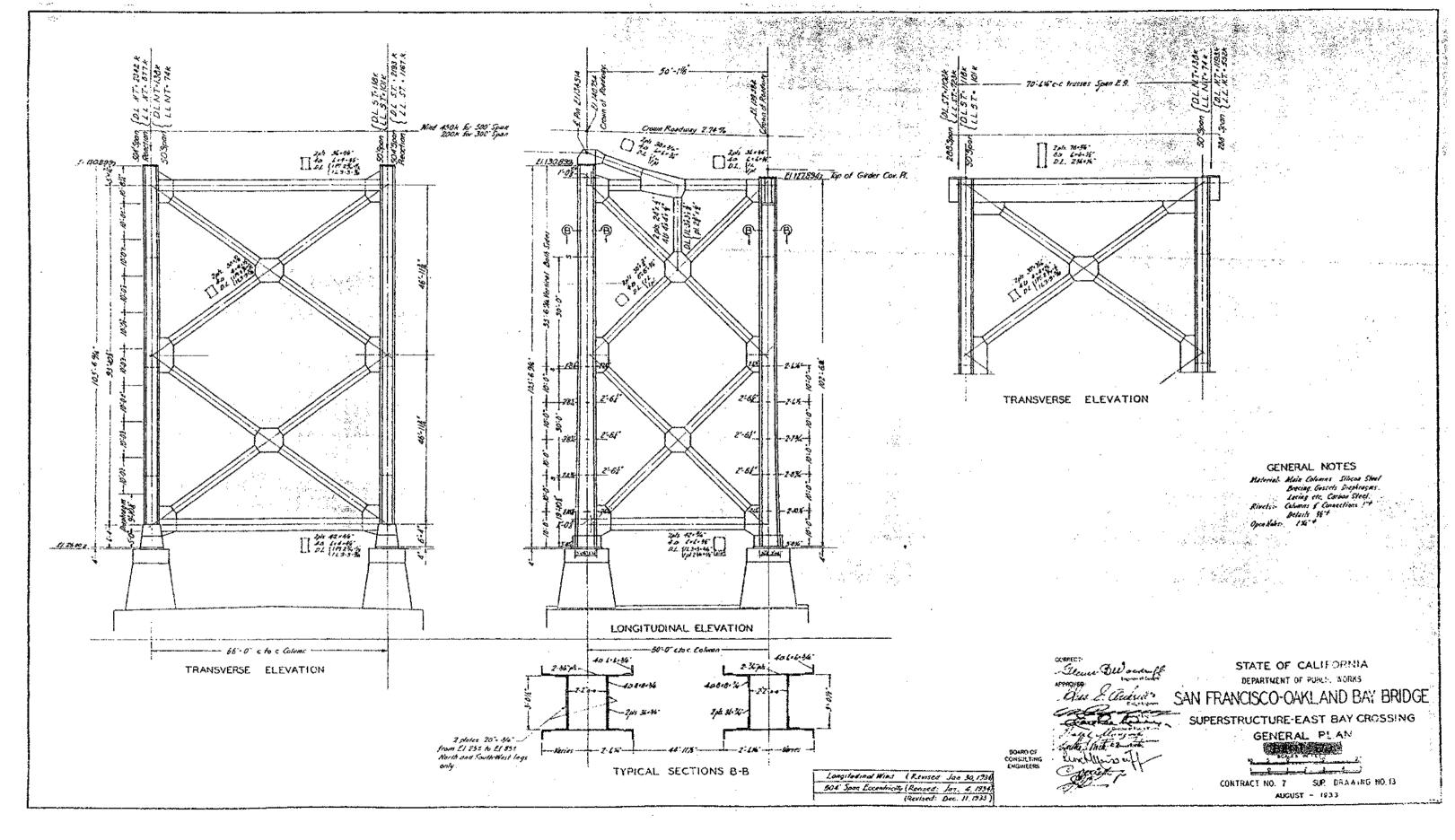


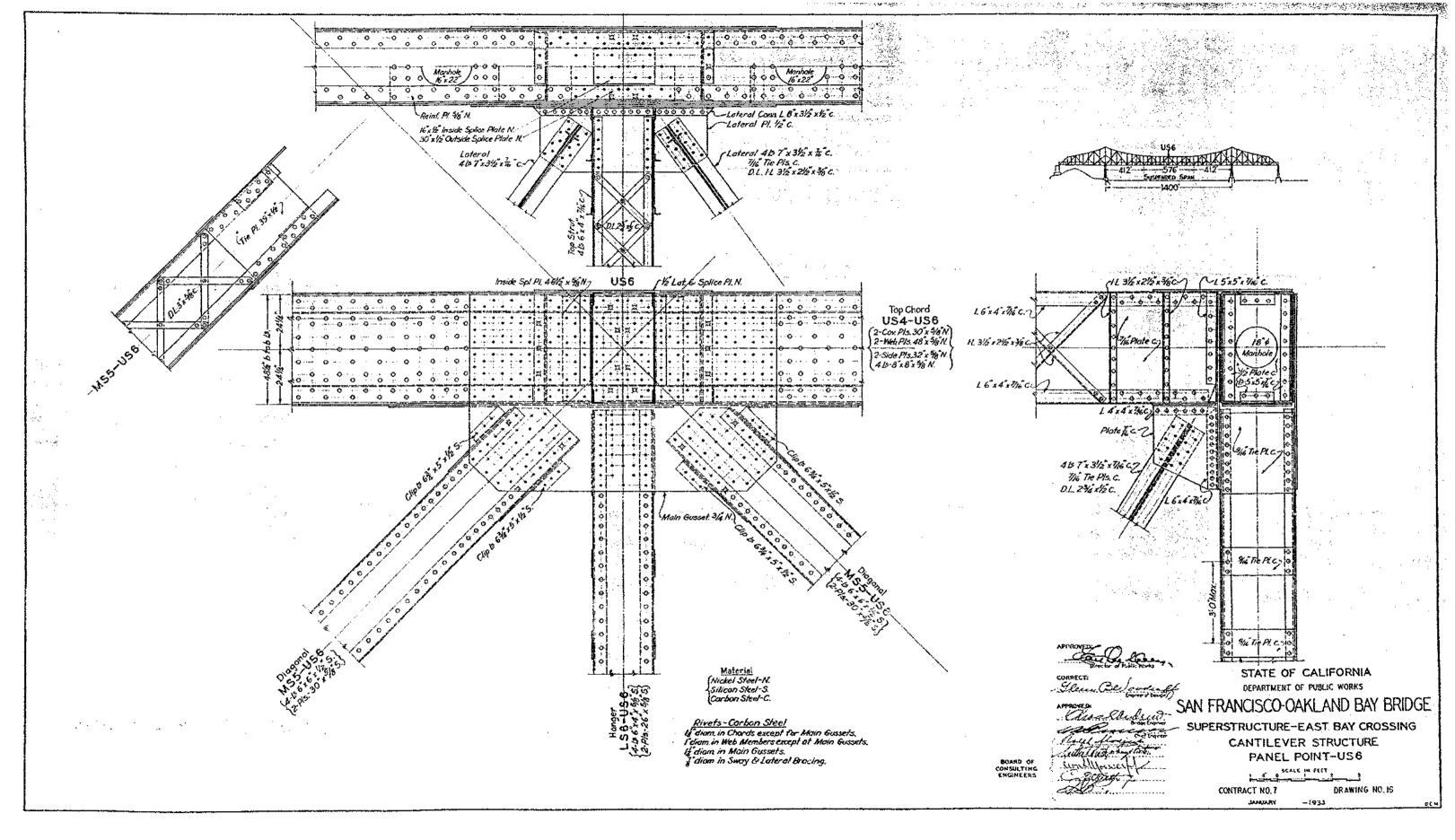


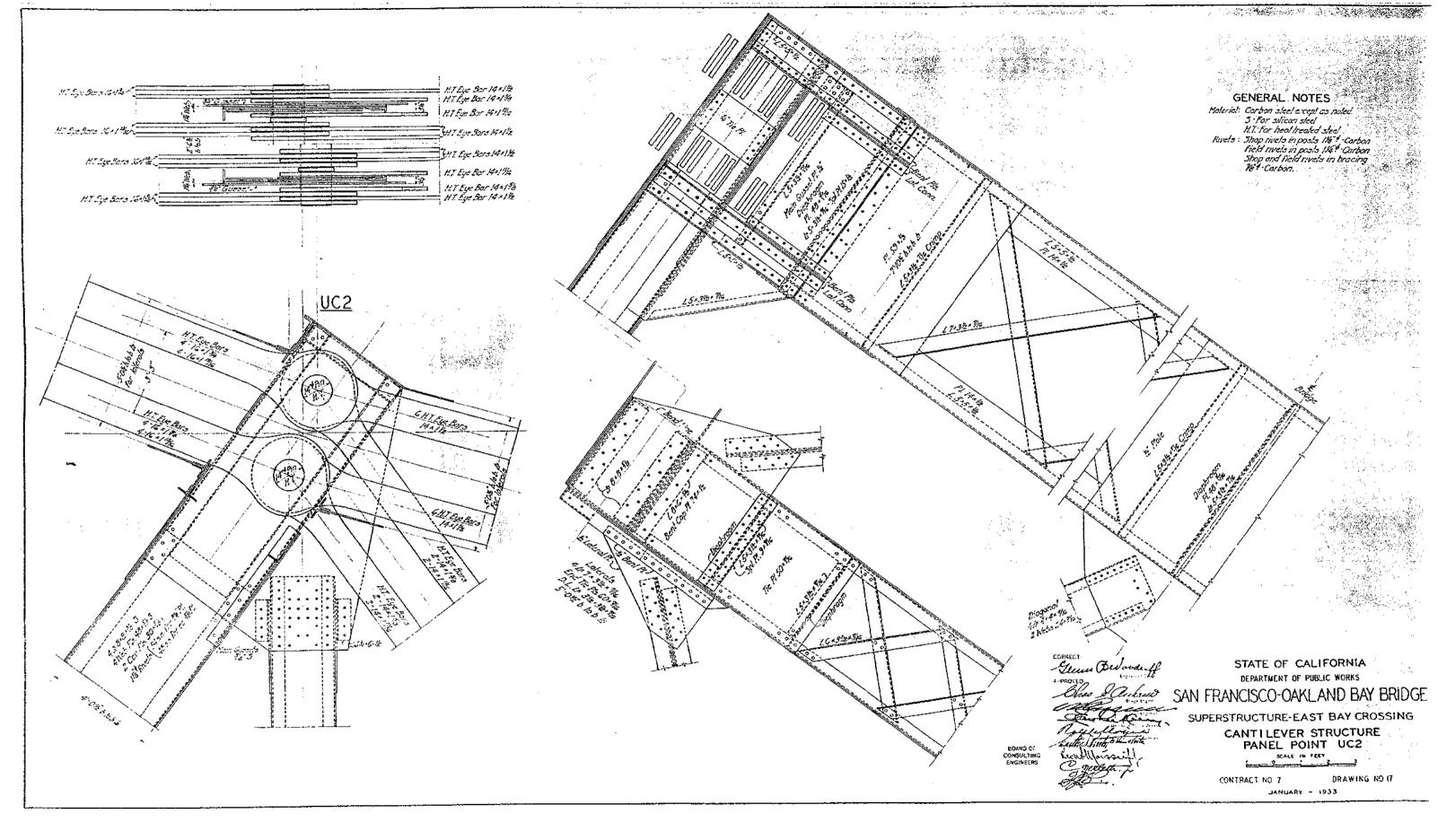


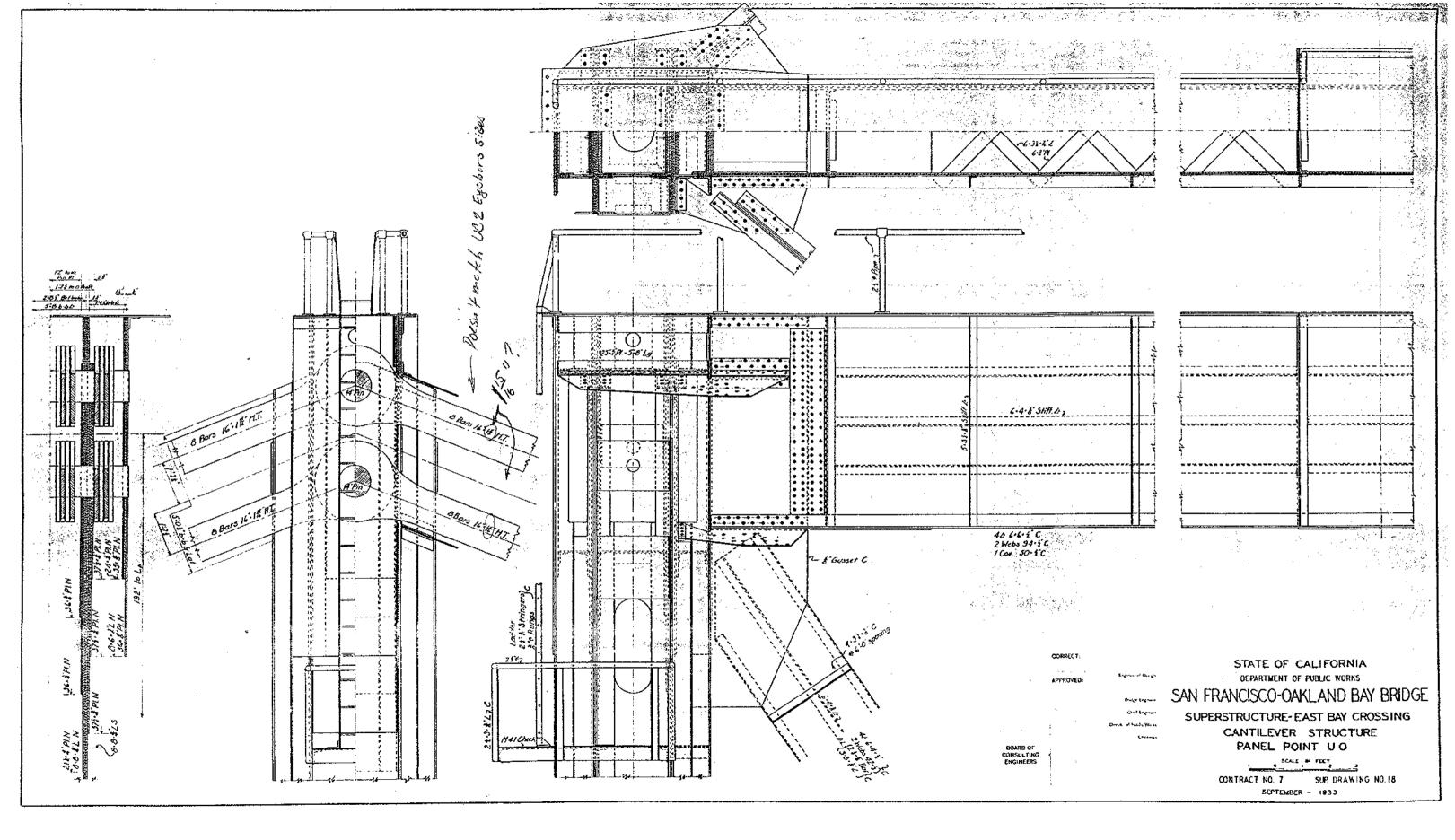


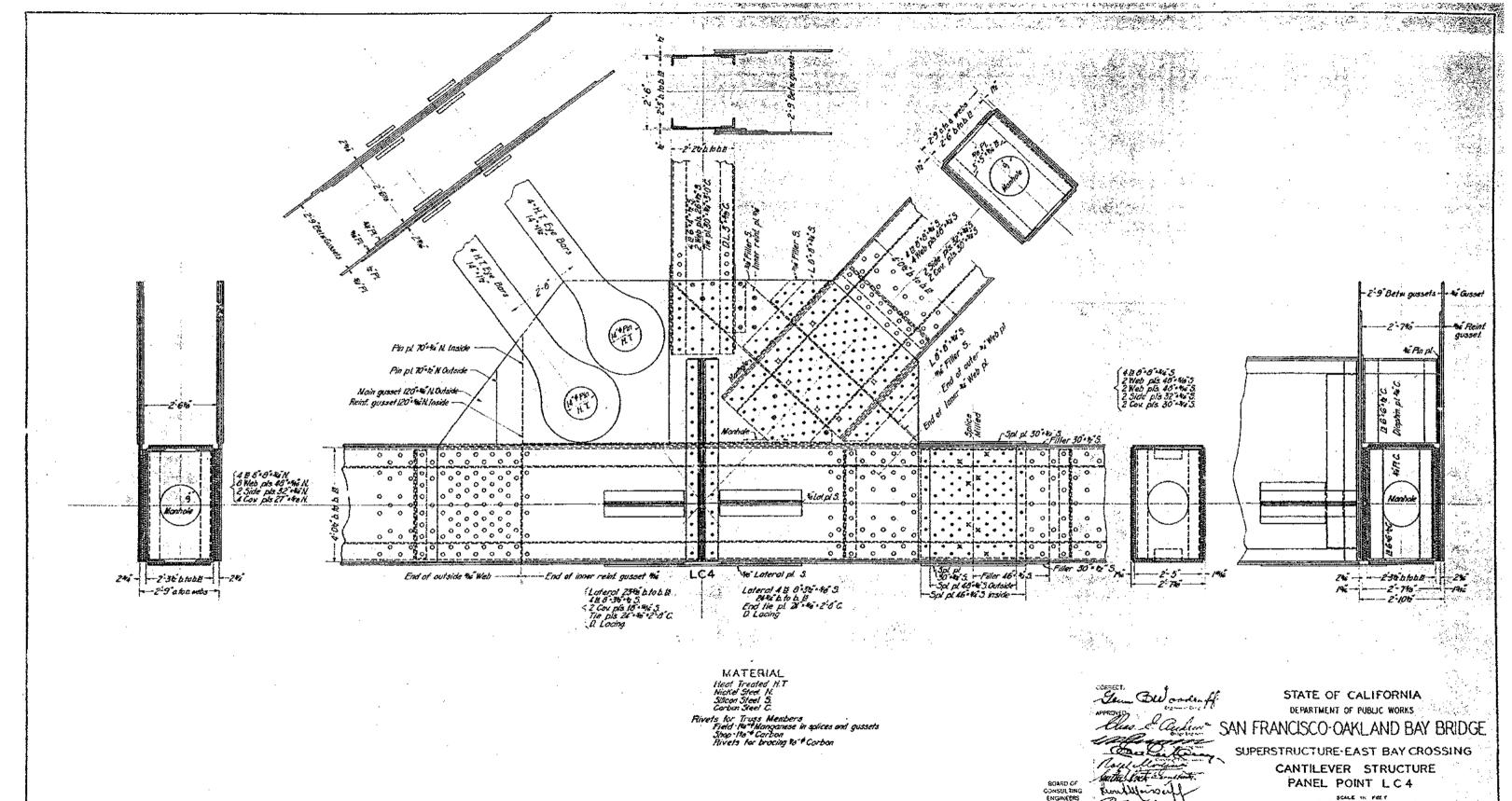








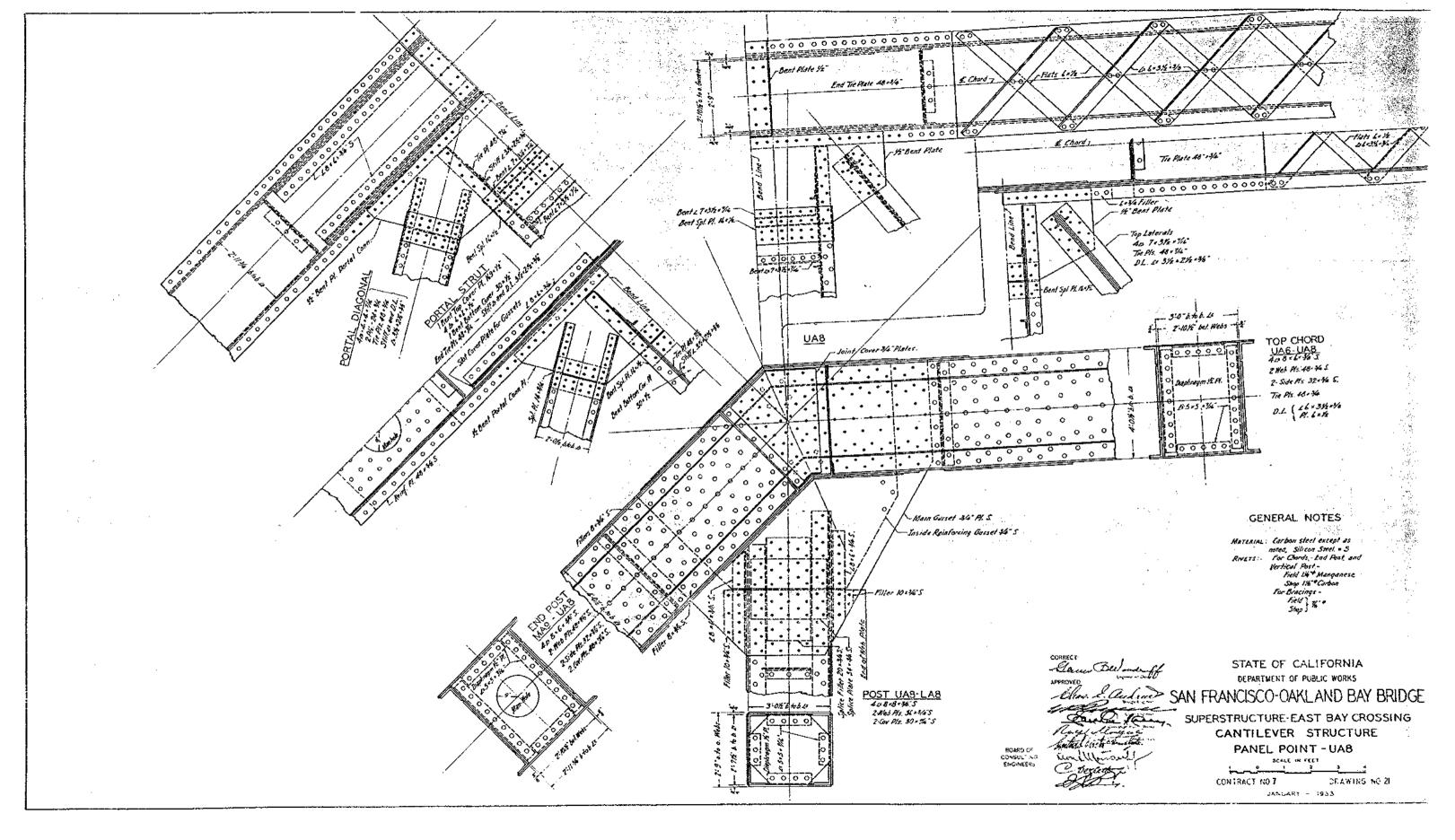


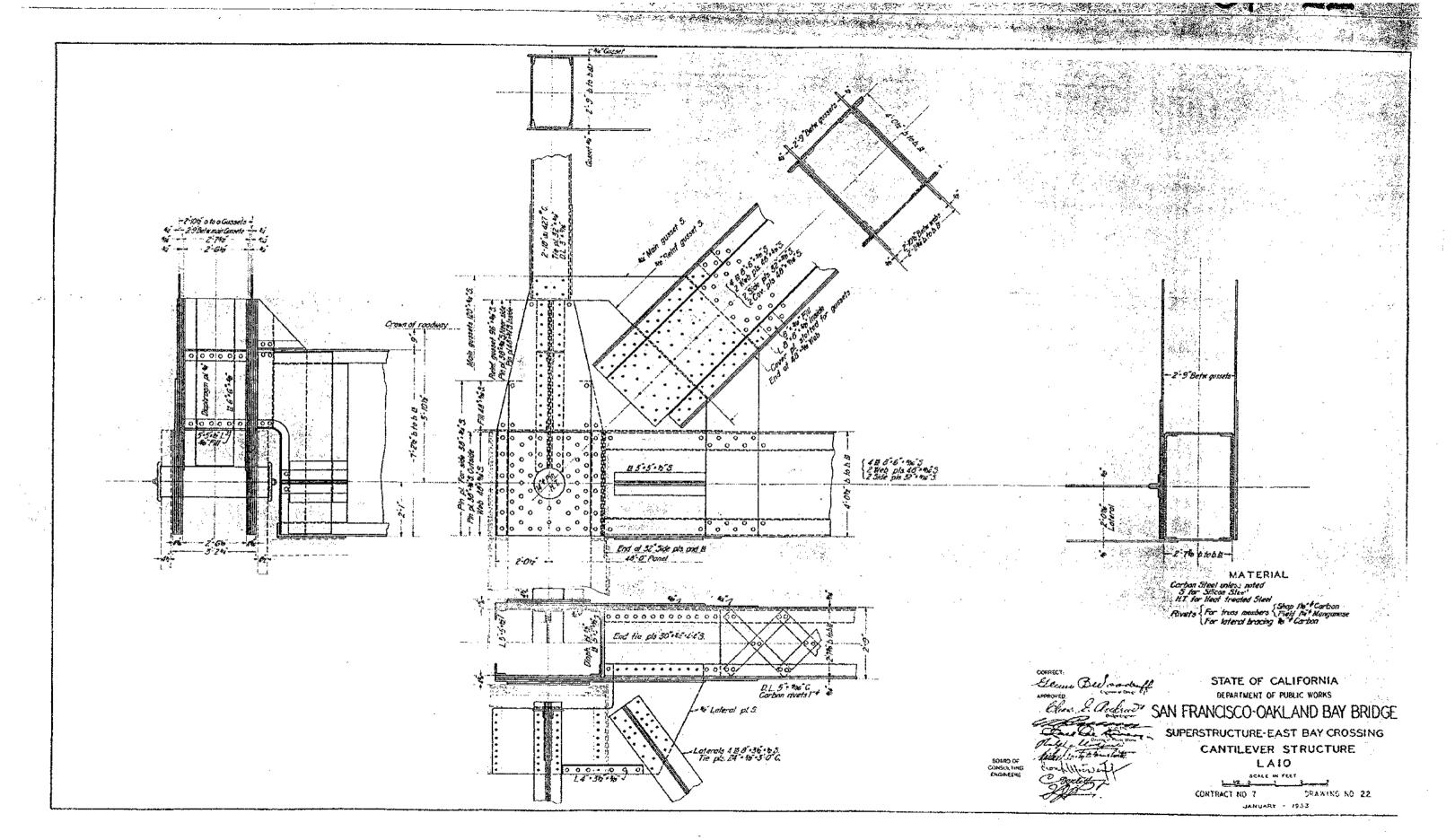


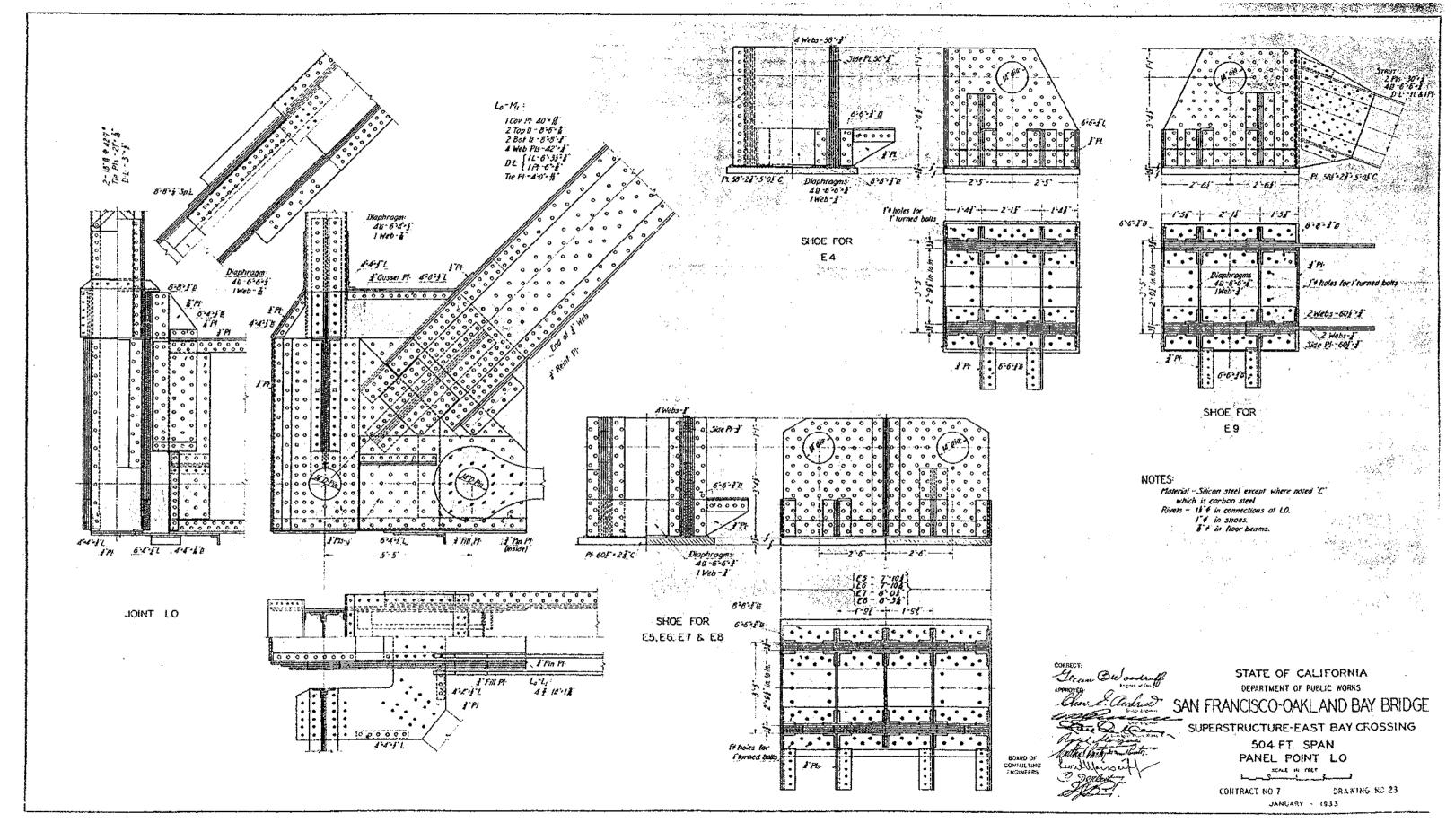
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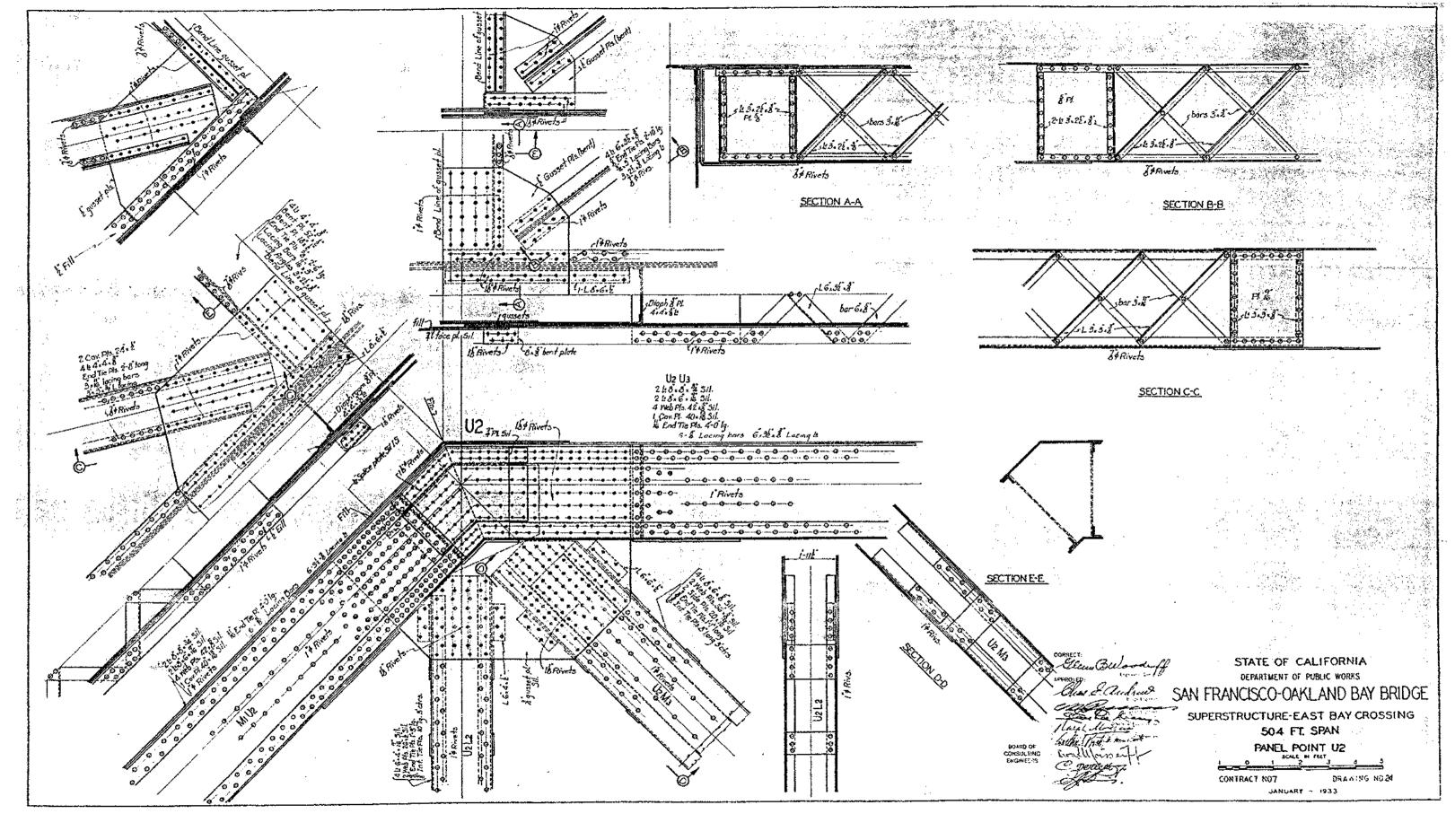
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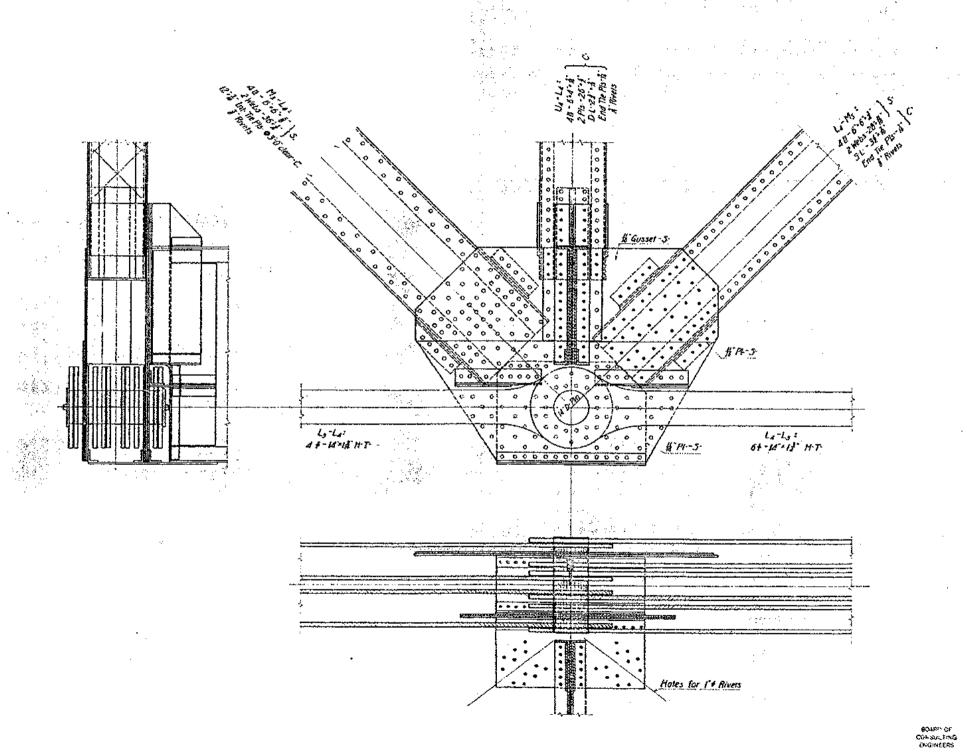
DRAWING NO 20











NOTES:

Hateriol* as notes* C* Corbon Steel. 5* Silicon Steel. HT* Heat-treated Steel.

Rivets - I'd except in main gusset where lield and shop rivets are 16 f.

Elew BW orderff.

Blow Elludrand

Augustina

Lord Harris A.

L

STATE OF CALIFORNIA
DEPARTMENT OF PUBLIC WORKS

SAN FRANCISCO-OAKLAND BAY BRIDGE

SUPERSTRUCTURE-EAST BAY CROSSING

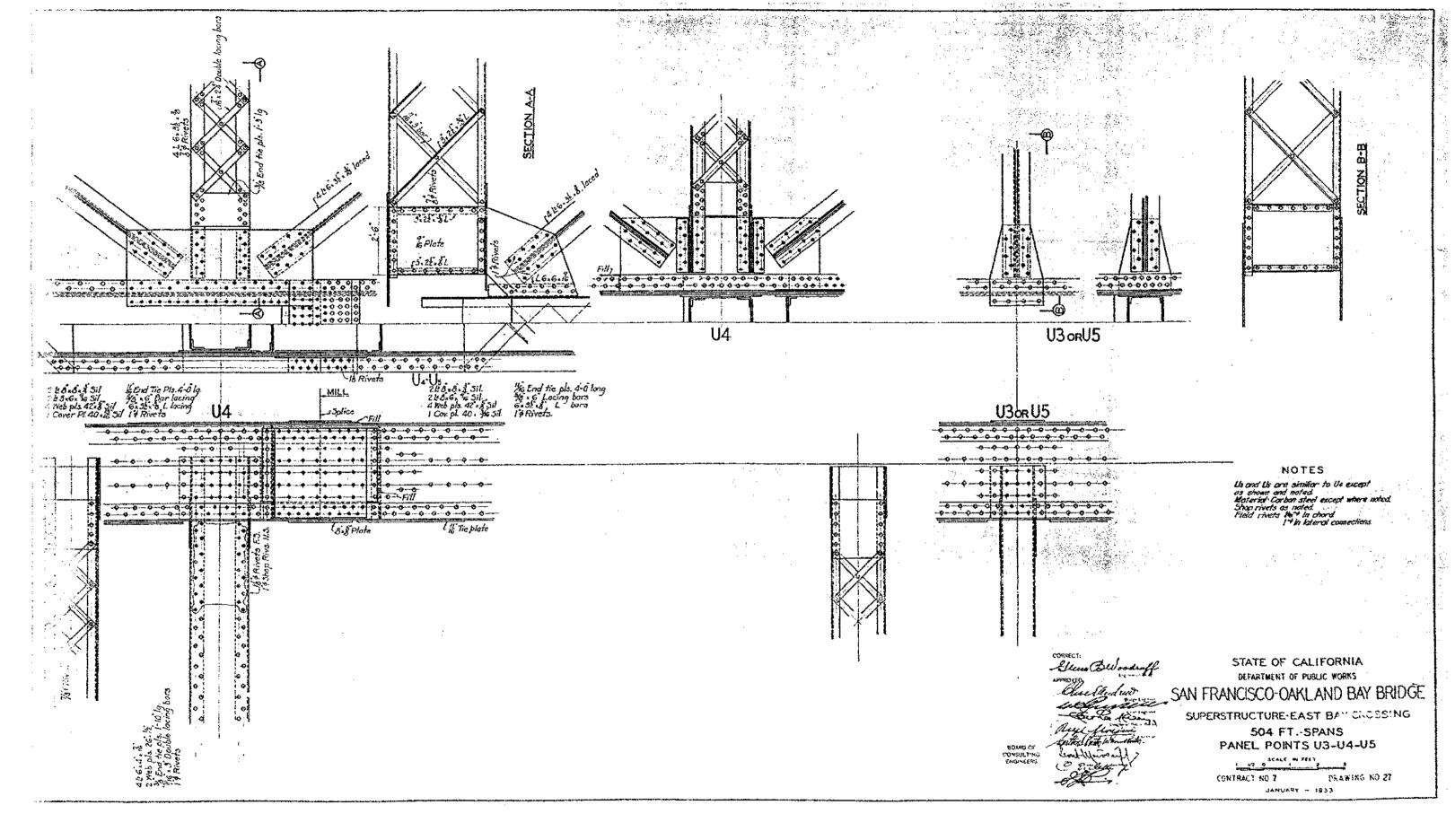
504 FT. SPANS PANEL POINT L4

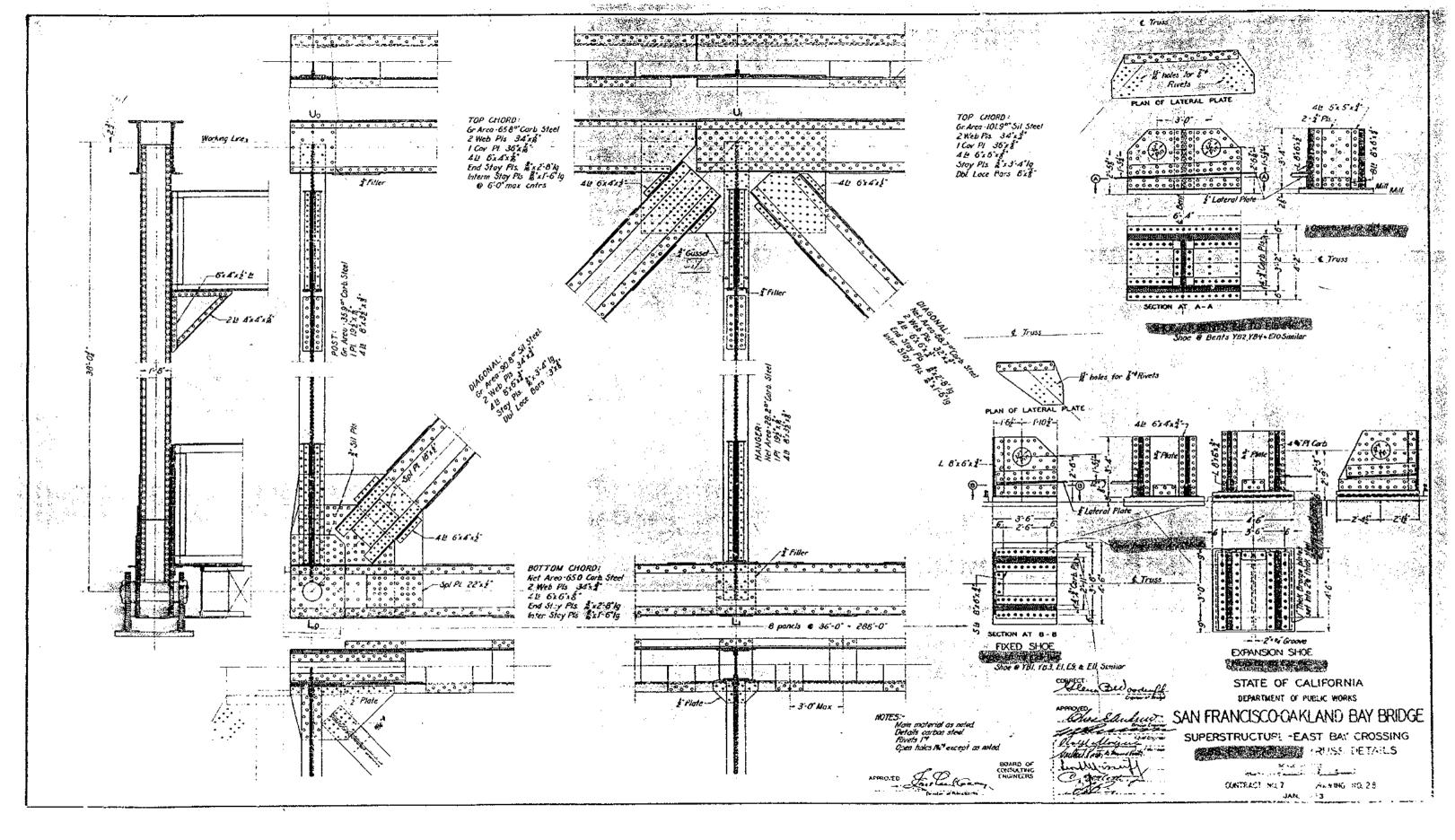
SALE IN REET

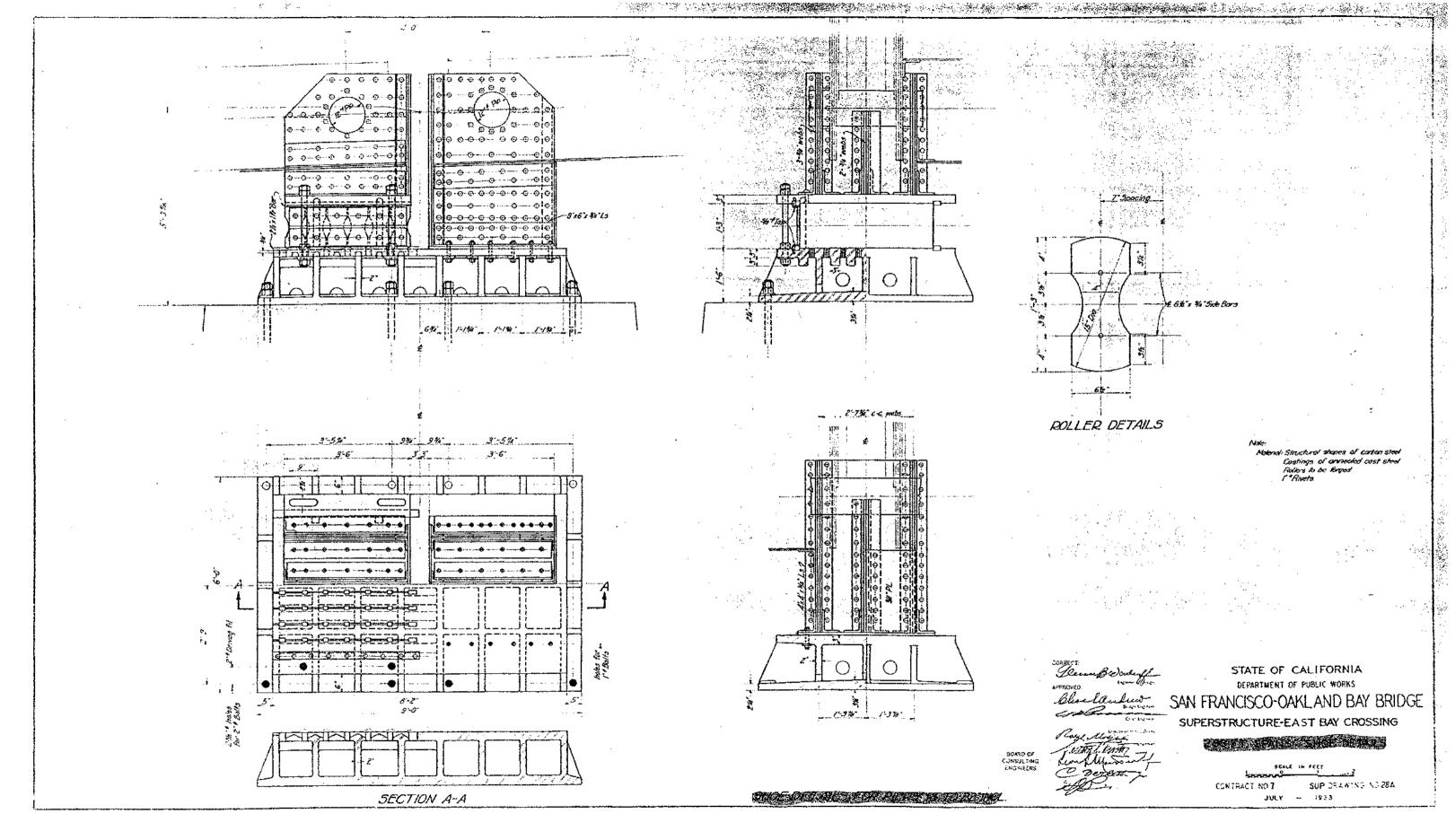
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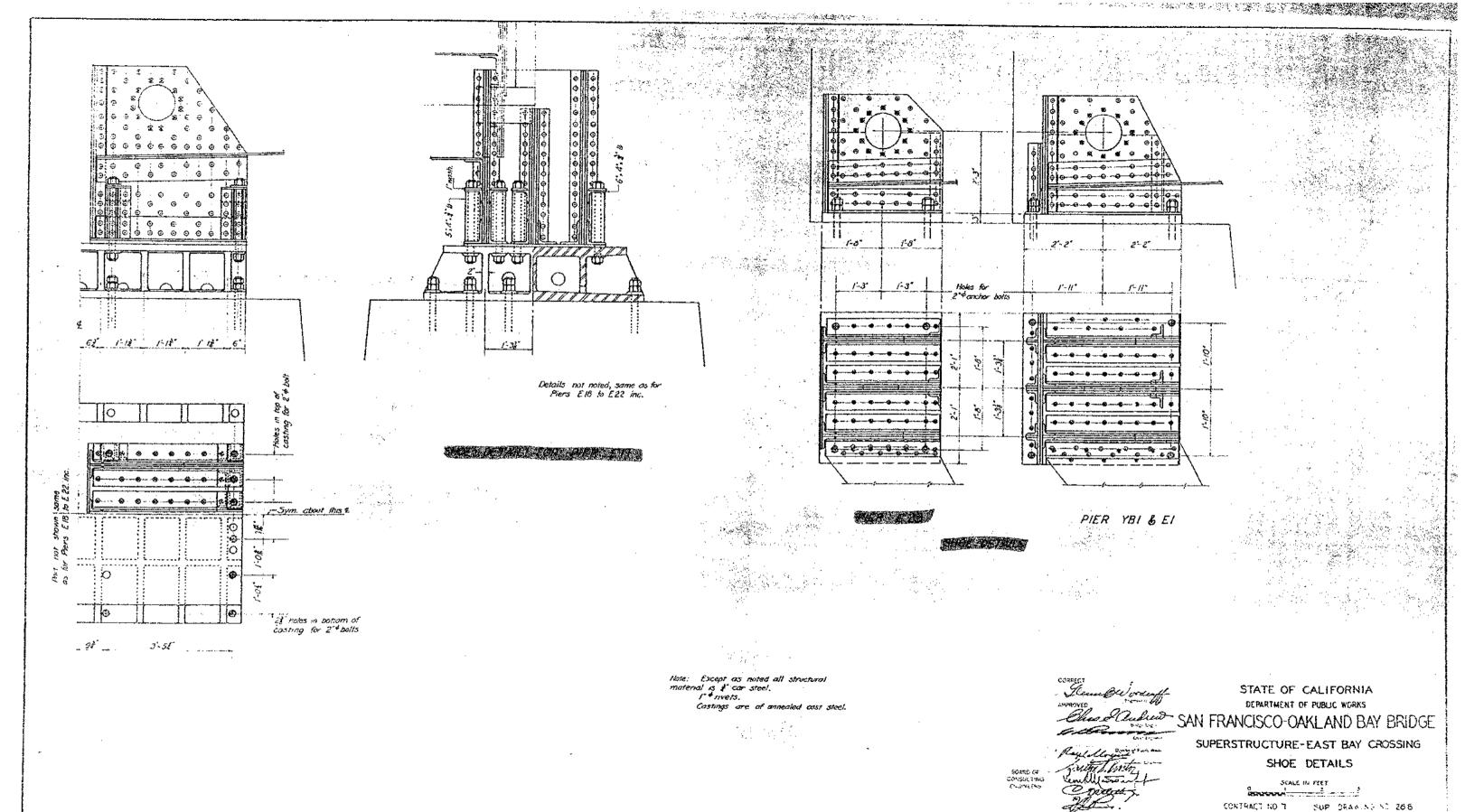
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JANUARY - 1933

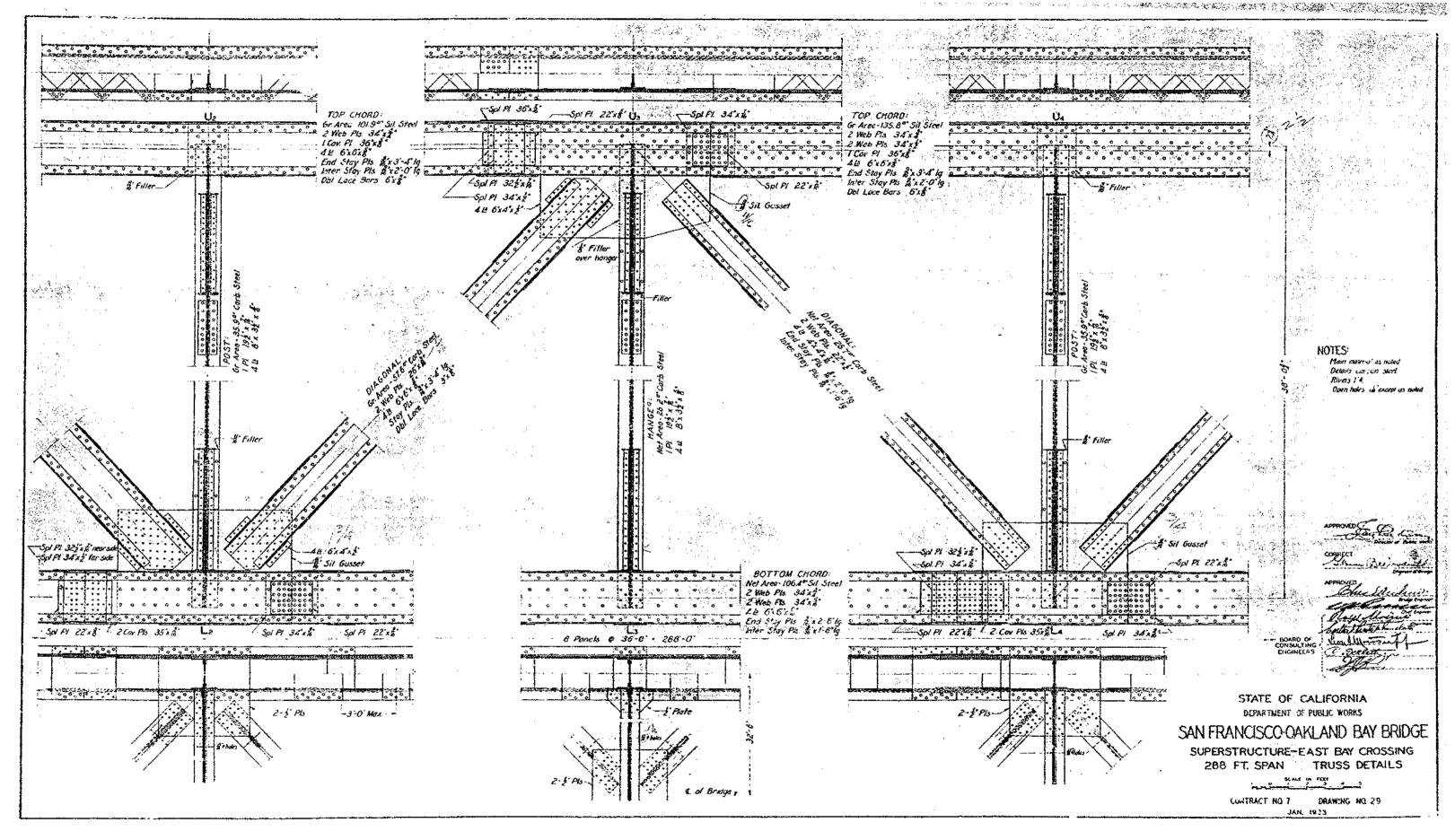


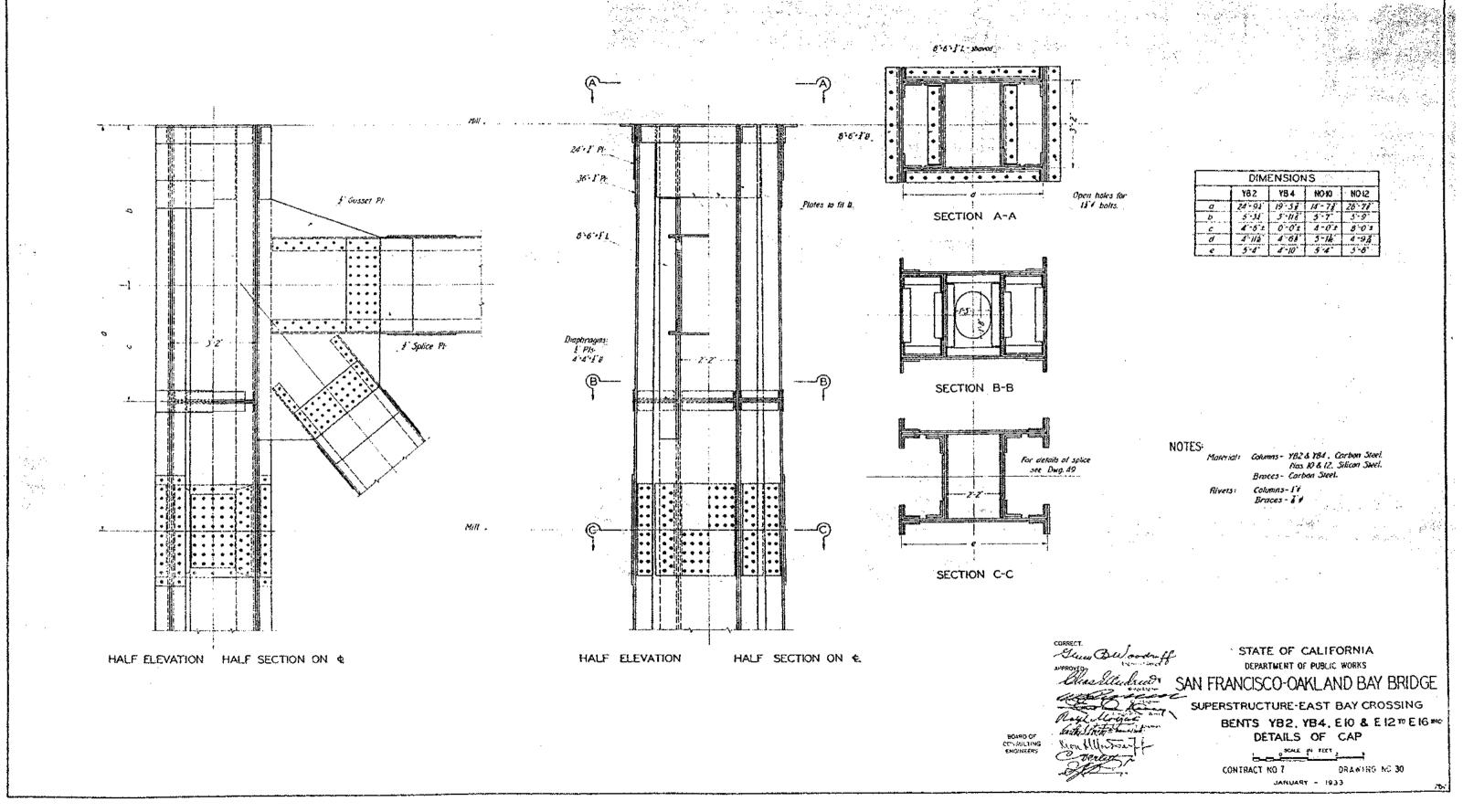


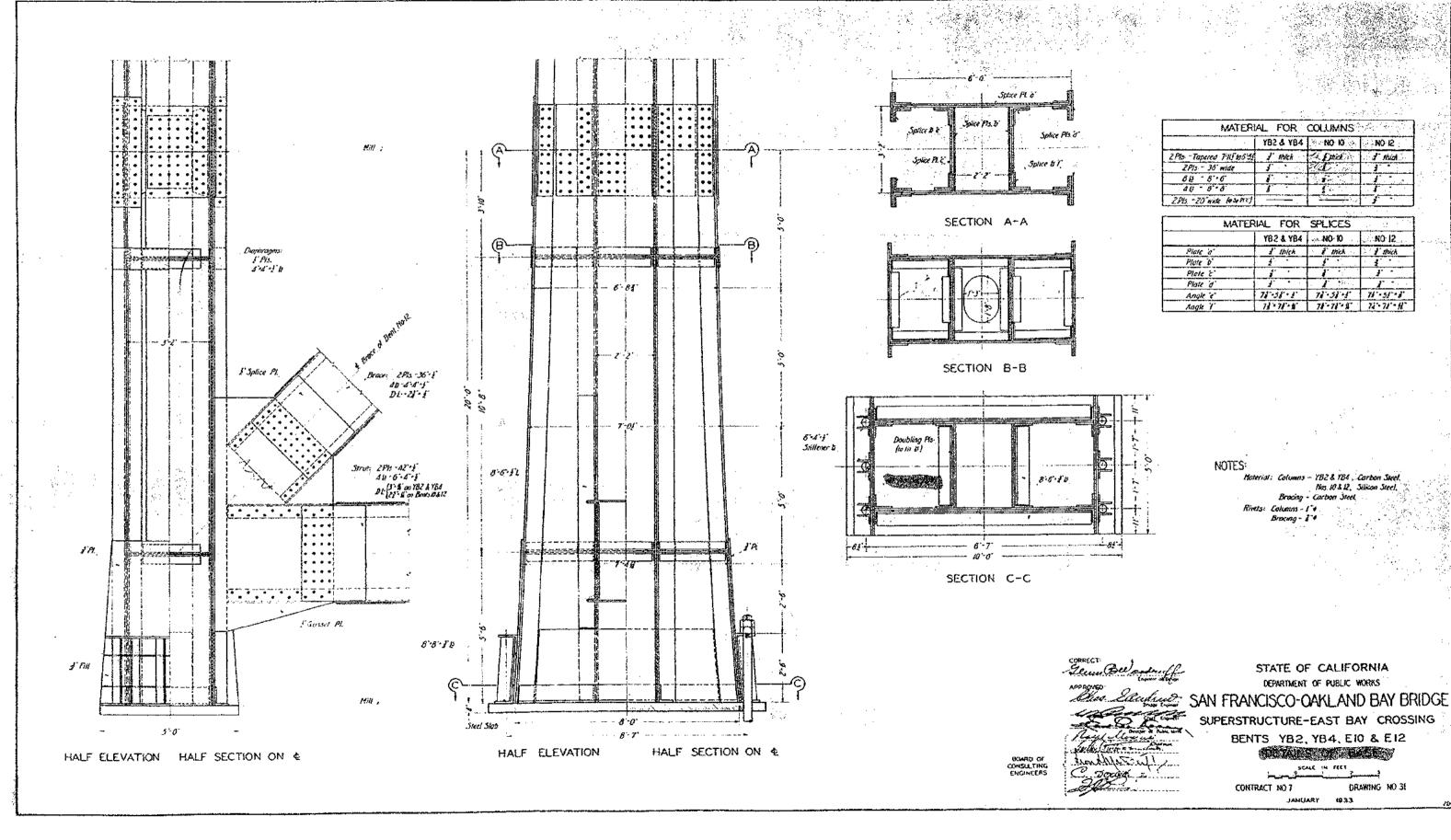


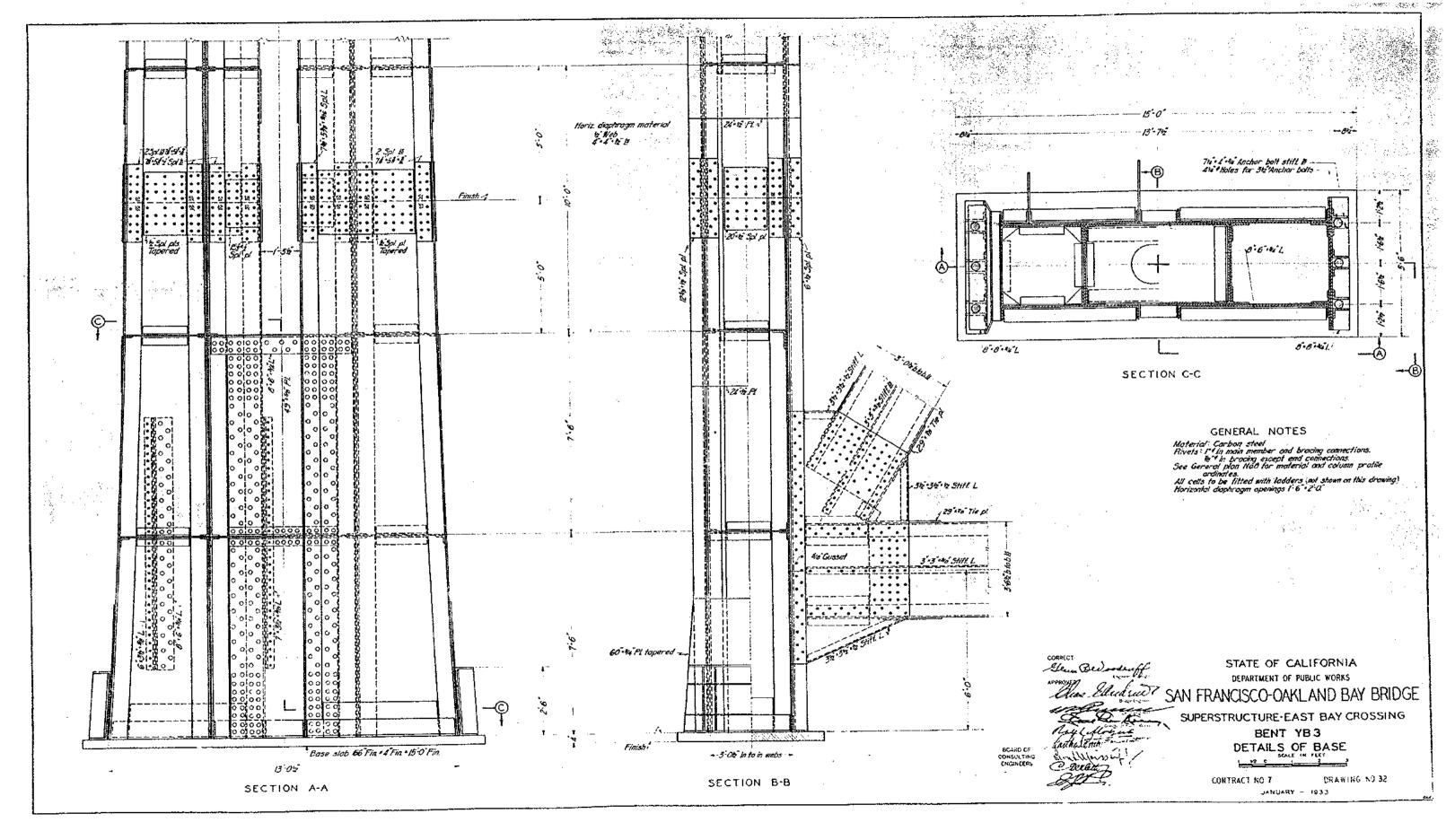


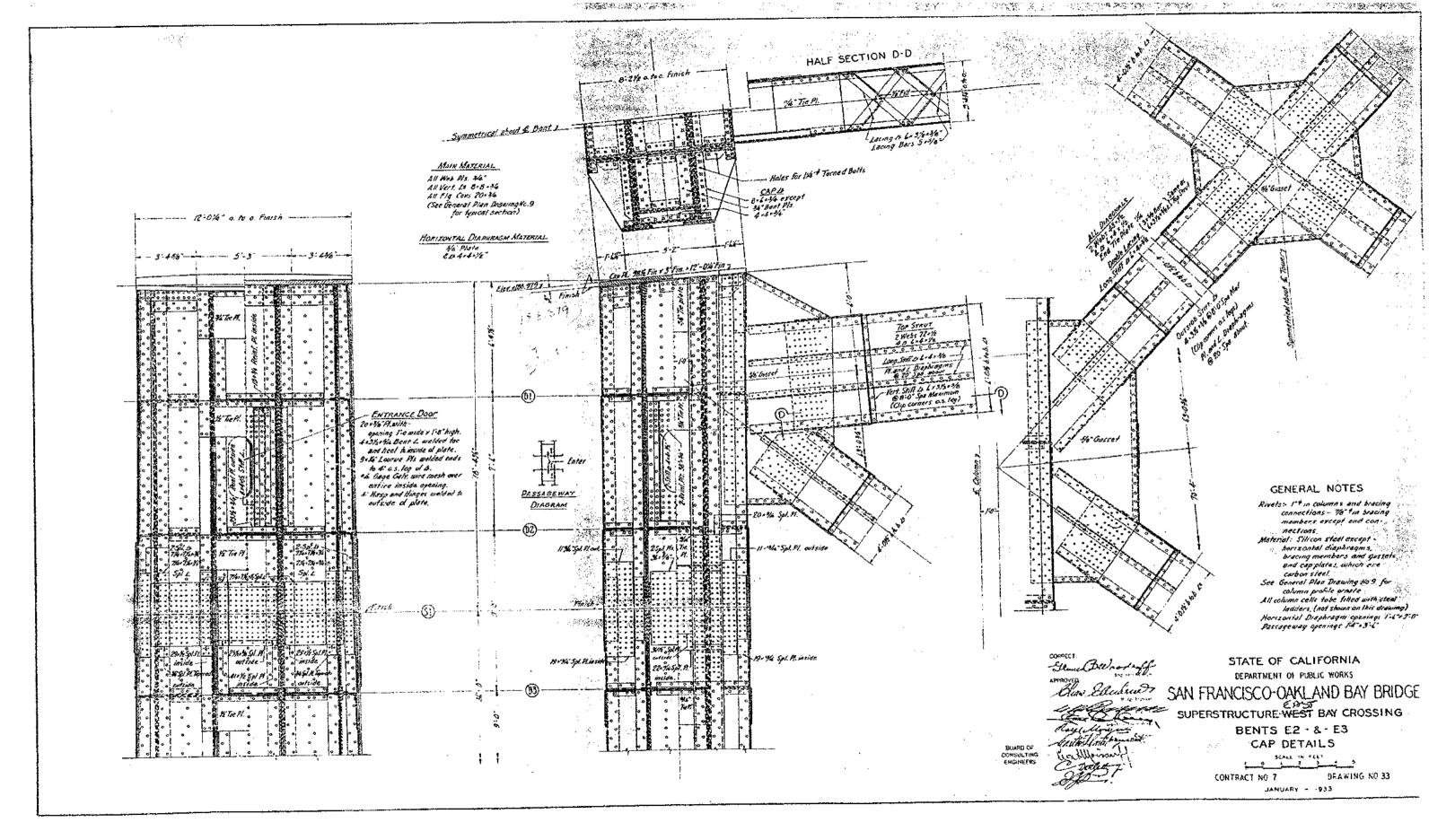
JANUARY - 1933

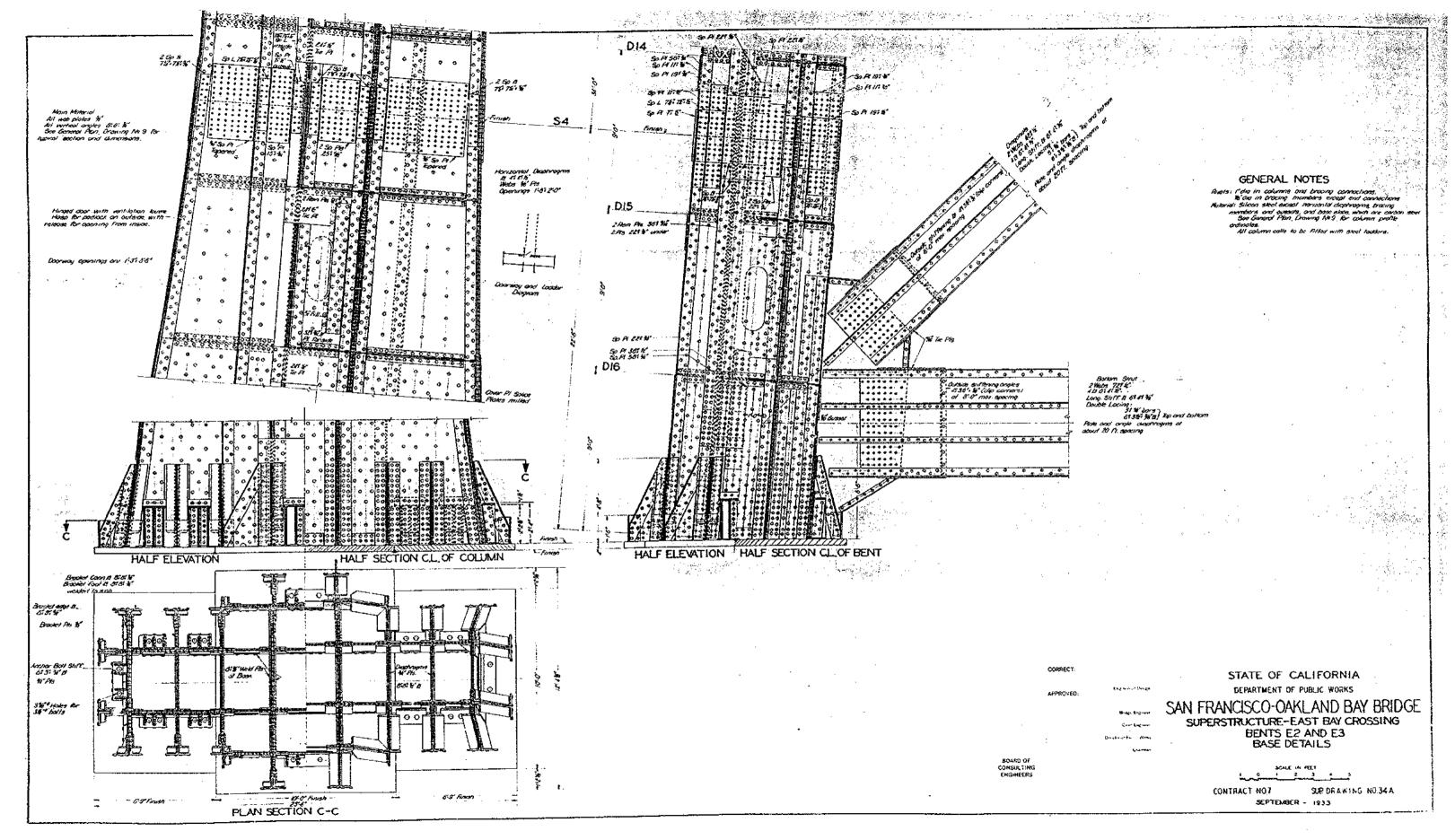


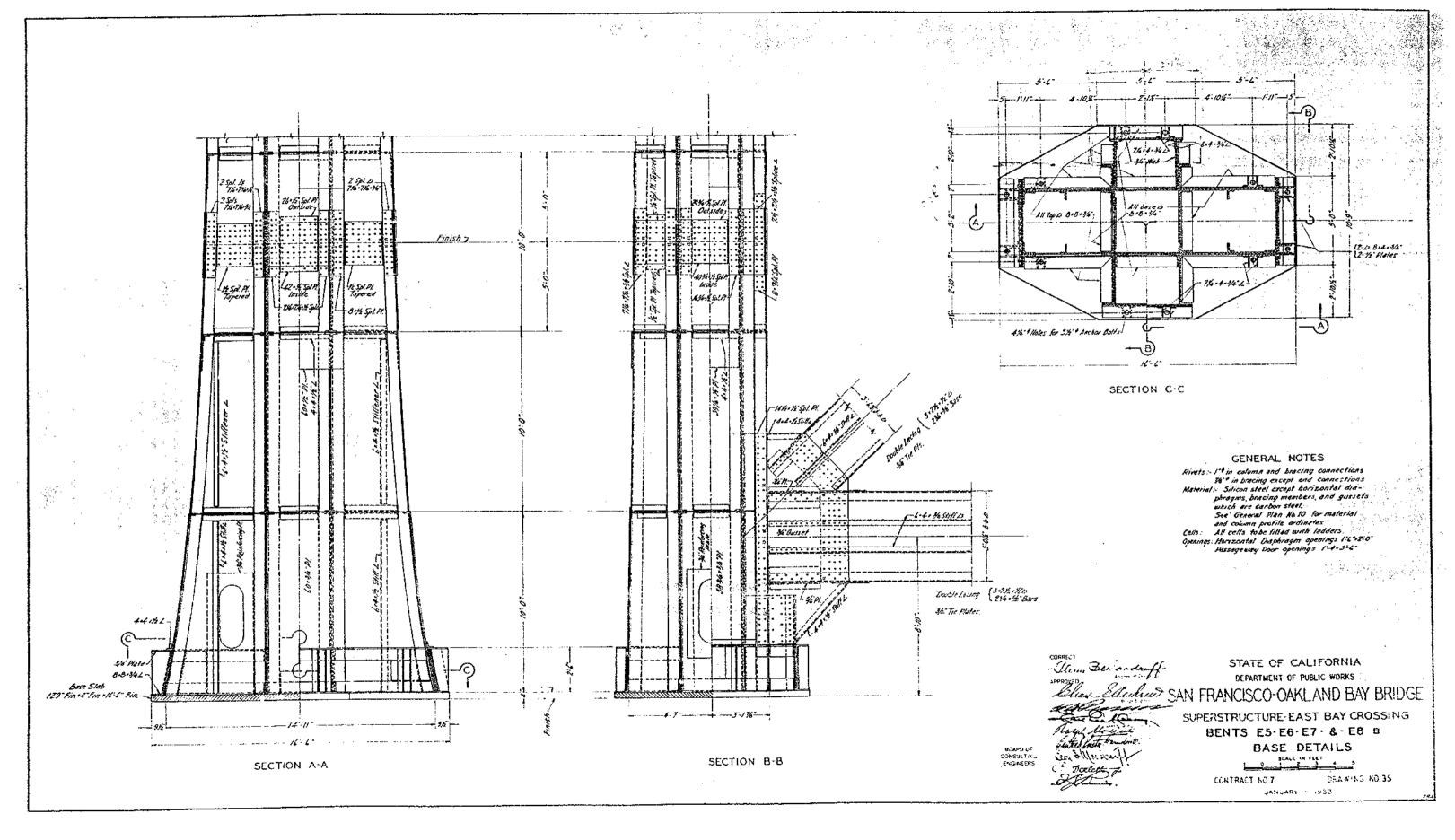


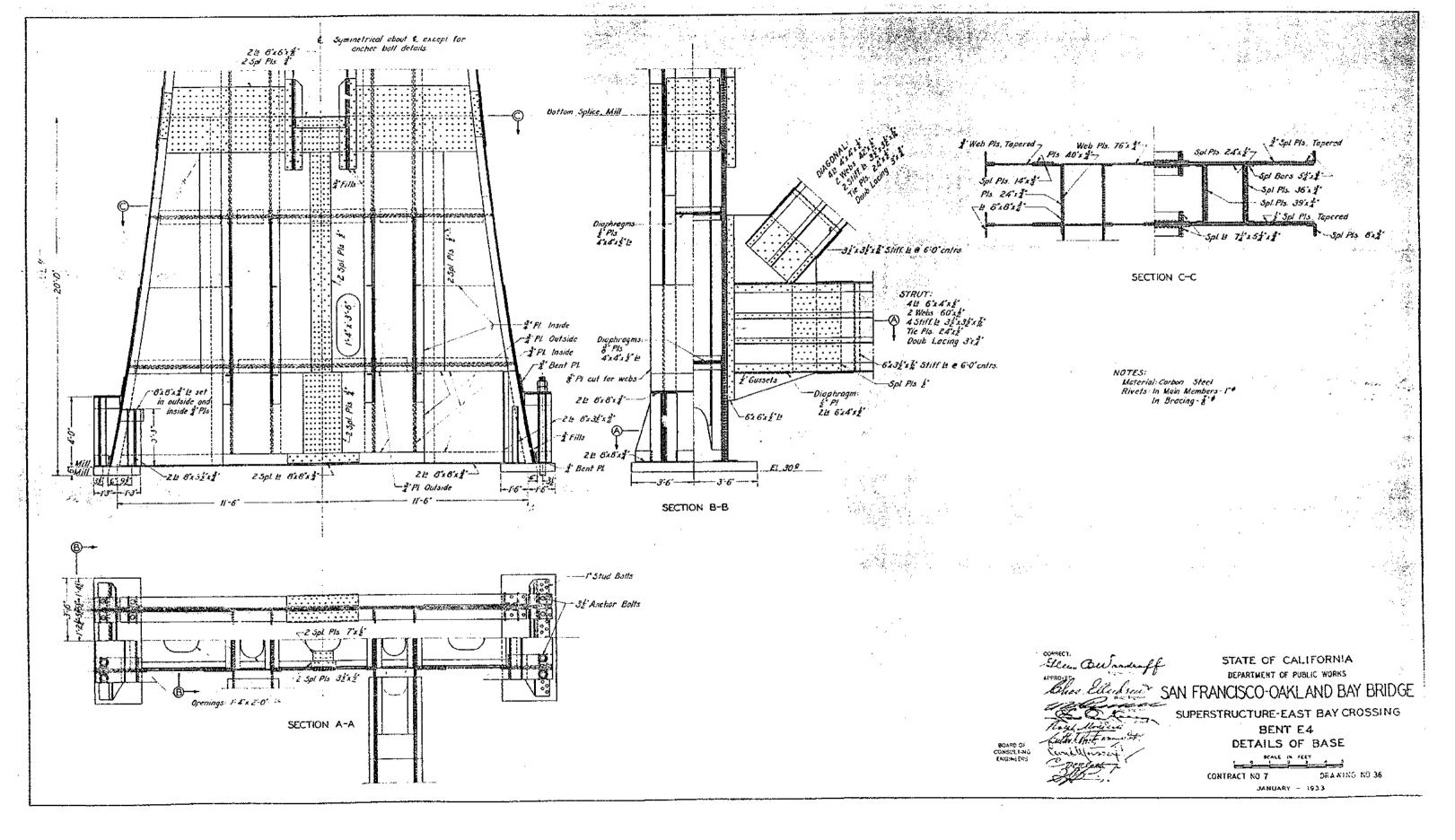


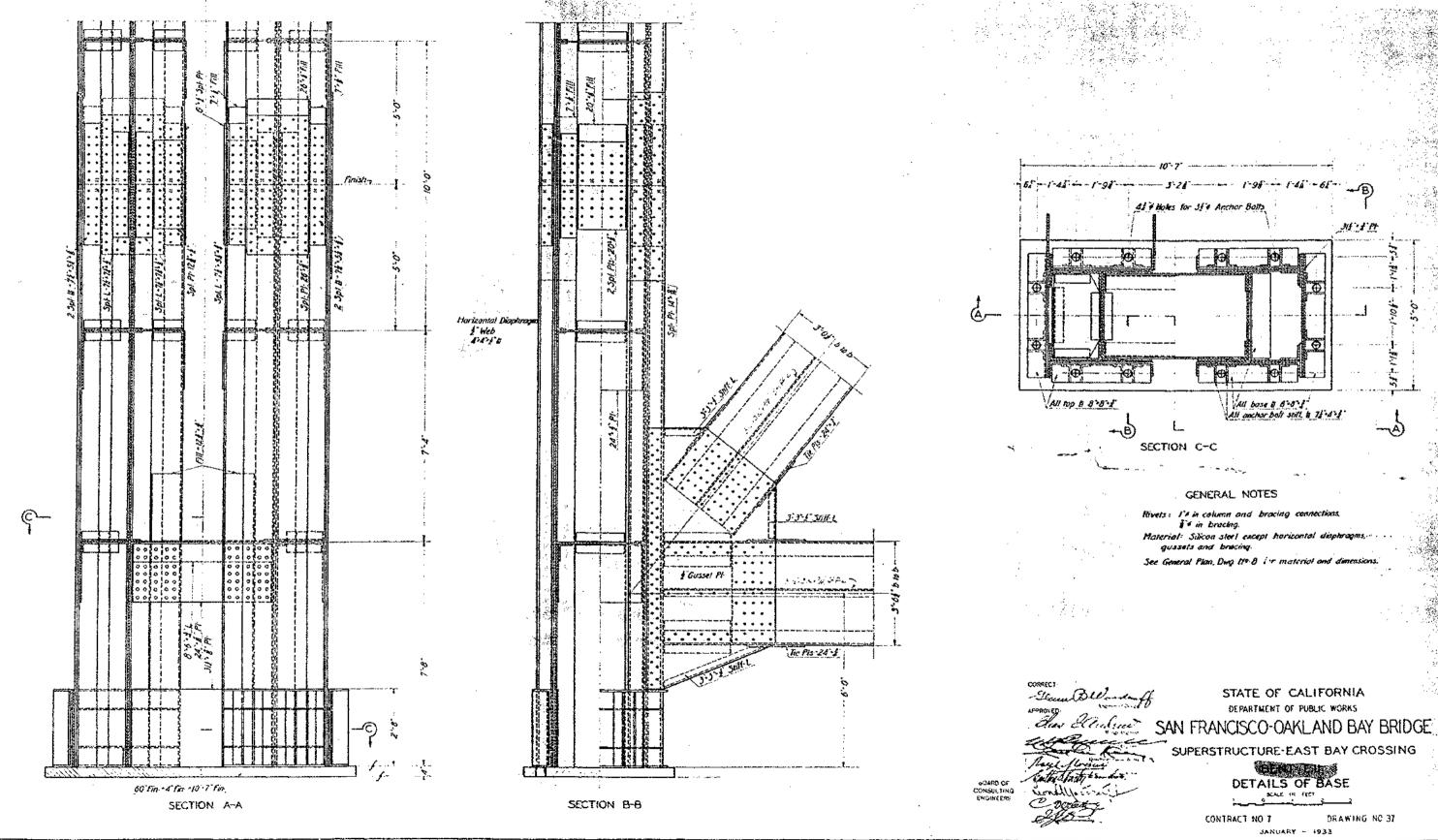




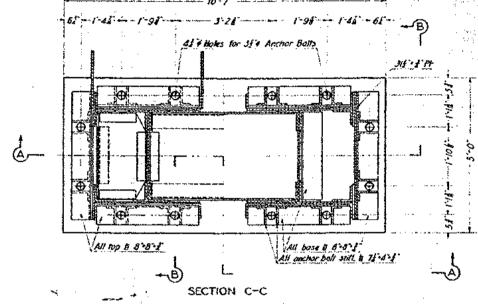








化氯化磺胺 医抗皮囊 化分类 化二苯基



GENERAL NOTES

Rivets: I's in column and bracing connections, ₹ in bracing.

Material: Silicon steel except horizontal diaphrogms,... gussets and bracing.

See General Plan, Dwg 11º 8 1 or materiol and dimensions.

STATE OF CALIFORNIA

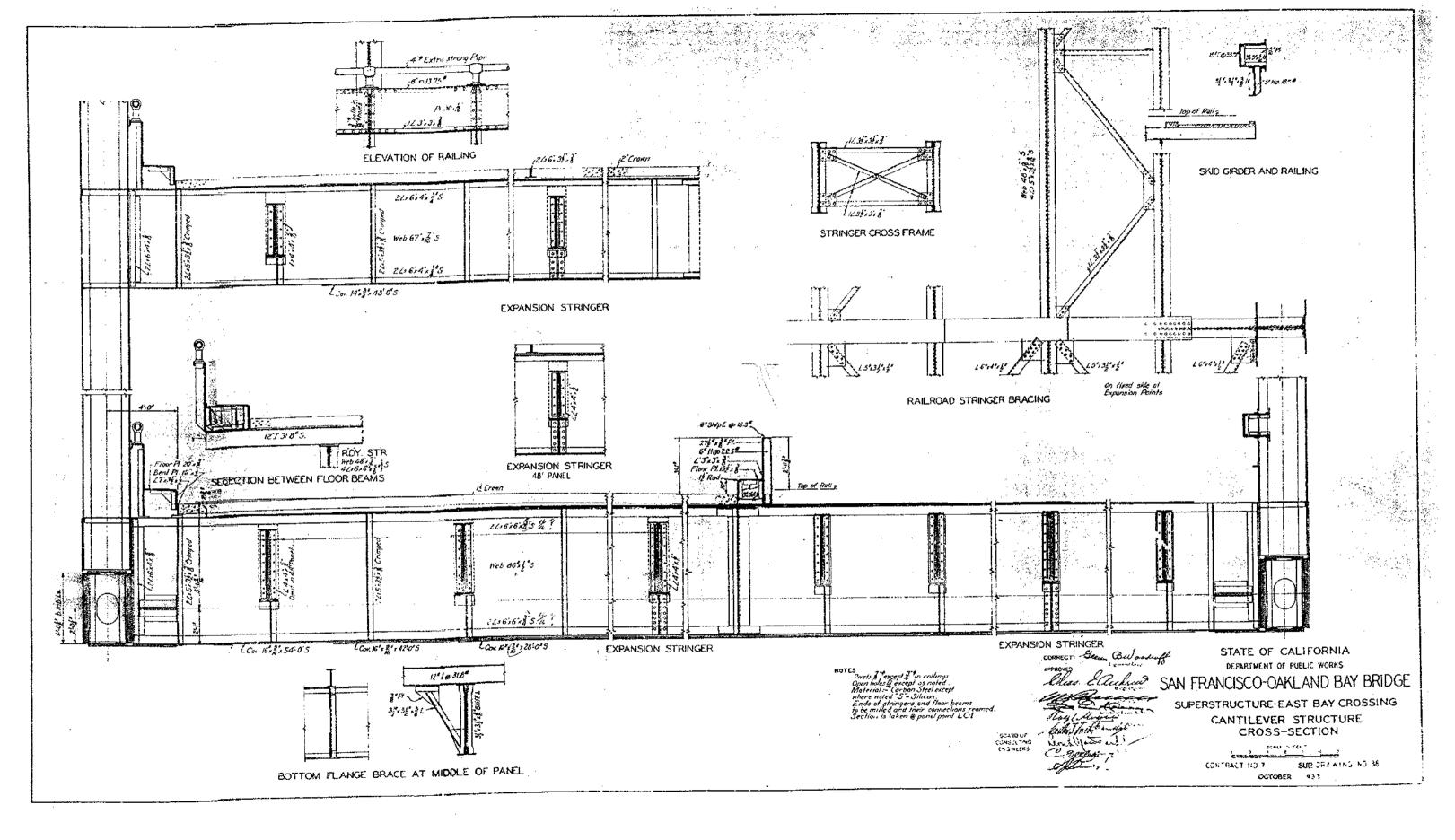
DEPARTMENT OF PUBLIC WORKS

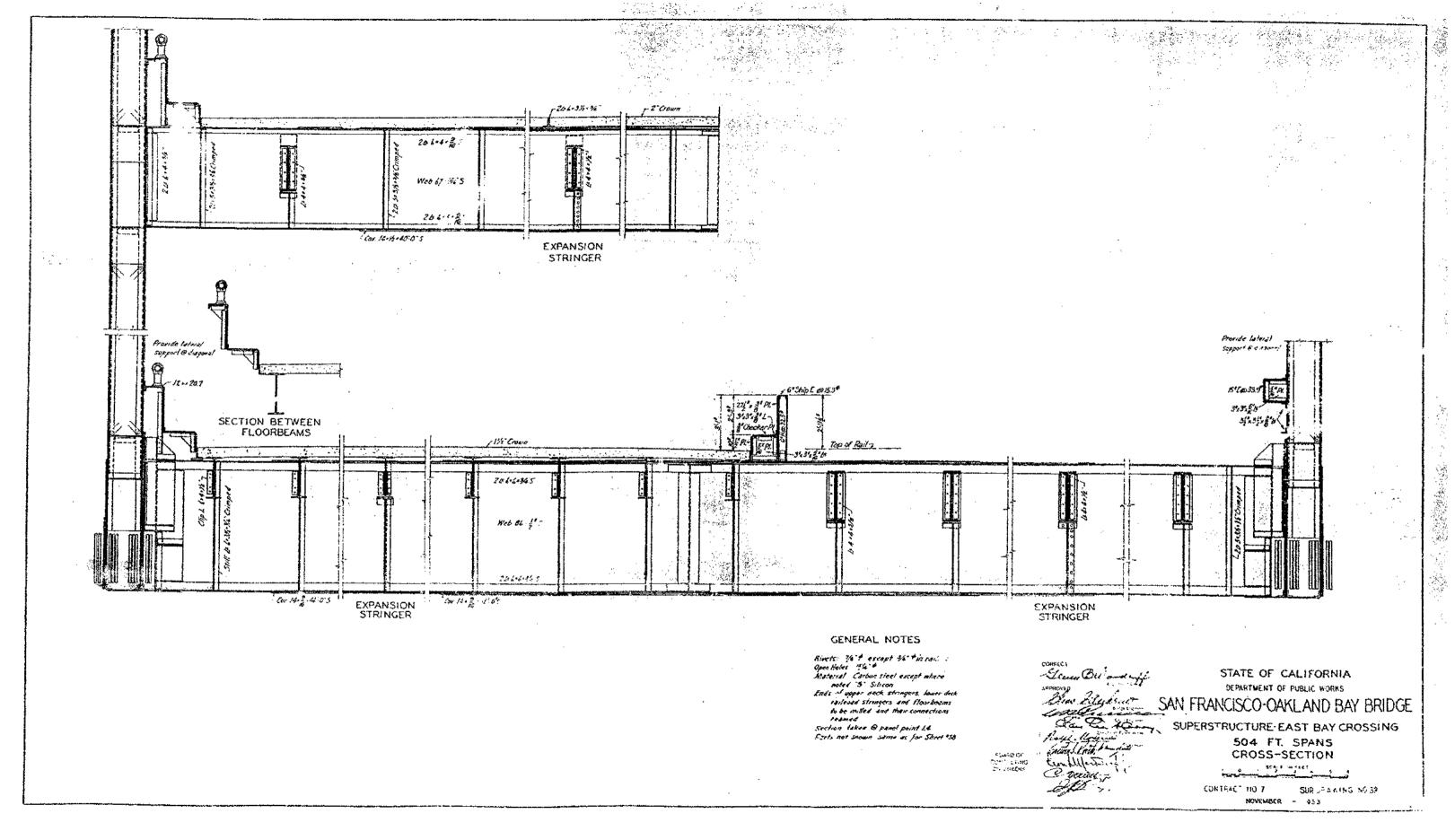


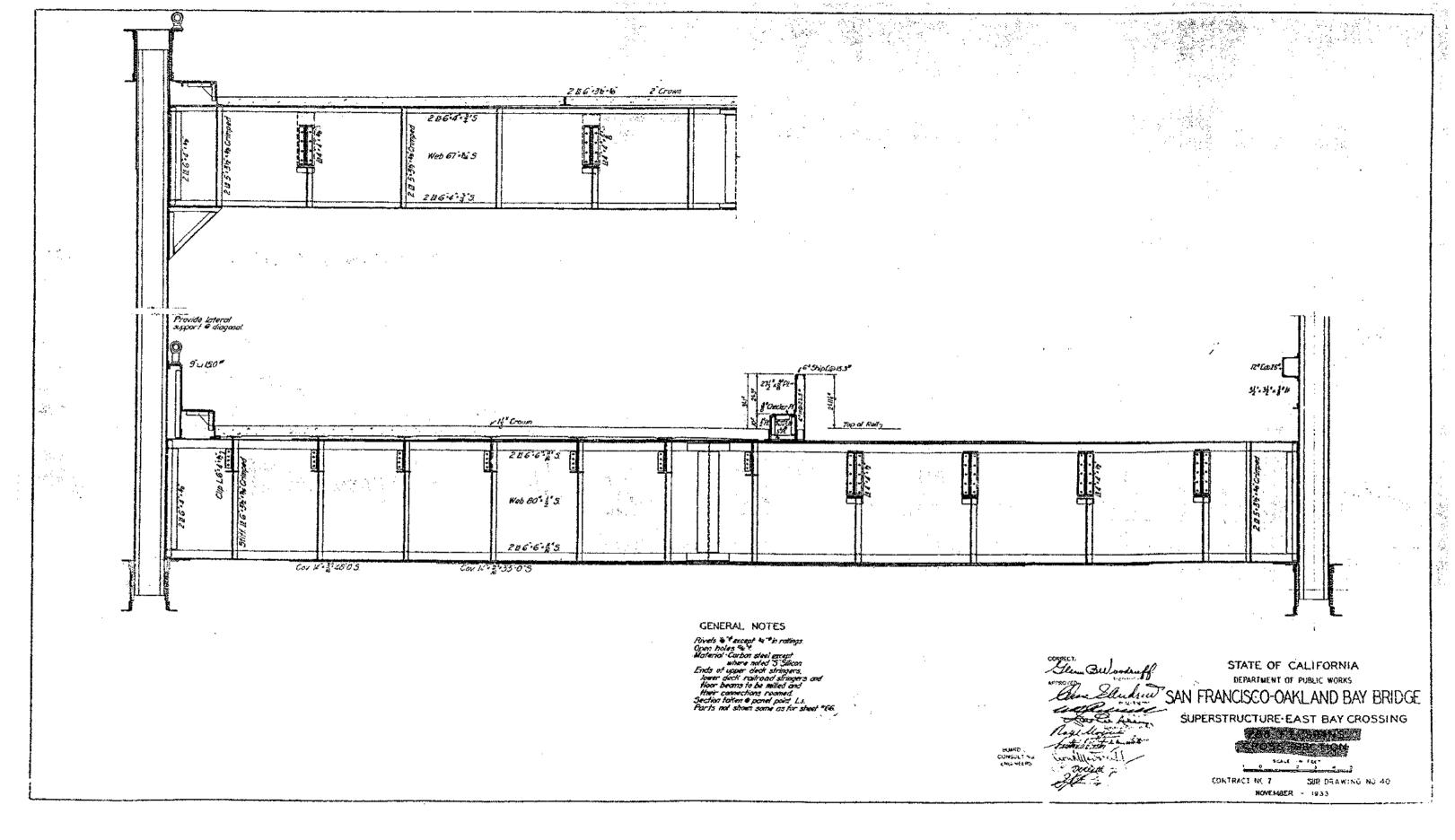
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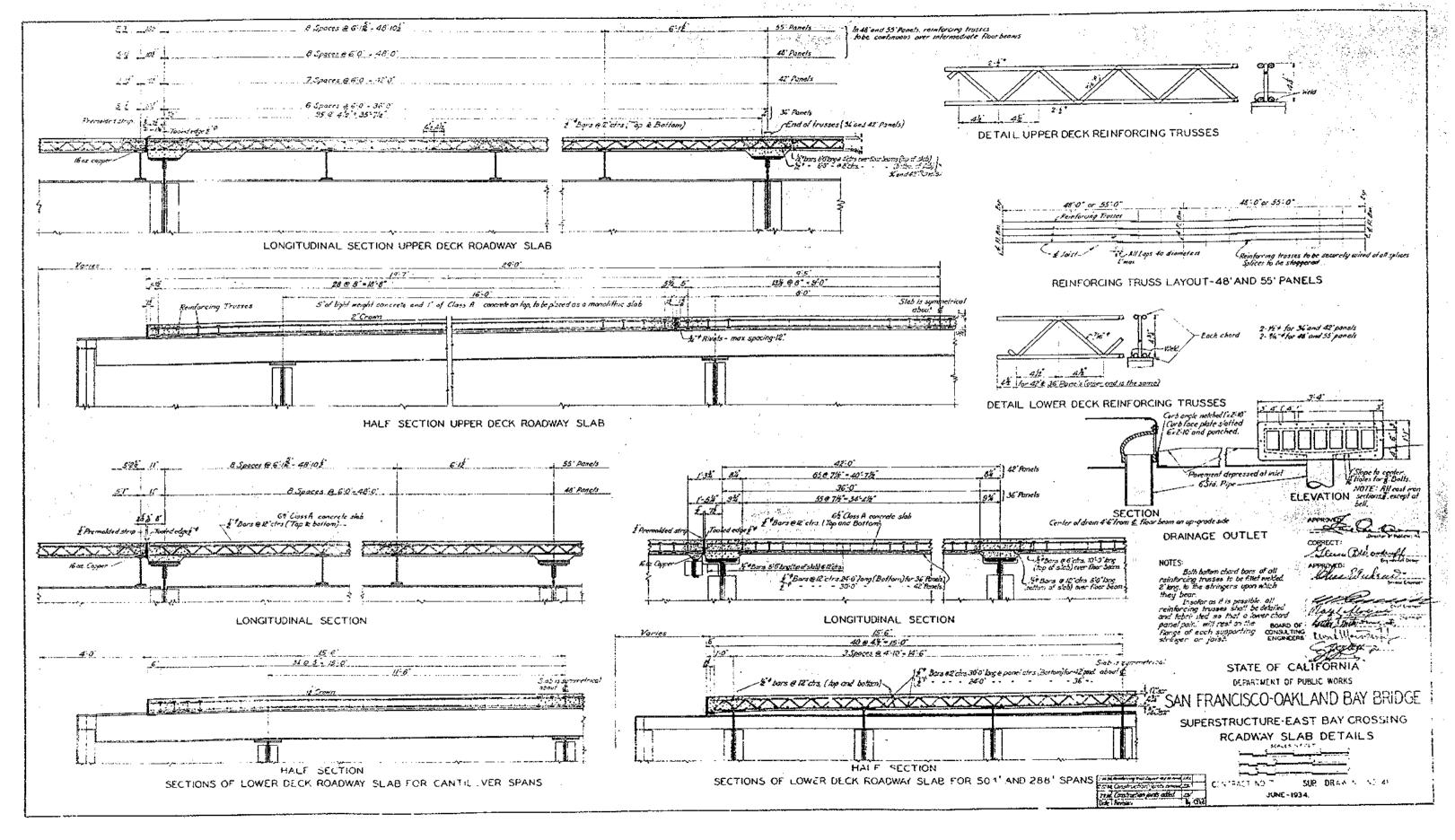
DRAWING NO 37

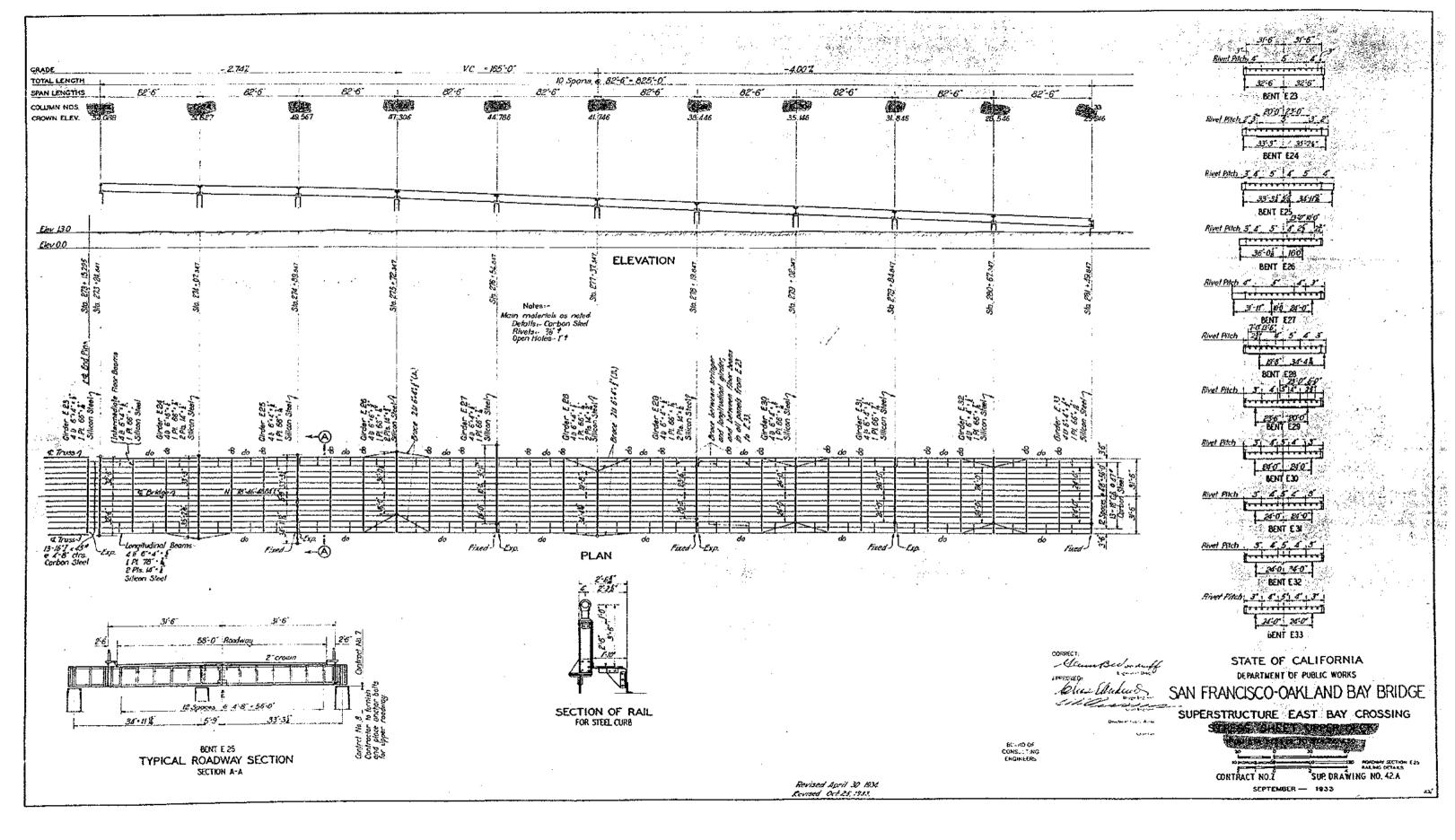
JANUARY - 1933

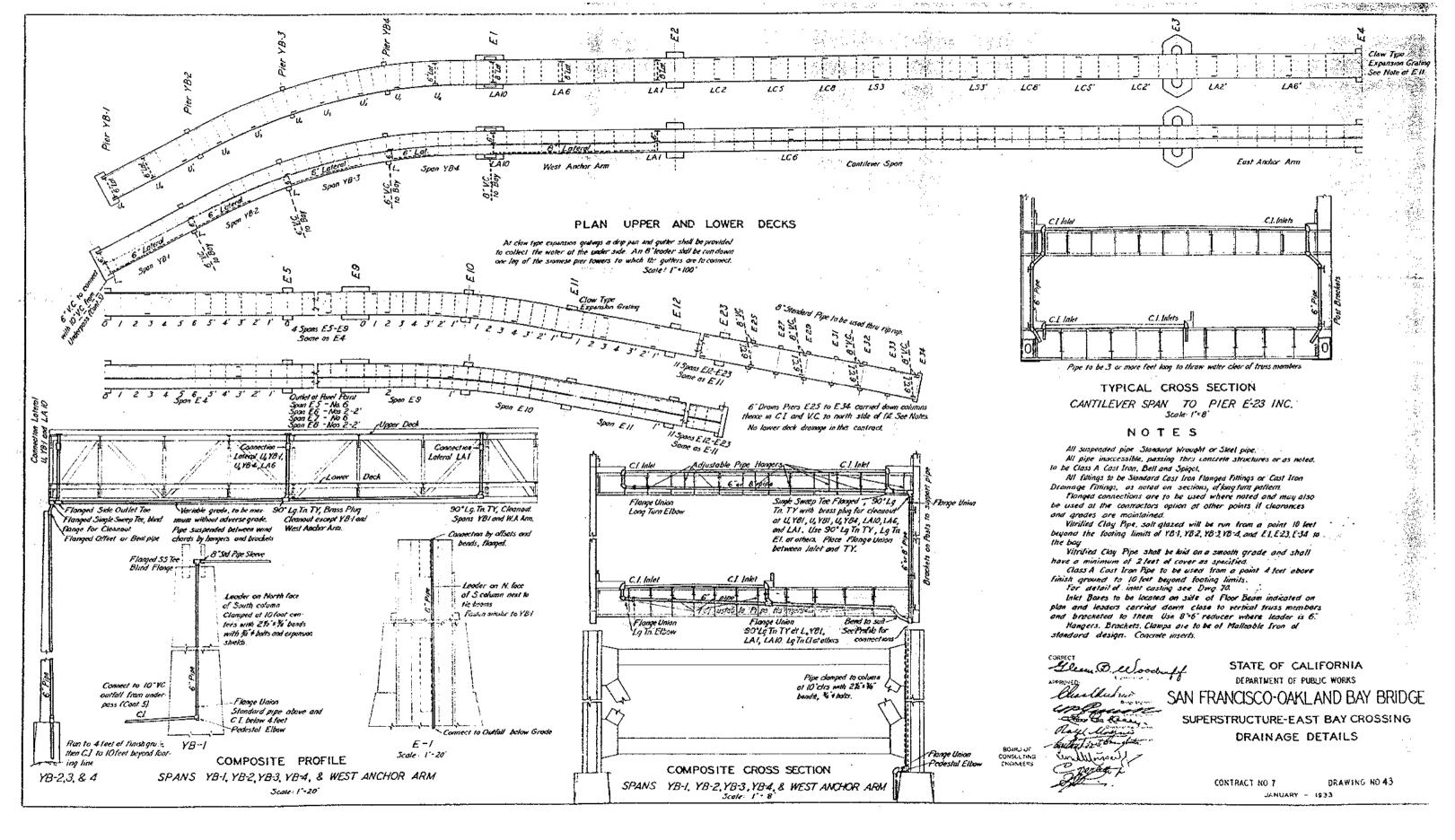


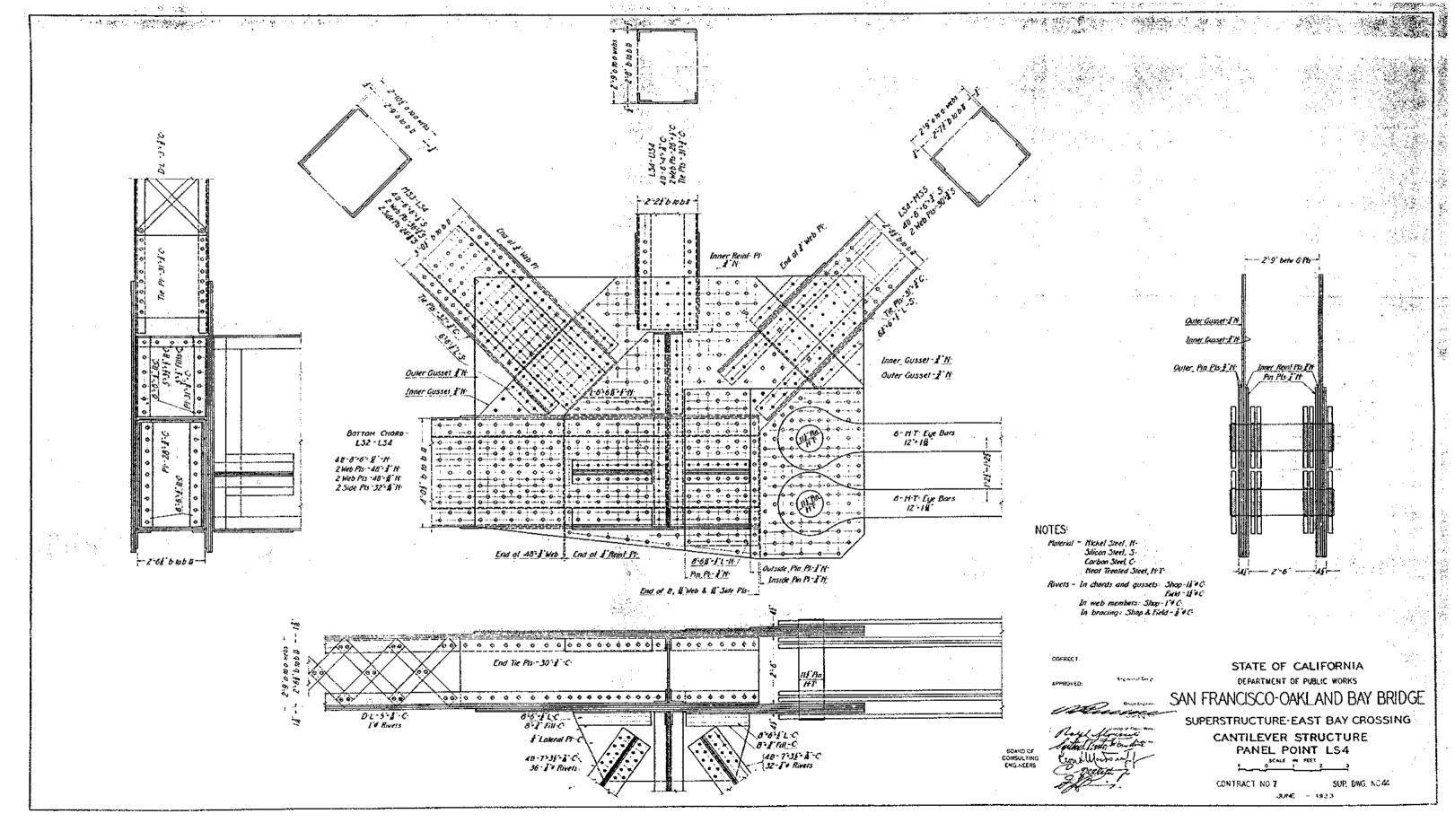


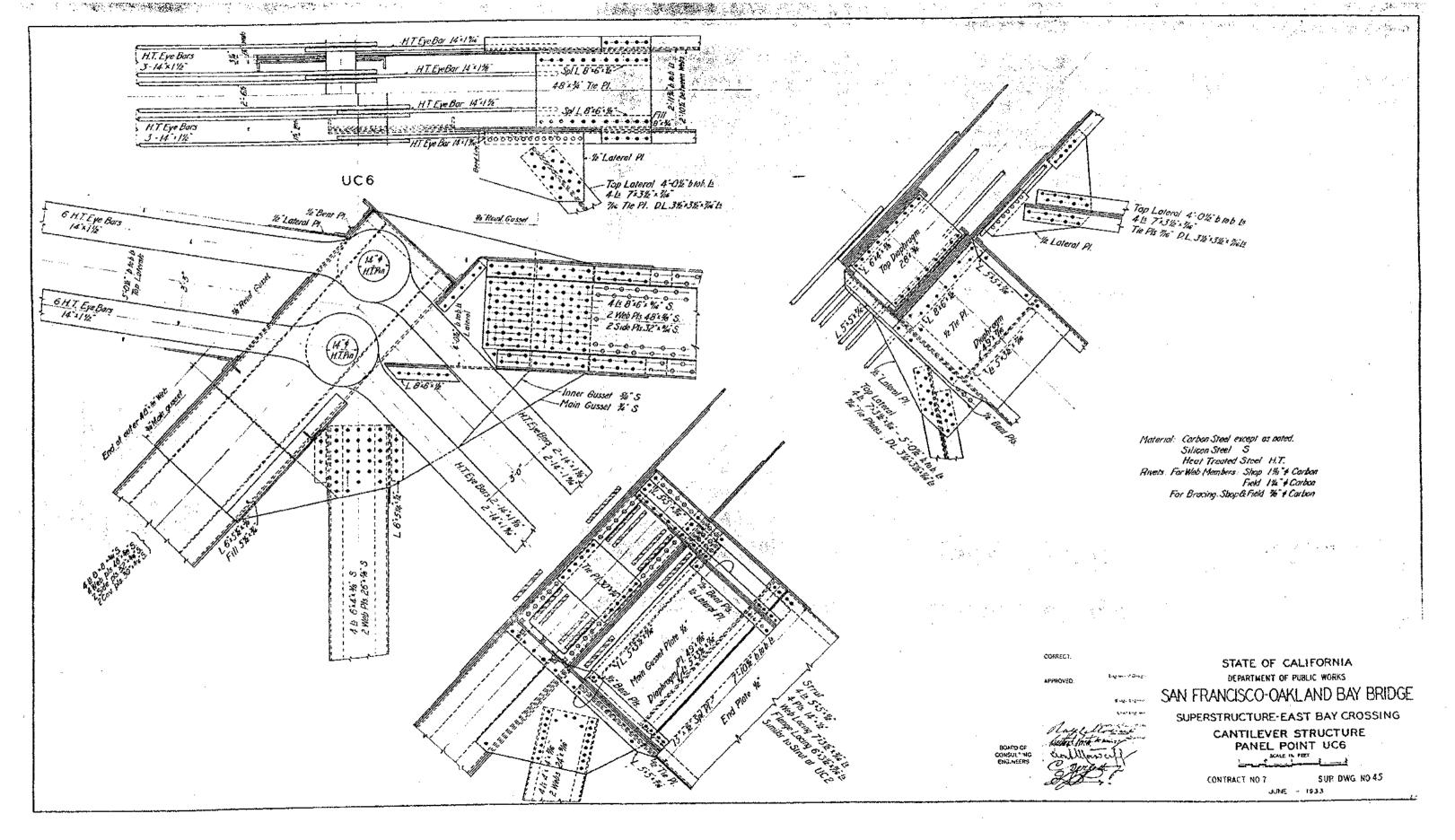


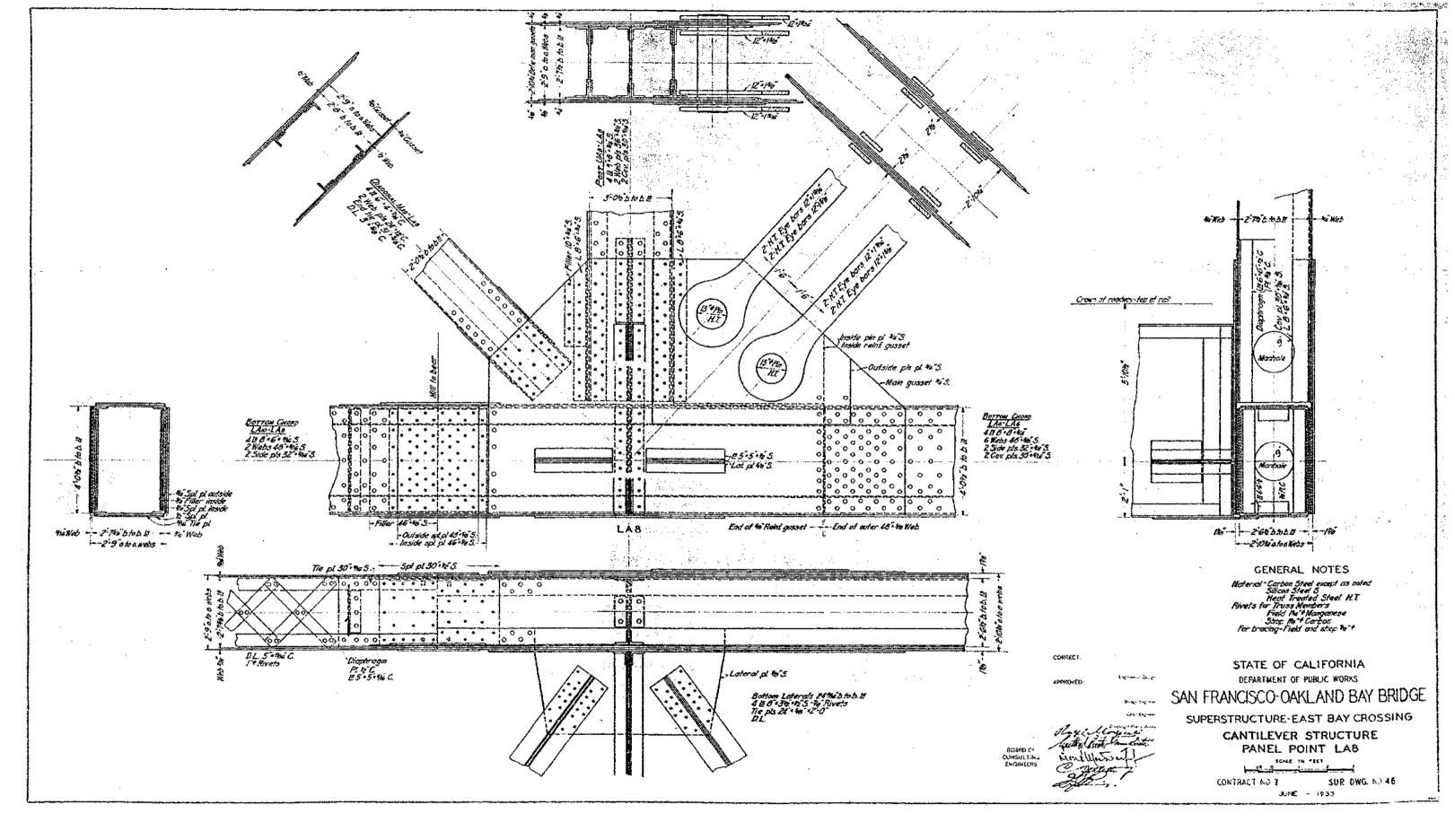


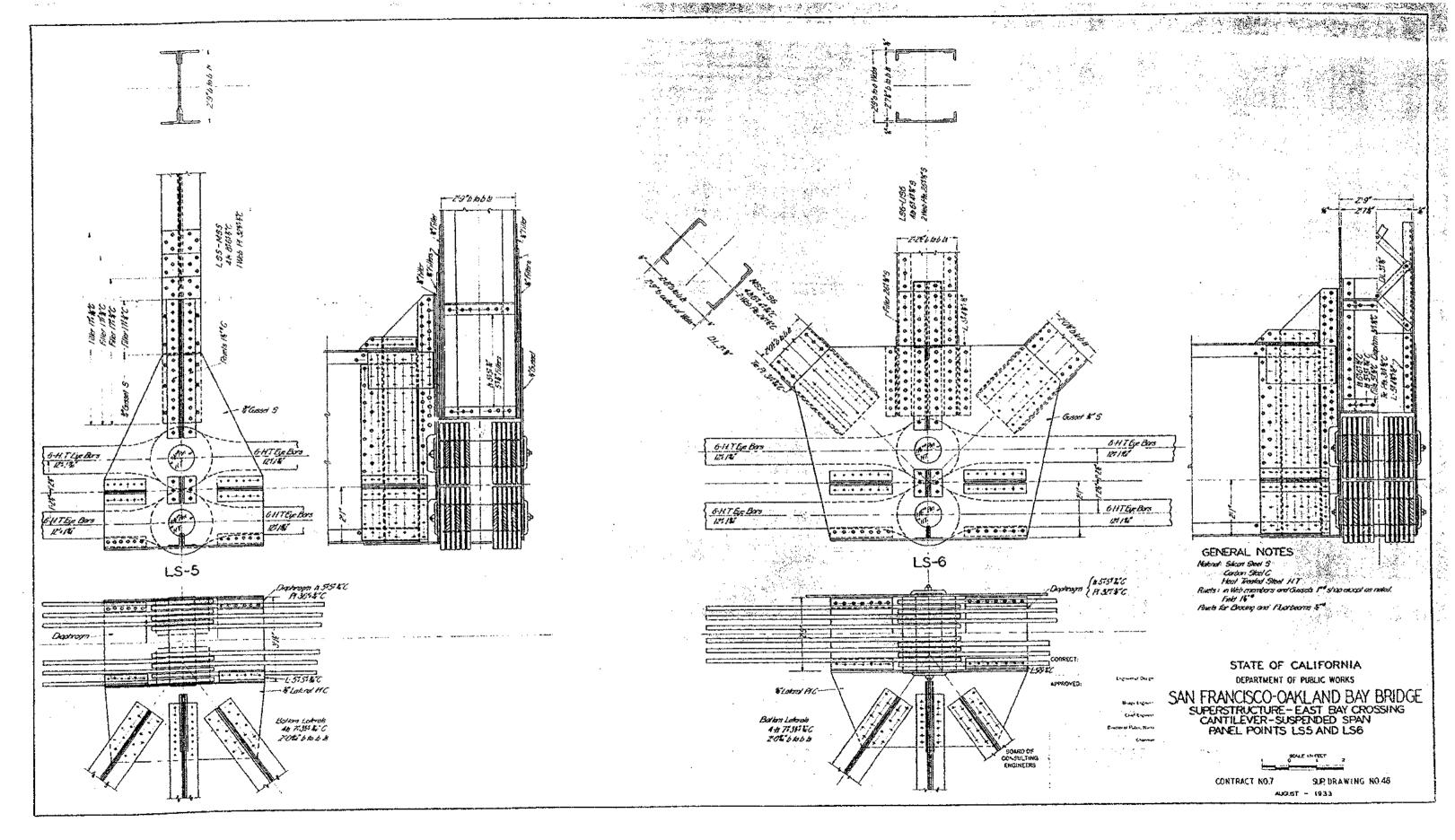


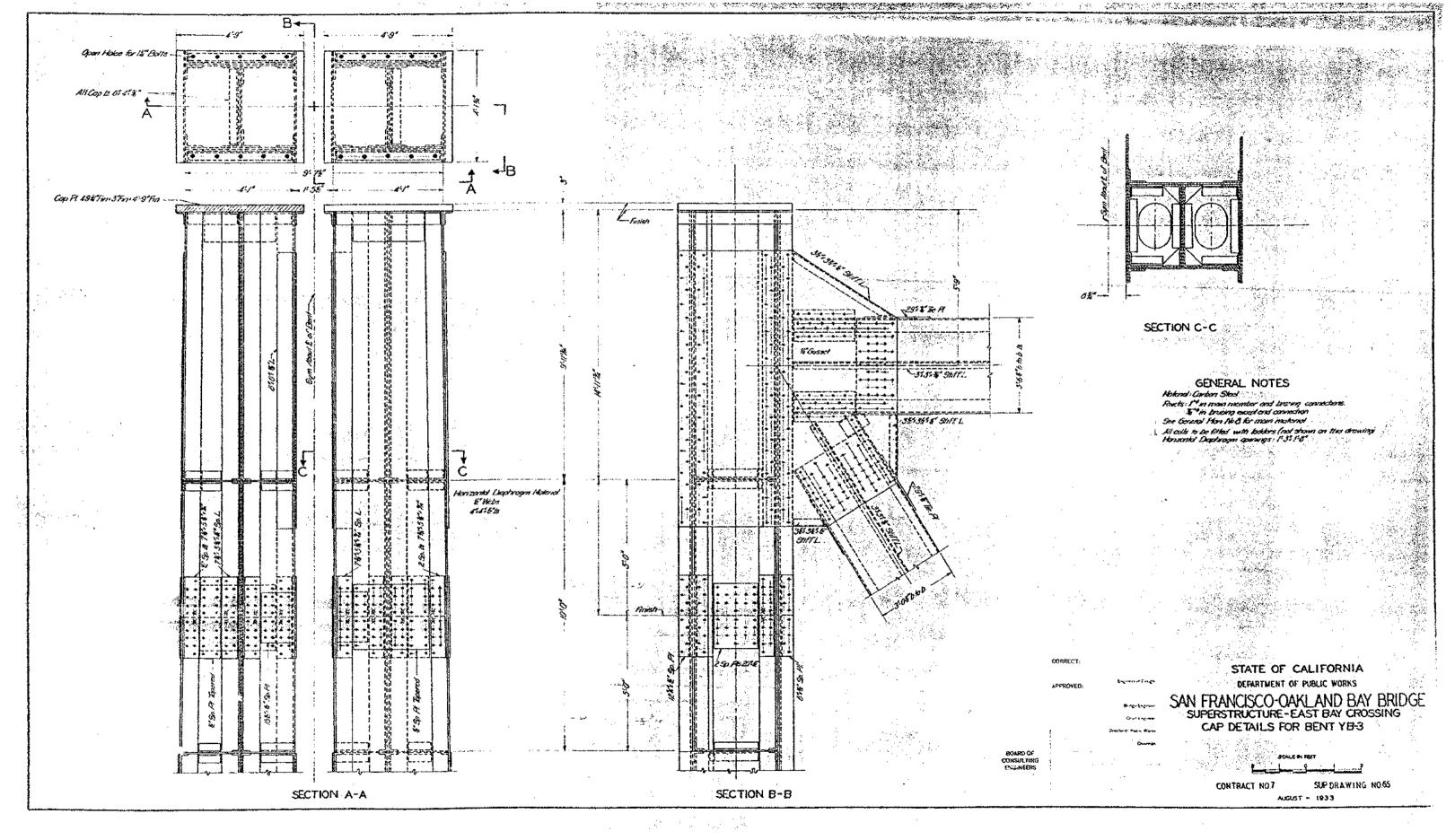


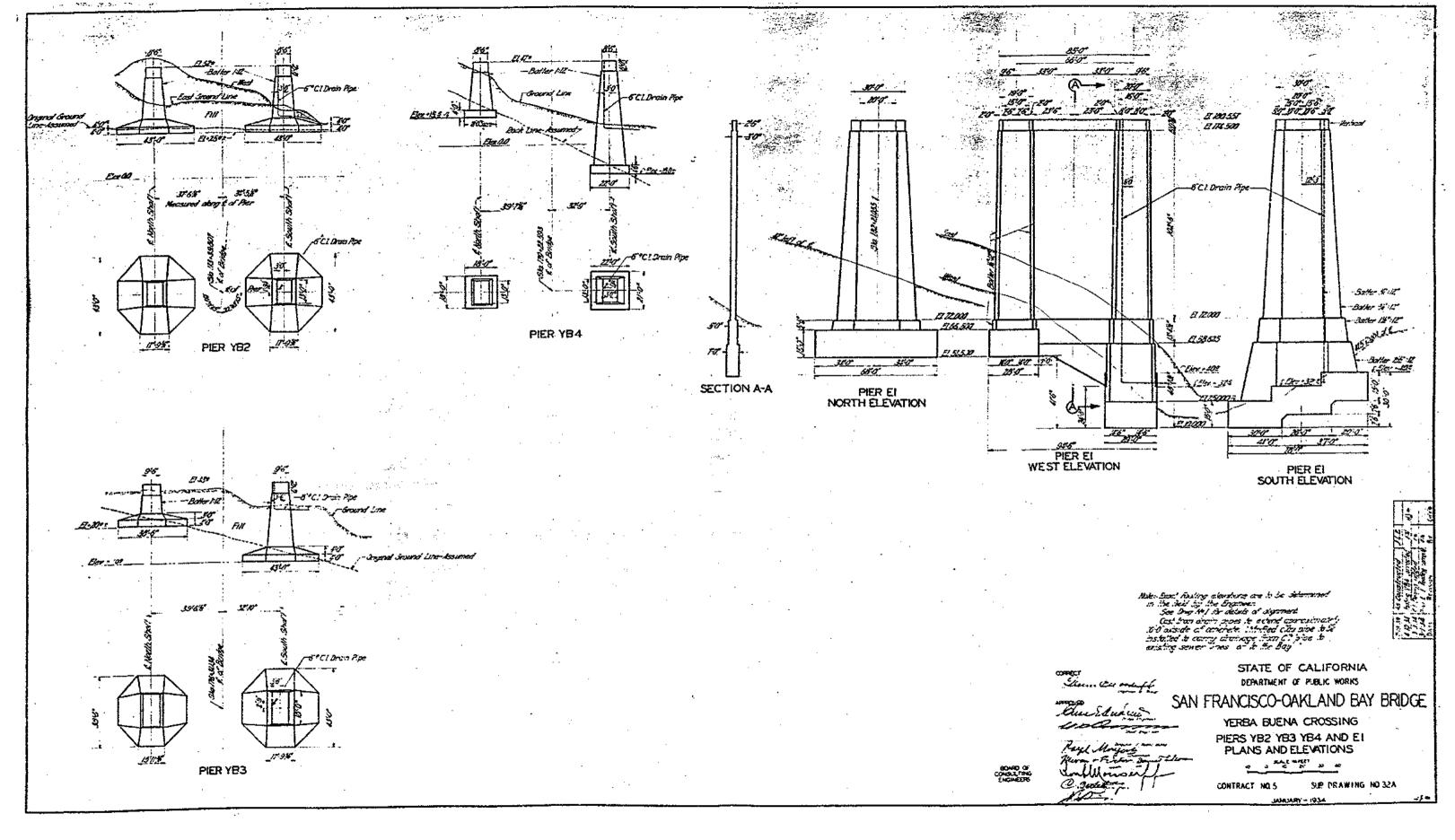


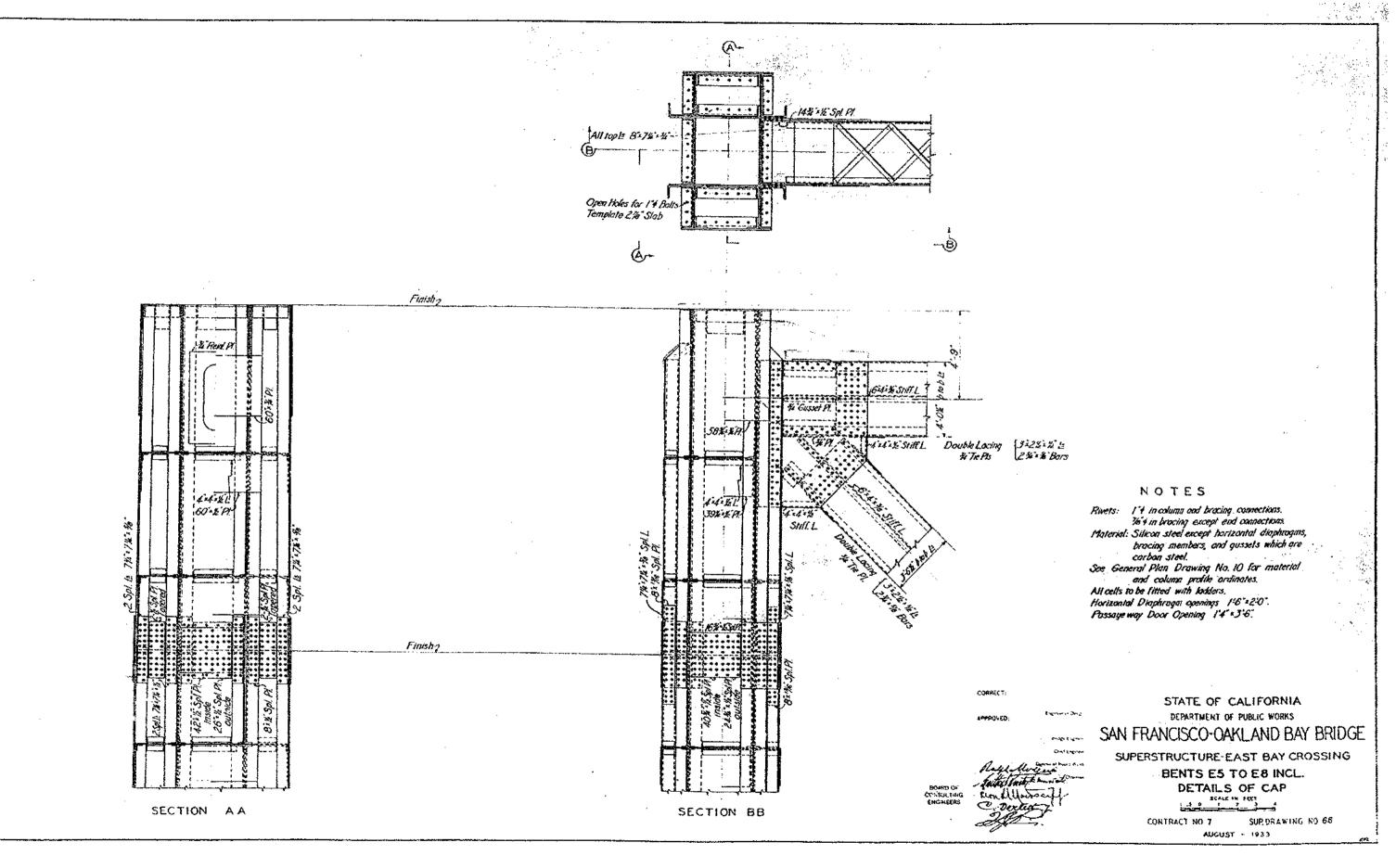


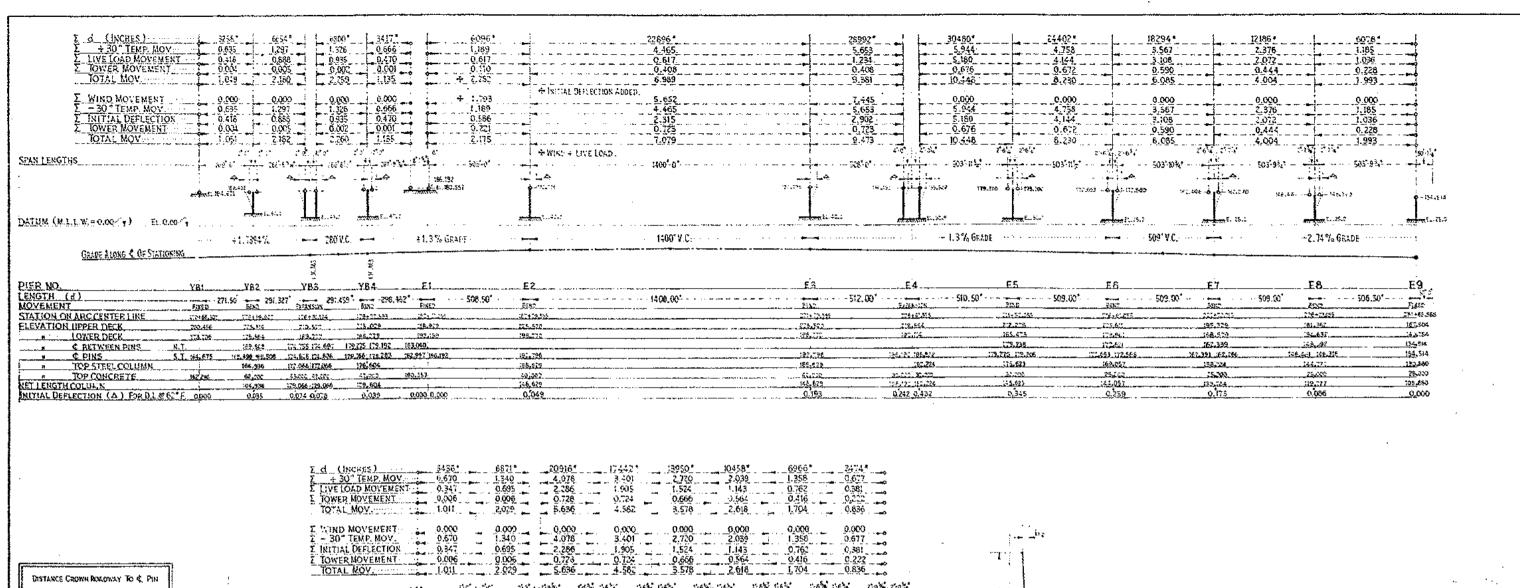


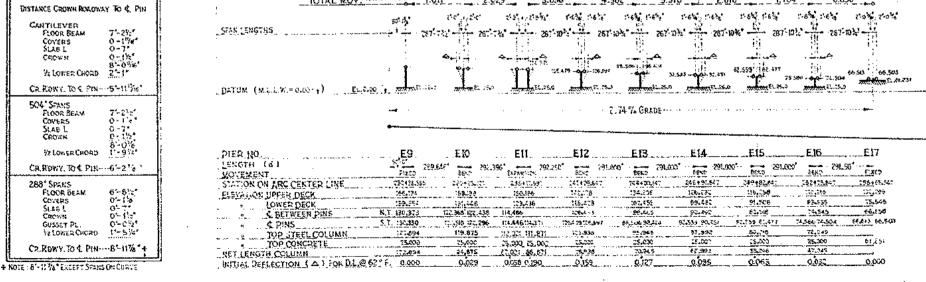


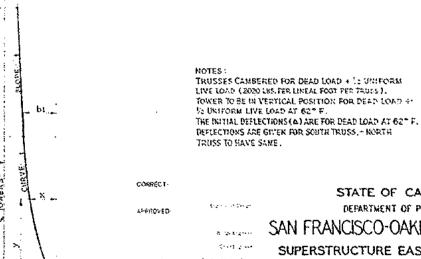












ACKED OF

CONSCIUNG

EQUATION FOR TOWER CURVES

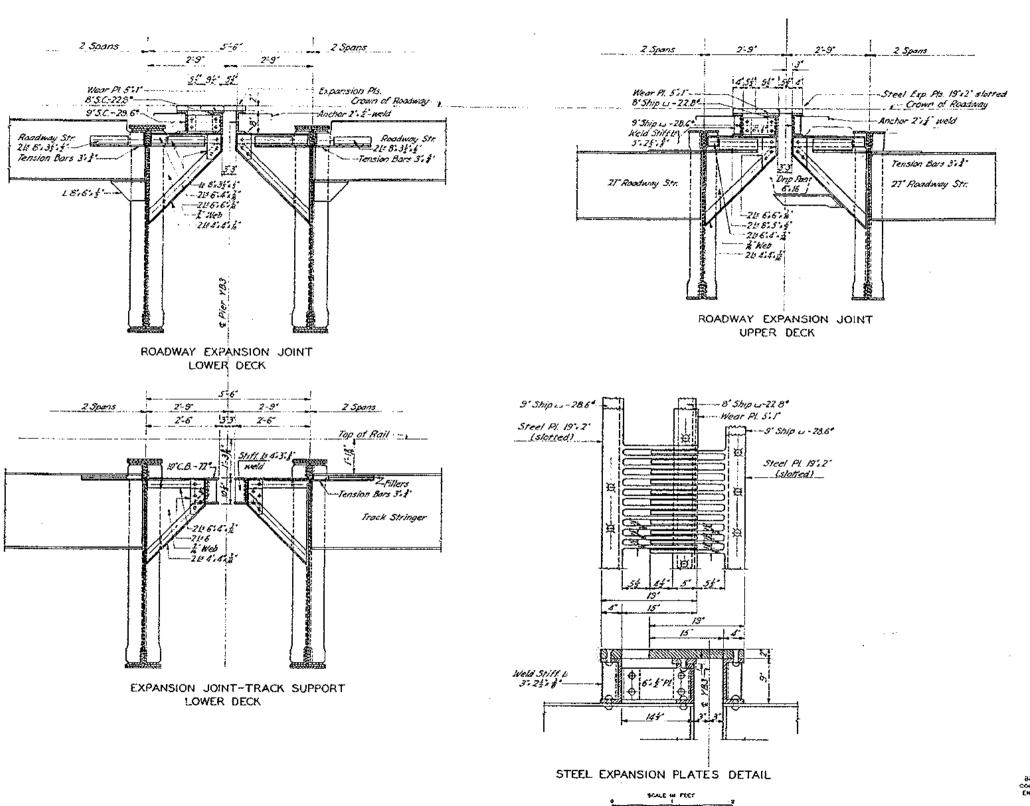
 $X = \frac{b_1^2}{s_1^2 + b_1 - b_2}$

STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS

SAN FRANCISCO-OAKLAND BAY BRIDGE

SUPERSTRUCTURE EAST BAY CROSSING ERECTION DATA - BENTS

> SUP DRAWING NO.84 CONTRACT NO. 7. SEPT. - 1933



CORRECT:

DEPARTMENT OF PUBLIC WORKS SAN FRANCISCO-OAKLAND BAY BRIDGE

SUPERSTRUCTURE - EAST BAY CROSSING

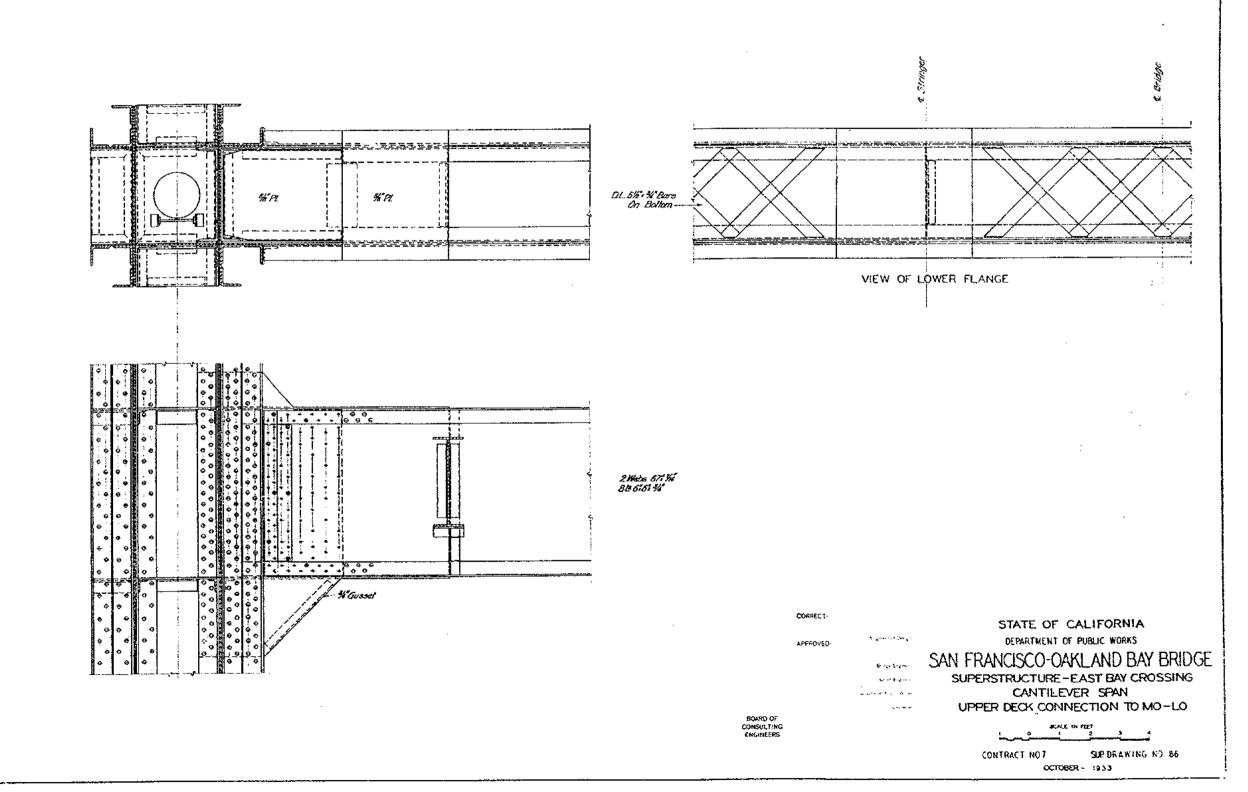
STATE OF CALIFORNIA

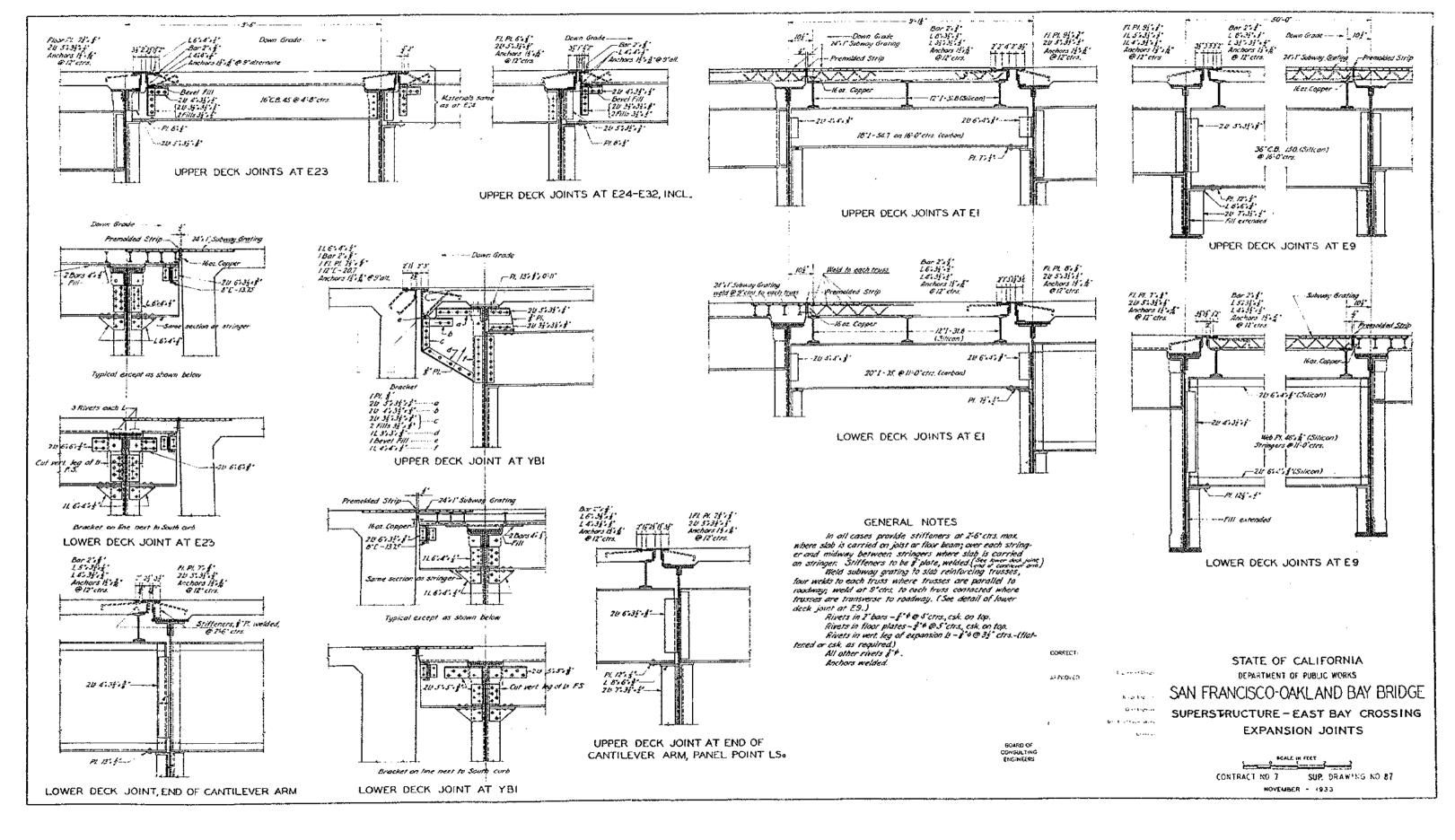
EXPANSION AT YB3 FRAMING FOR UPPER & LOWER DECK

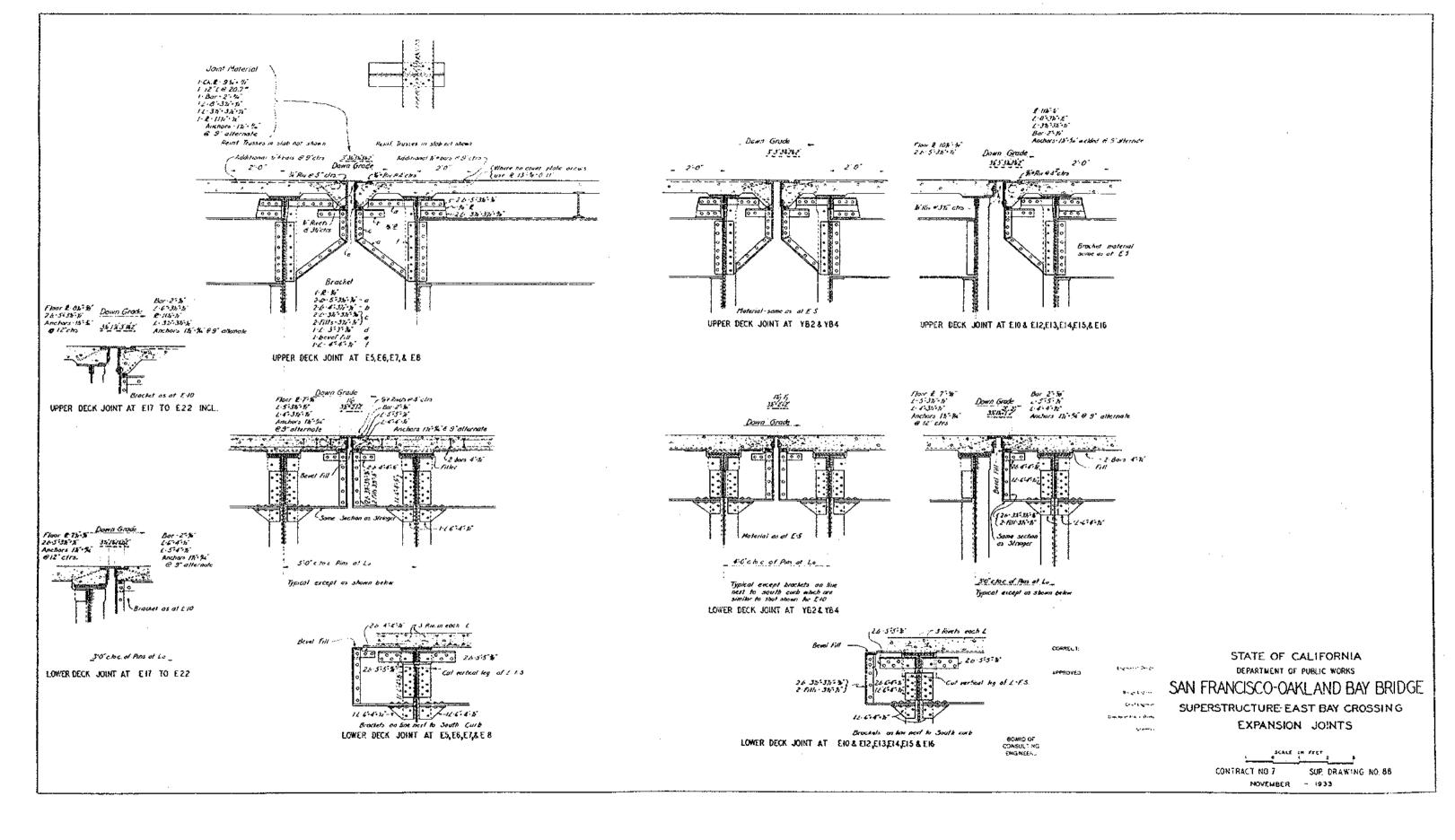
CONTRACT NO 7 SUP DRAWING NO. 85

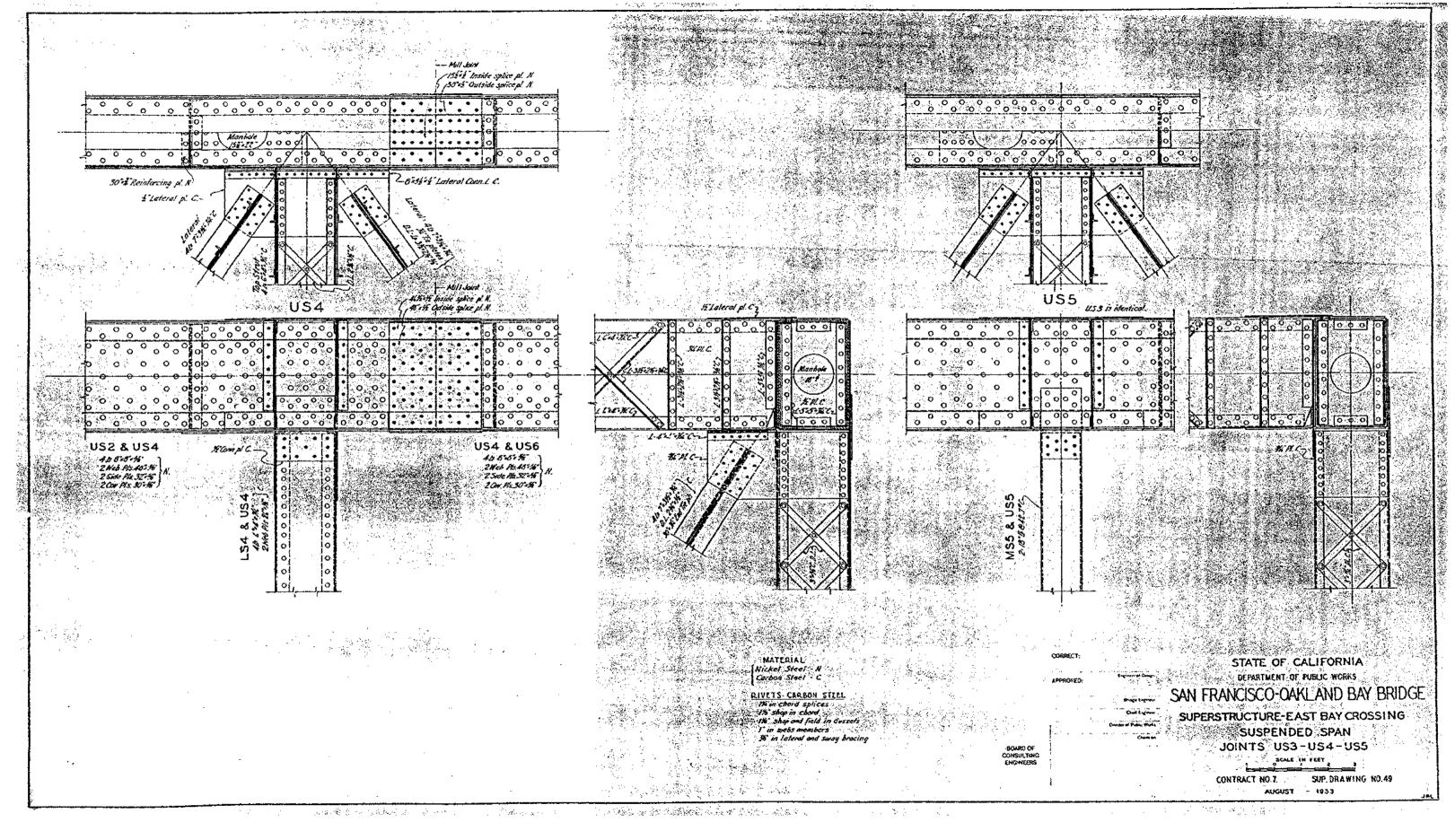
NOVEMBER - 1933

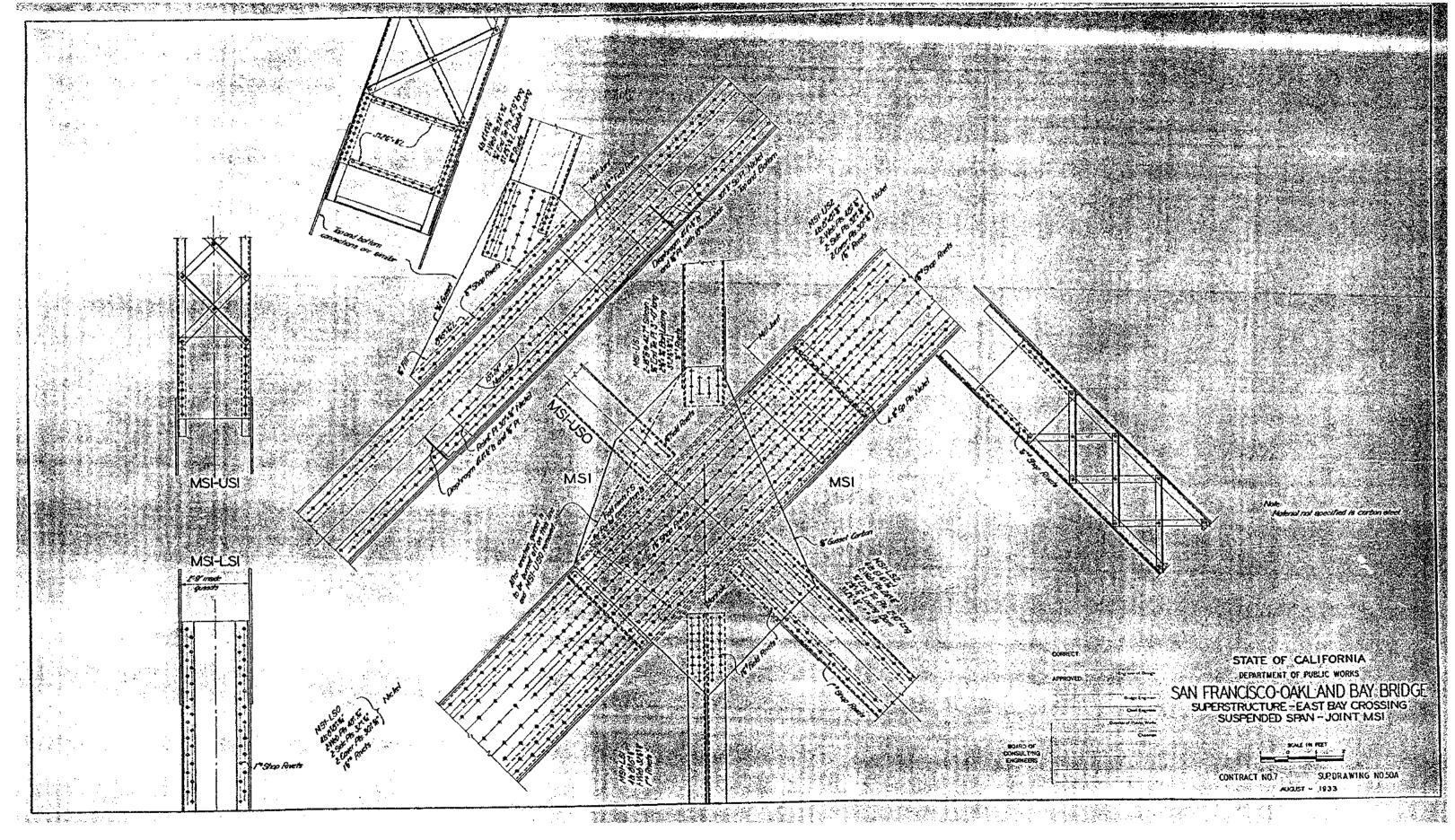
BOARD OF CONSULTING ENGINEERS

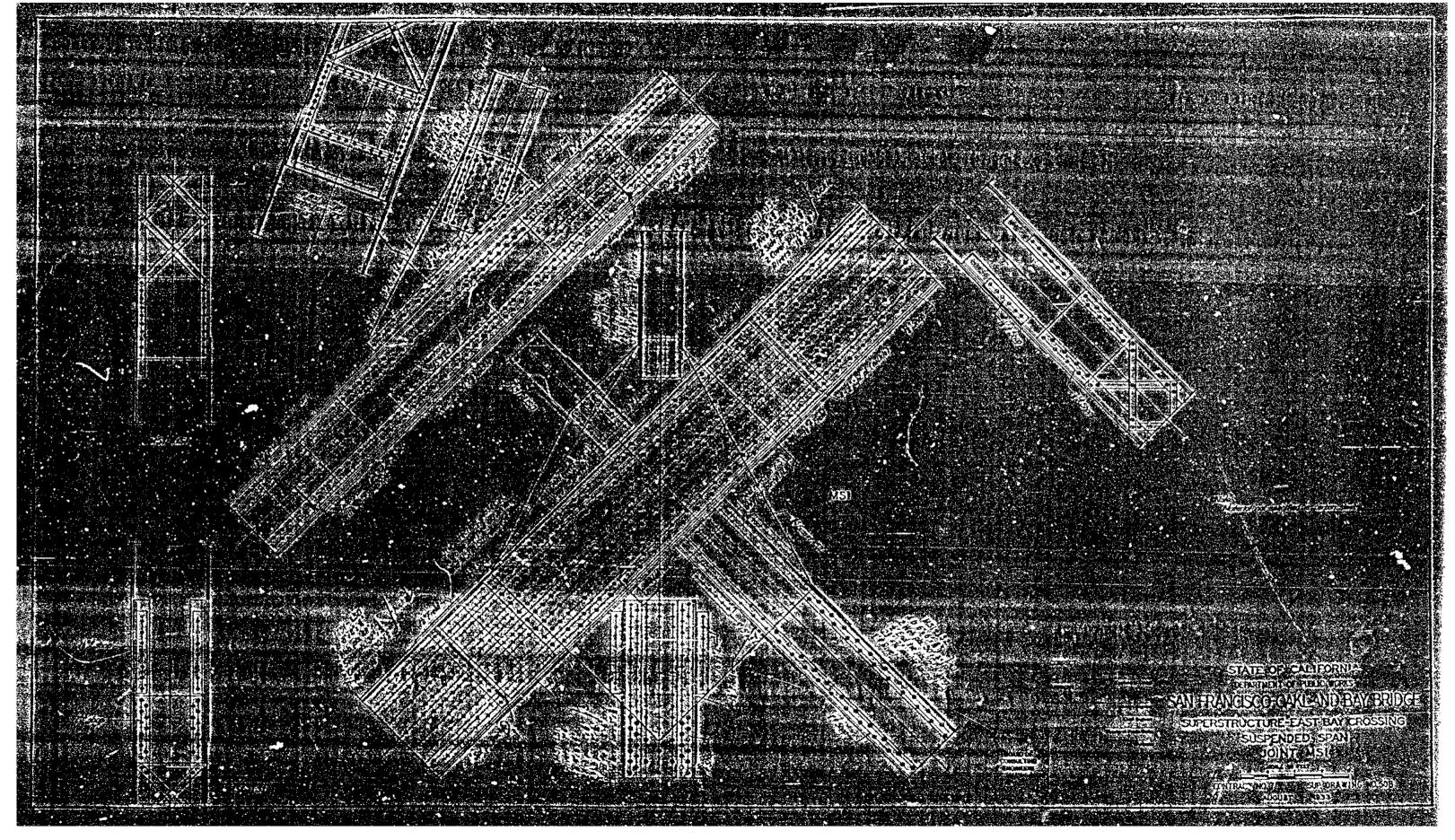


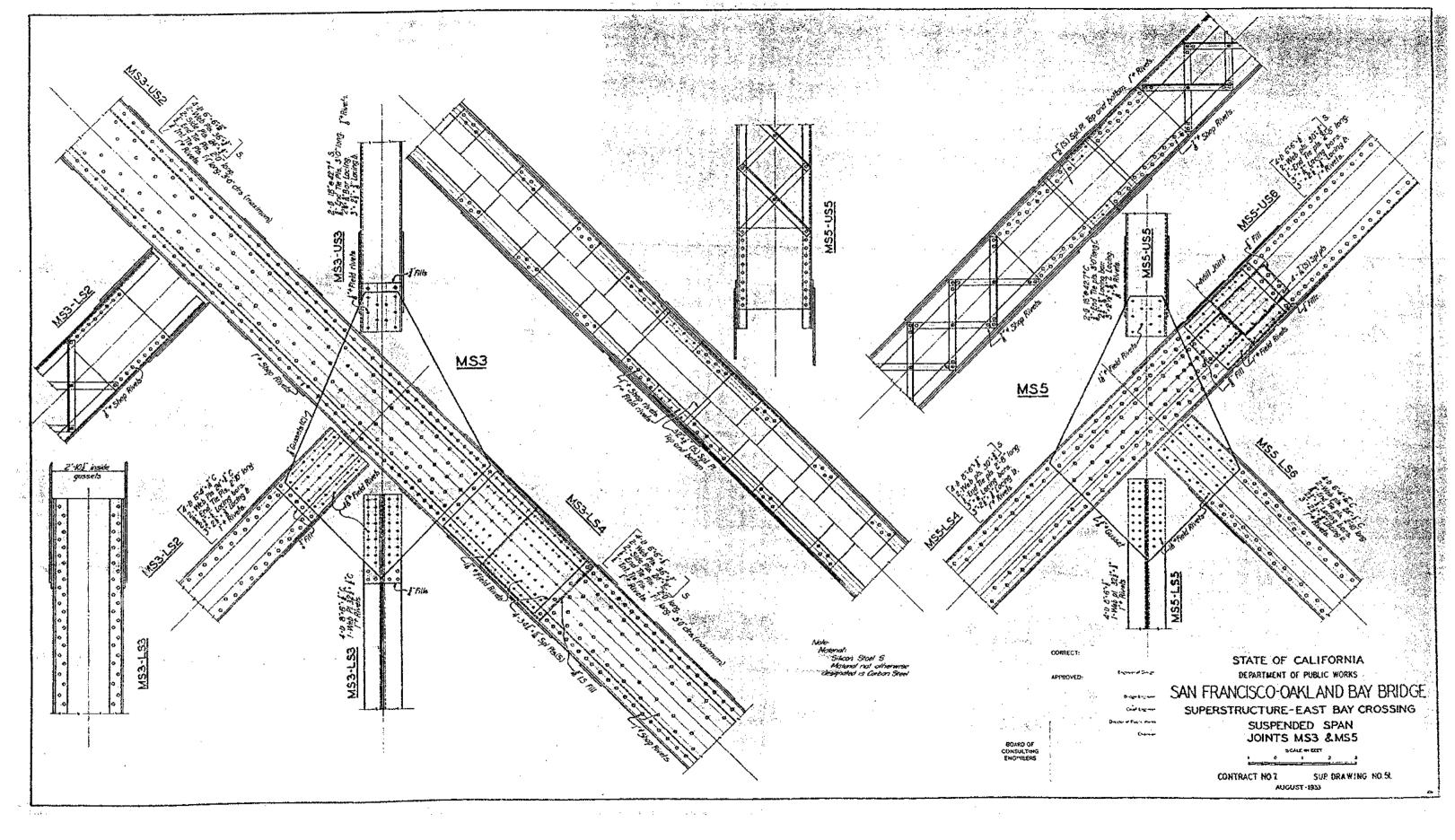


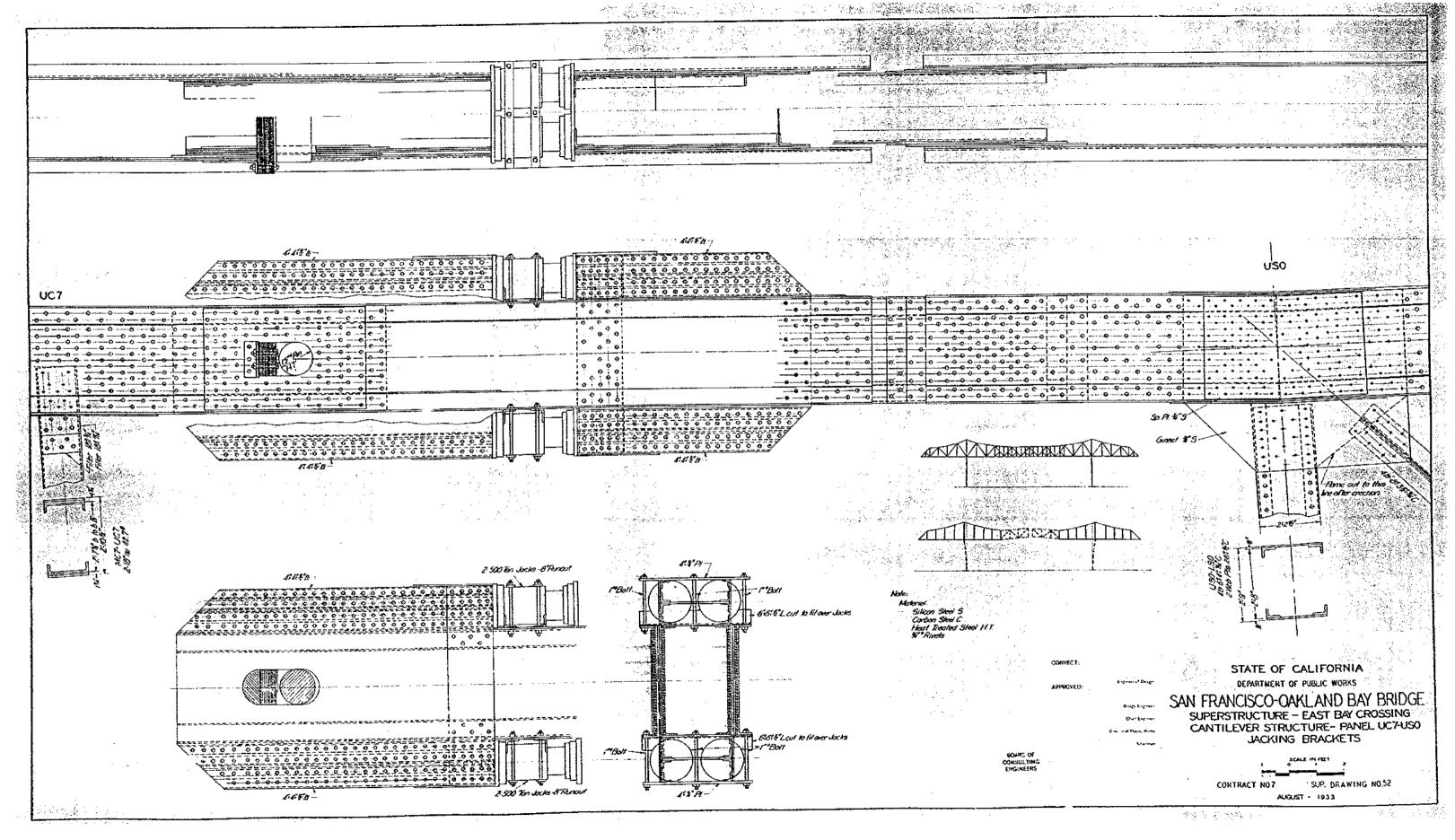


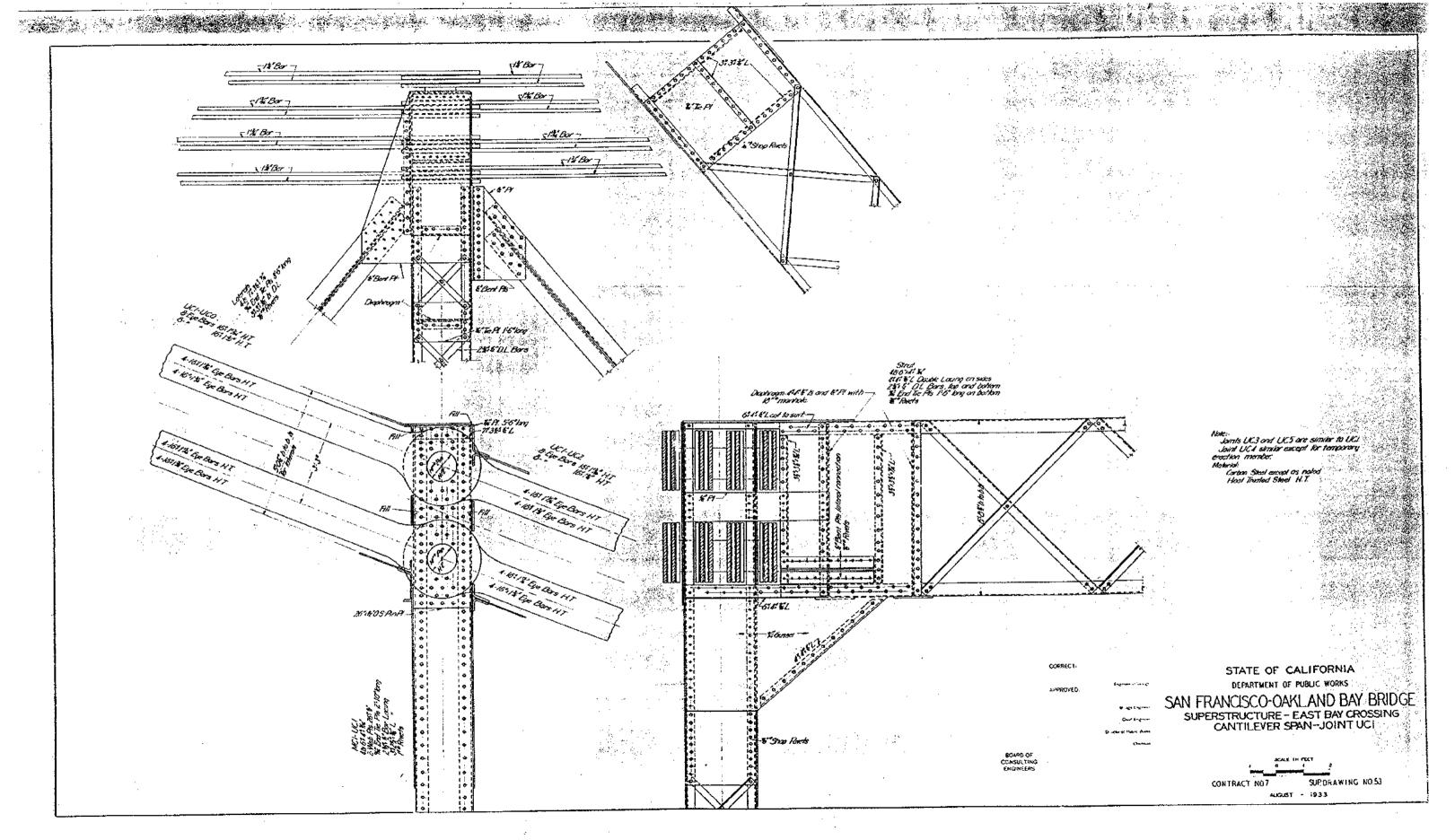


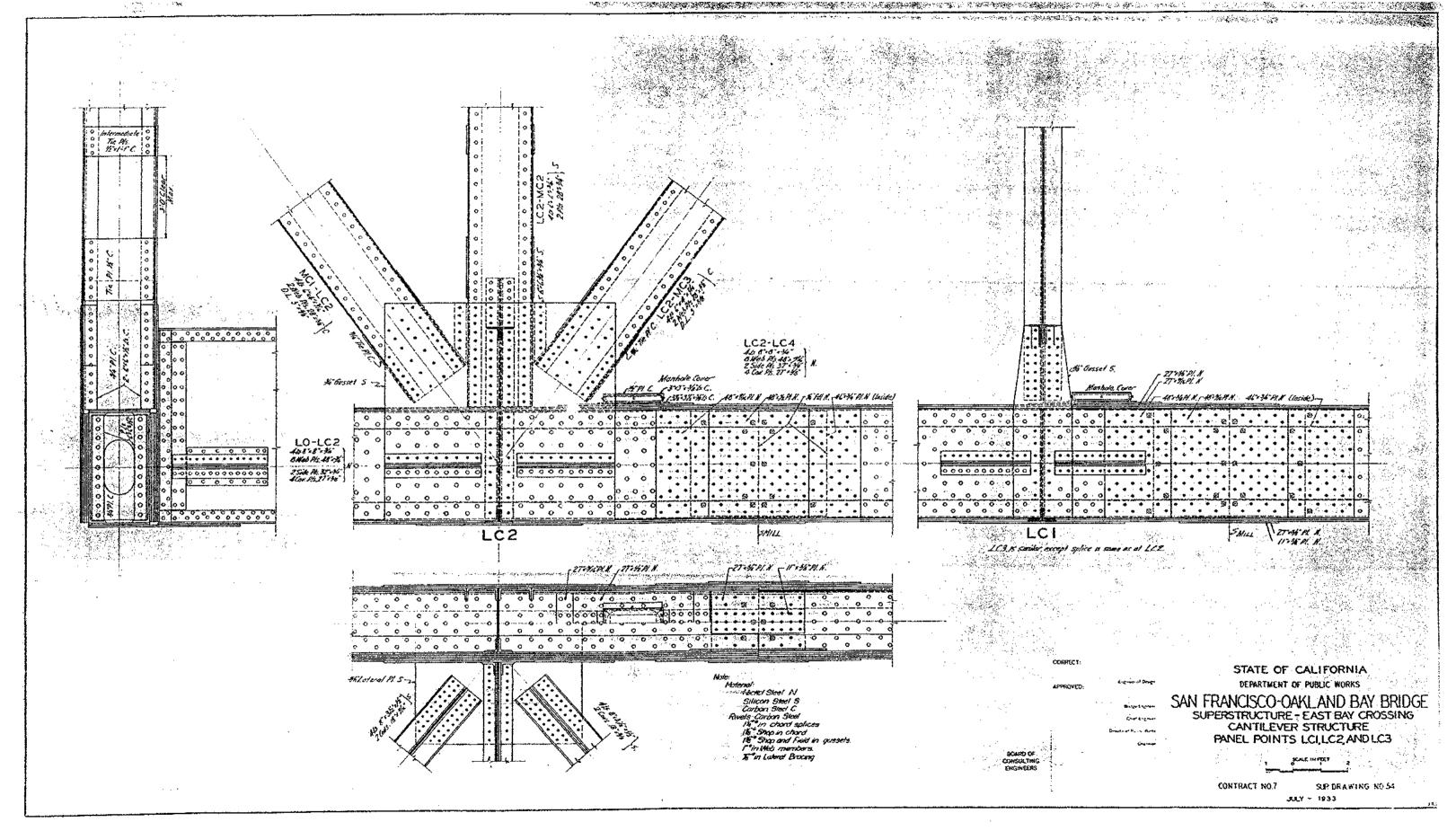


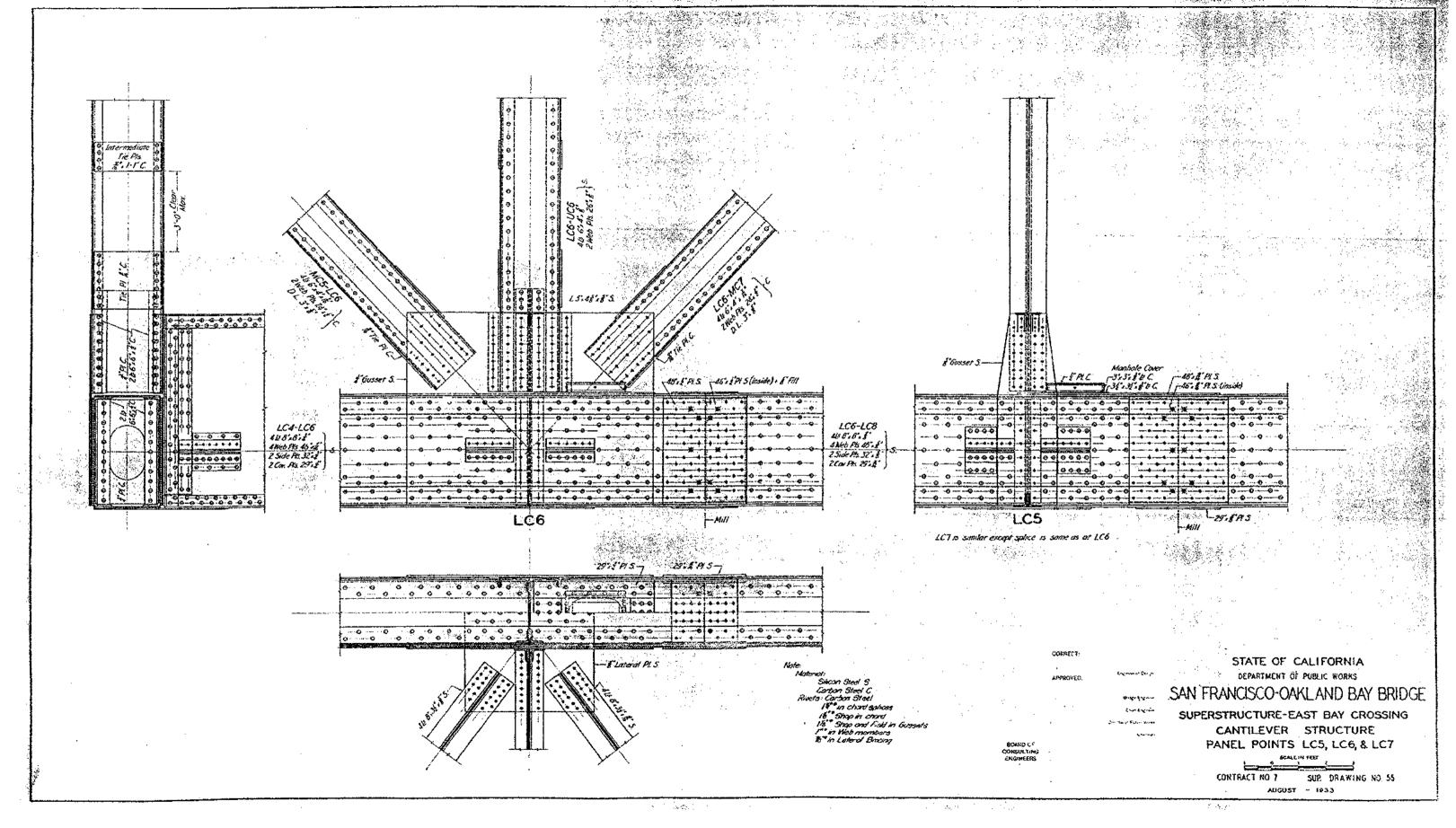


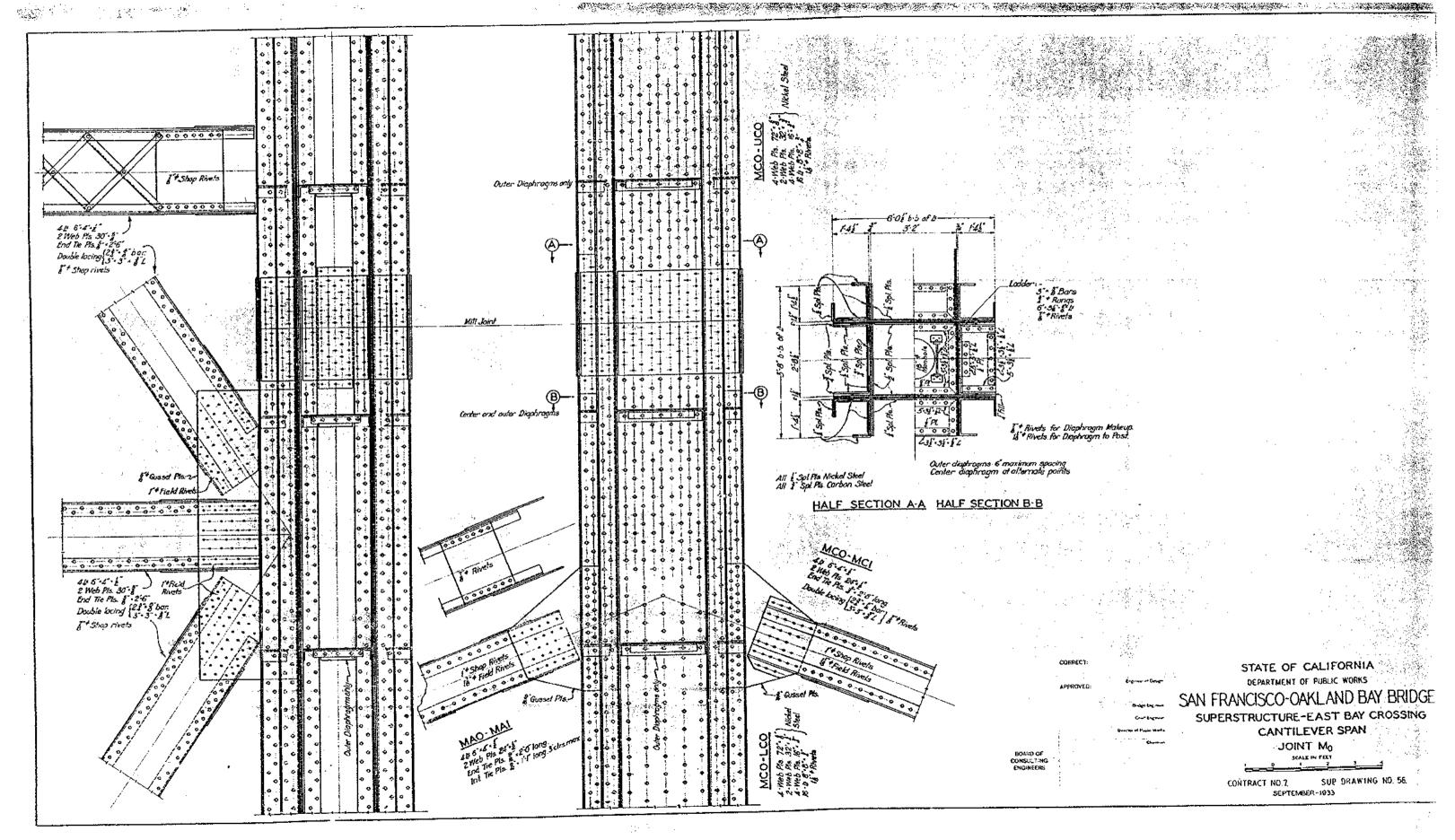


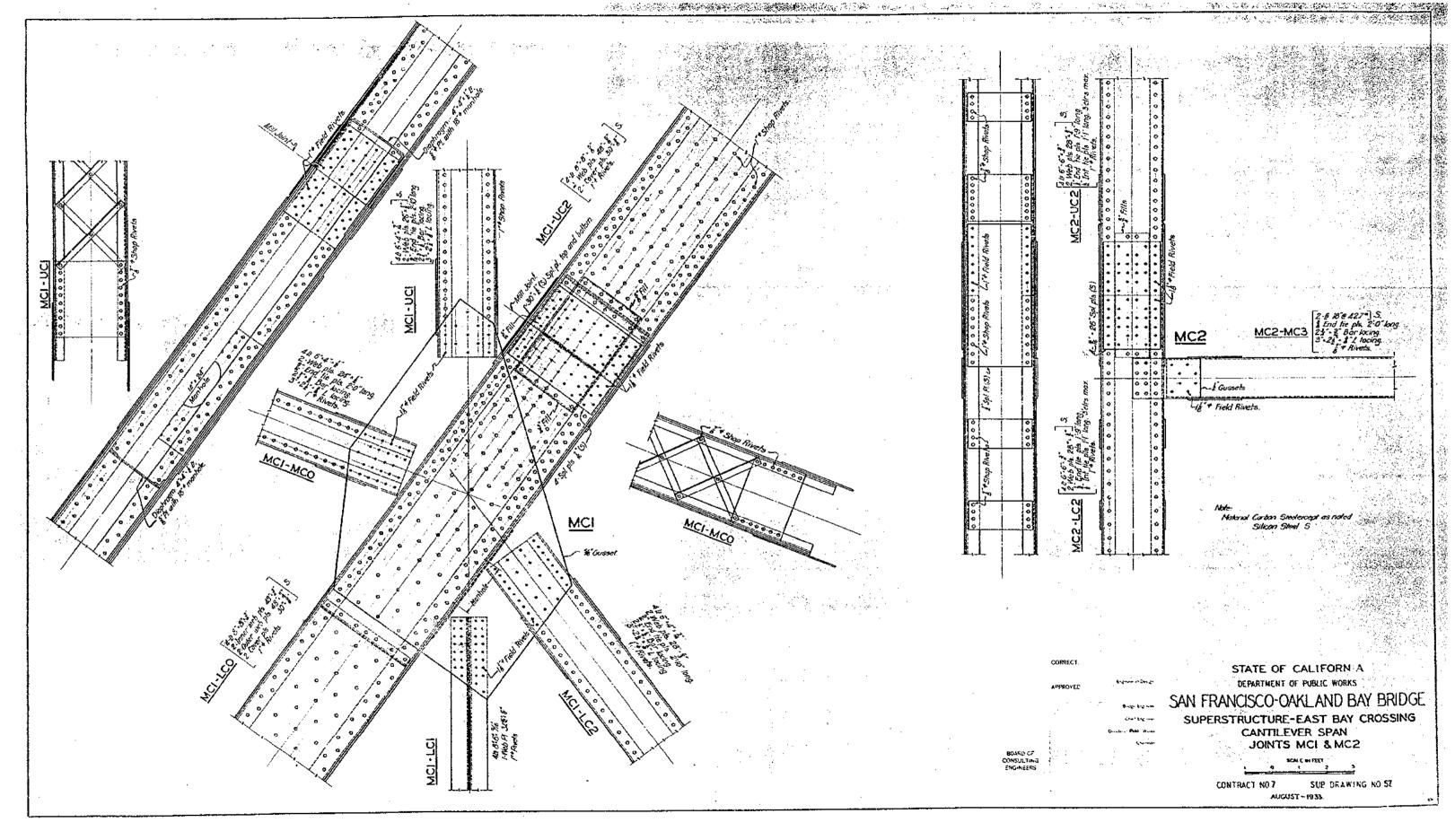


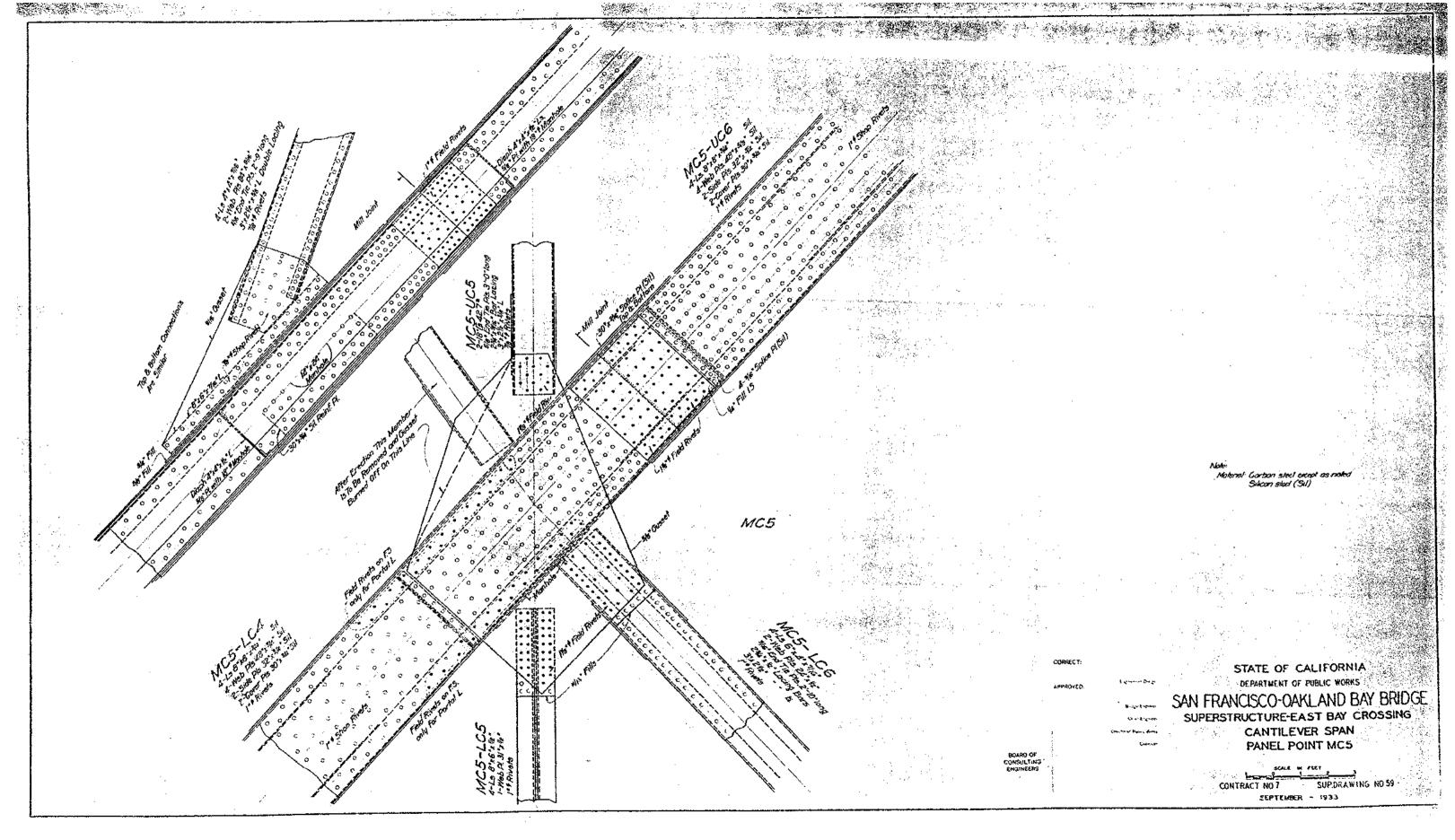


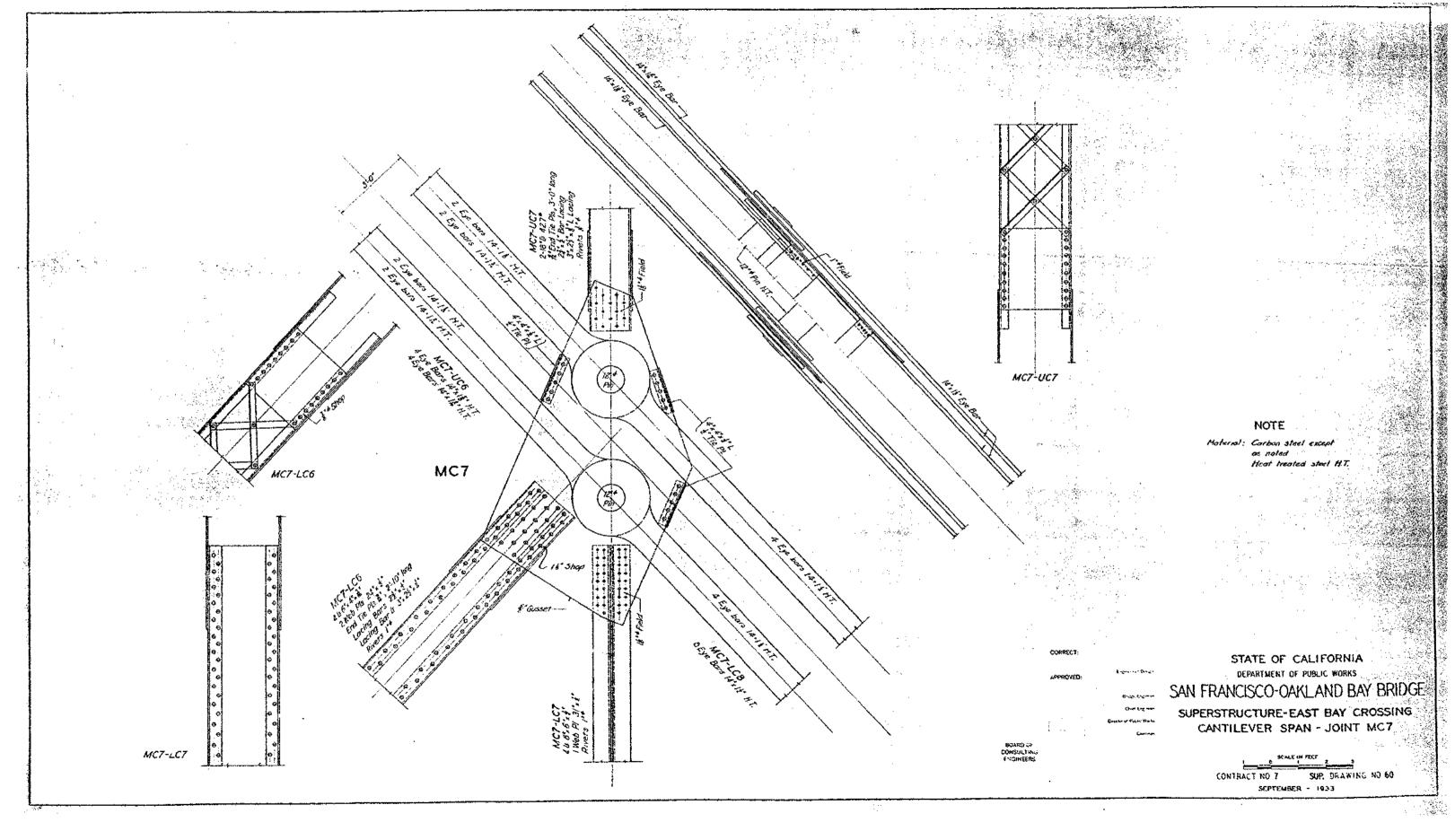


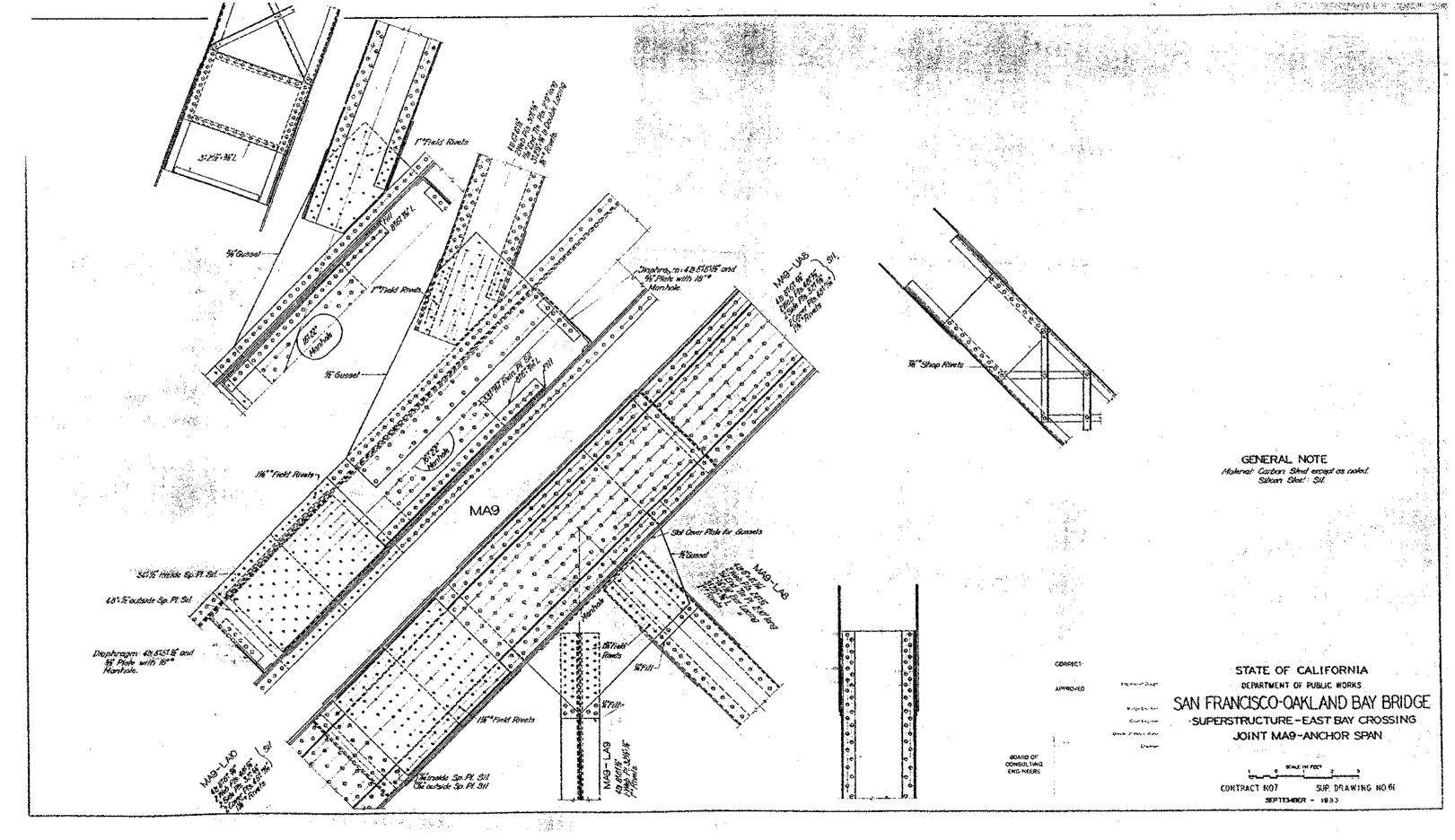


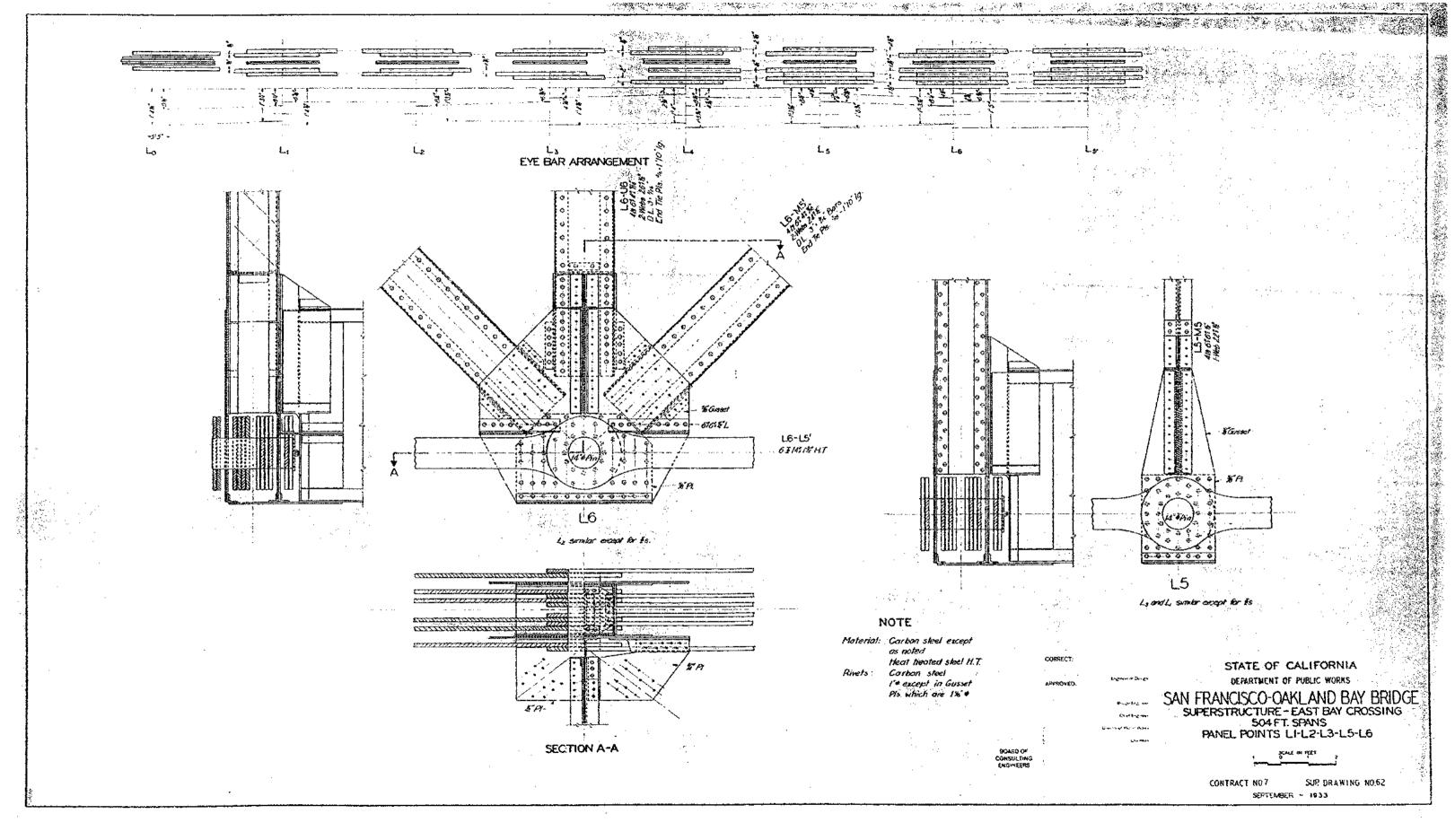


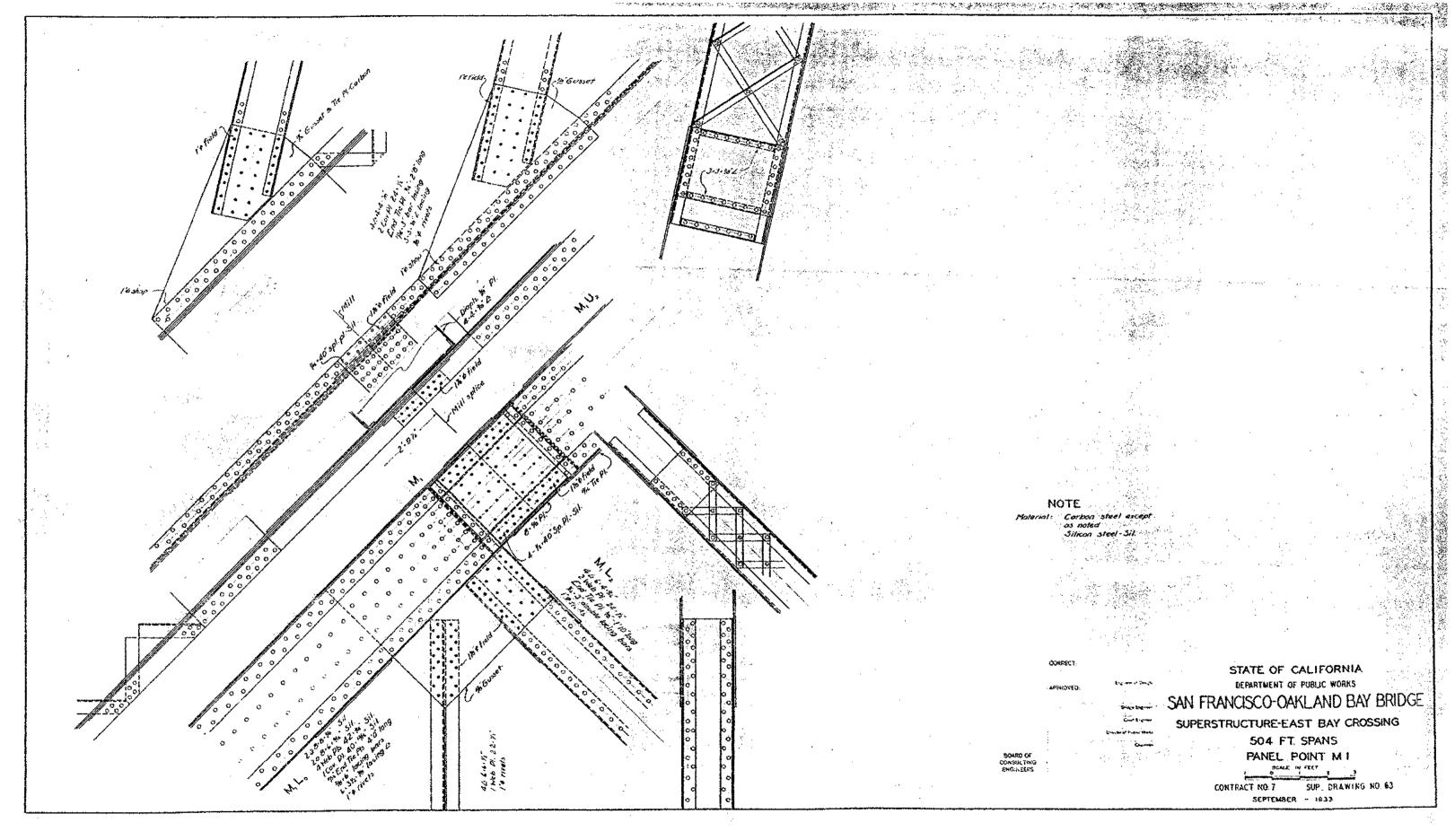


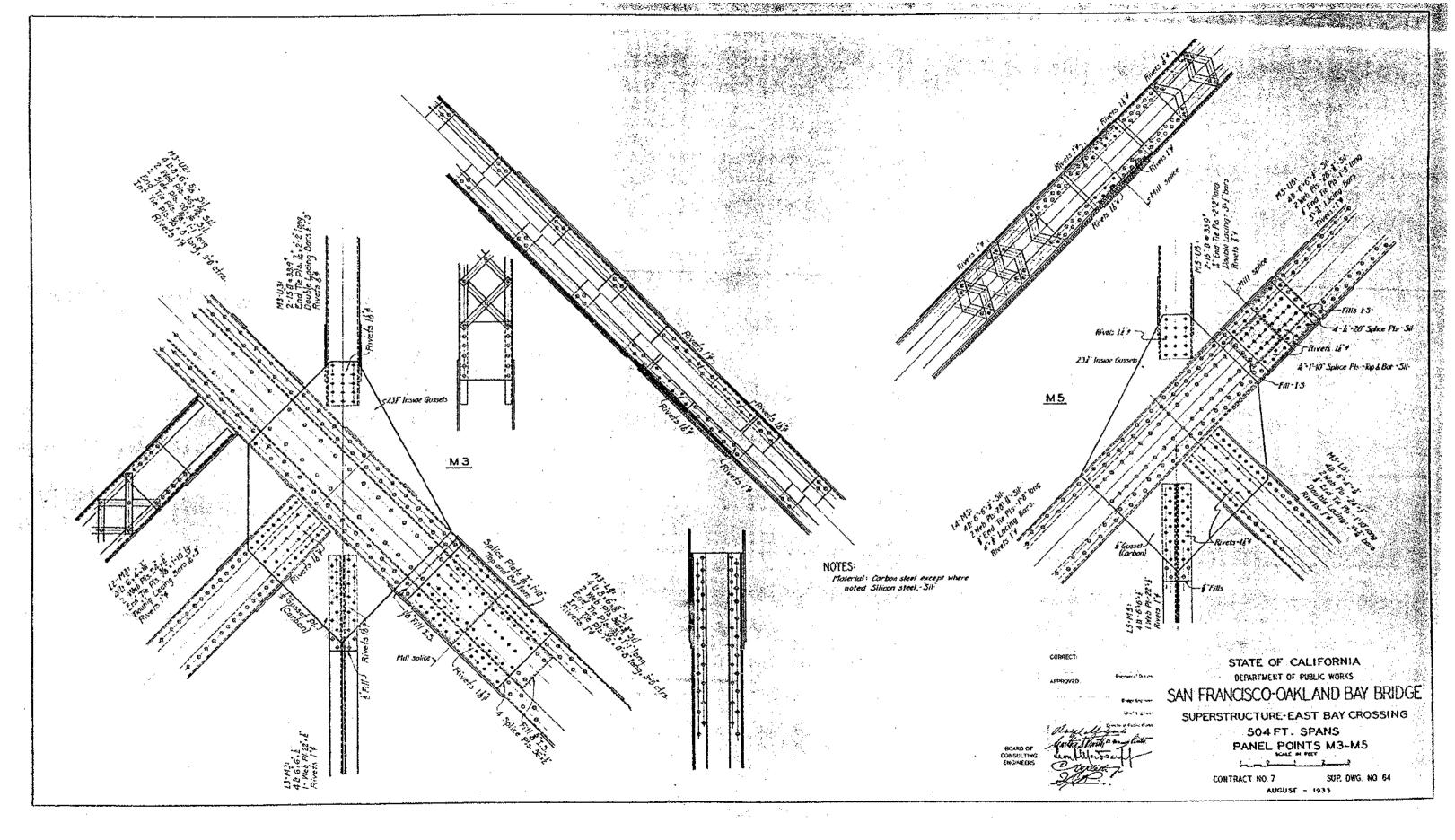


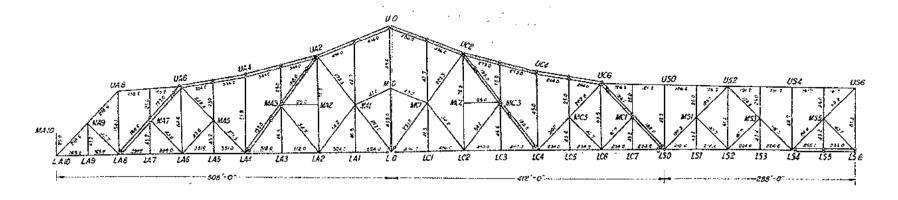












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SENGLE	FT - IAS	INCHES	STR	57R	DL.	4	PIN	ΣA	.57c	STR.	PLI	4	PIN	¥Δ	Av E 4	INCHES	Fr -14
O-141	55'-0'3	660.125	-19293	1350	1166	-0463	00%	-0.501	-5742	-1842	1158	0.485	0.016	-0.439	-0.500	660.625	55 0
AI-CA2	55 -0%	660.125	1025	-1950	11643	0485	I	-0 485	-9742	:8:2	-11584	-2483		-048	-0.484	660.609	55.0
45-143	55 - 6.5	650.125	10326	1350	-11676	0 598	1	-0.495	5777	1842	1160	0.195	[-0.495	-0496	640.621	55-0
A3-L44	55 - 0/E	660125	F 32	19.60	-11676	-0.595	T	0.492	-9777	-1842	-//69	0 495	[0495	0.436	660.621	55-0
14-15	45-0	576.000	4686	-644	5330	-1293]	0253	4426	-879	-5505	0291	F ~	029	0292	576,292	48.0
A5146	45-0	576.000	-2686	- 642	-532	-0293	1	-0293	4425	-879	- 5505	0291	I	-019	-0.292	576.292	48-0
46-L47	48 · C	576,000	-1728	-644	-5372	-4300	1	0.00	-2271	-879	-5350	-0293	T	-0255	-0300	576.300	45-0
LA7-148	48 - 0	576.000	-4728	-644	-5:72	0.00		-0.300	-6475	-879	-5350	0 299		0.29	0300	57€.300	48.0
LAS LAS	45.0	576000	-1845	- 250	-2.55	-0214		-0214	-1726	- 521	2067	aen		0.20	0 212	576.212	48-0
L/9-L/D	48-0	576.000	1845	-250	-2035	-6216	1	2214	1726	-341	- 3067	0.211		0.811	0202	576,212	48-0
UO-UAI -	59 - 3%	7/1.125	+13366	+1630	15050	·072i	100	-0.752	+2674	+2307	14931	-0.717	10.031	0.745	0.50	710.375	59.2
UAL-UAZ	59 - 3/2	711,125	13360	+1690	+/505	+0721	-0031	· 0.252	12674	+2307	14901	-07/7			-0.750	710.375	59-2
W2-W3	57-1%	685.56	+8228		1	•0.519	10031	+0650	-7786	+1497	+9203	+4616		4	-0648		
143 W.L	57-15	685 IS6	8228		-9325	-	+2031		-7726			+066		+0667		684.508	57.0
14-145	45-75	583 312				-0528		-0559	,	-1458		-0525			-1558	582.754	48-6
145-145	49 - 7×	563.312	8029	4		-0525	0.03/			+456		+0.525			-0.558		48-6
146-147	45-0	576.844	.2205	286	+2571			-0305		- 390		-0251		-0.50			48-0
U.7-U.6	48-07	576864	*****			+0293	<u> </u>	·C293		- 390		-0291	10.0		0.292		45-0
0 111	97 - 2	1106.094	-3543			-0675	000		-3361	- 513		-2671	-4016	-0687		1106783	92-2
V21-U42	37 · 2	1106.095				4655	-2016		-2591								+ +
1.2-4.43	92-2 3				-			,	-						0670	1106.764	92-2
/ TALL /		1106.094	.4477 .4021		+5/26	1099	-0.062		- 260	• 733		1.034	0.067			1104.936	32-0
43-144	92 Z Z	1106 094		- 487		1067	+0.00			1665	- iur		+4062		******	1104954	92-0
AL-145	70-0%	849.137		-	-5345	0531	ļ <u>.</u>	-0.535	-449		-2118	-0.529			-0.530	840,967	
445-456	70.0%	8 40437	-4316		-4869	-0541	-2016		2005	-755	क्रम	-0539	0016	0.55		640.993	
146- 4 47	20-02		+ - 222	570	+4792	-0767	-0062	10.505	3753		12771	4743	0.062	0325	-0.507	839,630	69-11
UT-148	70.0%	540 257			-	6730	5031	-076!	-3548		+4339	•C726	10001	-0757		839678	69-11
K8-K49	68-12	817906	+2960	. 407		-G42Z		-6472	2.56	555		40 GO		-2.421	10421	817.485	68-1
149 (40)	68-12 ₄	617.906	+263/	+357	+2995	-03.5		10375	366	+467	2973	-0373		0.375	· a 574	817.532	68 -17
1.2-LA2	147-11	1775.000	1332	· Æ 3	. 14%	-1007		1.06	+1262	+222	1486	1.601		+1.001	.1.064	1773 996	147-10
140 LA4	112-4	#CE 000	-800	+126	- 926	<i>+0.726</i>	4026	10.42	- 748	• 172	-520	-07/5	100	0.73	-0757	:407.265	117-3
46-146	102-0	1224 000	-1023	+162	+1485	-0396		·¢396	955	194	1179	0.354		03%	-0355	1223.605	101-11.
148 149	94-55	:16: 375	-2247	27	-25/3	-0183		4453	-2:35	370	2505	2580		0.550	2582	161 957	96.9
VAI-LAT	23-11/2	667,500	+513	+ 153	+666	6430	} - '	-0410	+475	+ 16!	• 640	42.155		0355	-0.366	857.112	23 - 15,
/43 £43	73-112	557.500	-517	153	-670	-0352	1	• C 393	• 25 3	+ 161	+644	-0.377		10 377	.0304	657.116	73-16
245-145	51-0	6:2 500	-404		-535			-0254	- 375	+ 43	- 515	-28/5		-02/5	-0250	611.750	50-11
147-147	51-0		1401	. :32		0253		6.25	3.2	-:43		ر 22 ت			-0248		50 H
45 (49	46-4	550 ± 7		. :34		-1179	- 1	-5229		1	+ - 1	6220	1		074	550 463	44
1.021	96.0		169		1	069	A tour		169				one			1152 107	96-C
2 10	58-5	75E 200	- 11 ±	1 %	- 13		-0.3K	-0065	- //3	o					CO19		56 B
45 4:15	50-8		-106	0				0.35		- 5	105		-CCIE			704065	53 B
42.7.427	43.4.2	550687	- 58		• •			C Ses		0	+ '-	0005	25.64			550732	45.4
AINAZ				0	- 55	-0.645			- 55		- 58		·		0045		
	92.2 1	1105092		- 55		0739		-6 ZDS		- 69	-556	0235				1106.332	92.2
43 £4Z	52. Z			- 55		-034-	100	-2 560	-236	- 69	-503	0307	-0016	2,356		1106 455	92-2
45-246	70.0%	ECS_137	-425	- 49		- 557.7		0507	-25	- 67	~470	-0306	أمما		-33%	\$60743	70.0
47-LA6	70.0%	845437	3.3	- 49		-6245			- 5-2	- 67		G 266	-oore	0.787		840.718	70-02
29.28	60 - 6	017.506	-330	- 50		-6255		C.255	-340	- 68	378	0.753	اا		-0254	818 160	65.2
10-10		1152 000	£210	-1258				-6.5J?			11416	-2687	0016			1152.905	35-0
10-10	9€.€		-10644	1275		€326	0.00	-094			11867	-0522	0.016	0530	0940	152540	36.07
10-10:	55 3	7/1.125	. 0	. 0	_0	. !			5	0	0		ļ .i			711 125	59-3
23 1242	55 0 4	660.25	٥	_0	0		.		0	0	. 0]		660125	55.03
49.40	30.0	3£0.000	-140	- 28	- 168	-0361	1	-cani	-140	- 28	- 163	-0081	'	0001	0081	160.081	30-0

			,					_EV			RM			<u></u>			
ļ	LENG	TH			TH	TRUS	s		ļ.,,,,			TRUS	5			FABRIC	LENGY
MENBER	FzIns.	INCHES	DL. STR Krey	515	264	Δ	PiN	ΣΔ	STR	ELL S.R	265	۵	PIN	ΣΔ	ÁÝ ŽA	INCHES	Fz-In
10-111	55-074	660062	-9929		11222	-2495	0.016	-054	-9400	-7.65	-11165	-0495	-006	2511	-0 5/2	660 574	55:0
101-102	55-0%	660.062	-9929	-1293	/1222	0.492	<u> </u>	4495	9400	1765	-11/65	6205		-0.495	24%	660558	55 0
(6-10)	55-0%	550.062	9971	1295	1186	0.523	ļ	-0.523	9450	1765	125	0.521		0.521	0.522	660594	55-0
£3-1.64	55 0%	660 062	9911	1293	11264	1053	L	-0.529	945)	-1765	-11215	0.521	L:	0.52	0522	660582	55-0
CA-1C5	48-0	576,000	3220	- 453		0.255		0233	-304	- 592	-3617	-0297		-0.297	-0255	576.2 3 8	46.0
(5-166	48-0	576000	-3220	433	.5657	C299		0299	3045	-592	3617	0.297		0297	4295	576,298	48-0
C6-LC7	48-0	576000	3260	433	7693	0.30		0,902	3000	- 592	- 3672	0300		2300	0.301	576301	48-0
C7-LC8	48-0	576,000	3260	-433	-3693	-0,902	000	03/8	-3060	592	-3672	0.300	-0.016	Q316	-03/7	576.317	45-0
UO-UCI	59-6 m	7/2.469	•13346	-,685	19036	-0721	-0031	+0752	-1250	2505	+/493	2719	-001	-0750	-2151	711 . 718	59.3
KI-IK2	59 -4 %z	7/2.031	·/334	+1695	12000	+6721	-0031	4752	1267	+2305	1198	47/5	-0031	·0750	+675!	711.280	59 - 3
VC2-UC3	57-2 he	686.437	7227	• 955	82V6	-0688	-0.031	-27/9	6900	1309	+8209	12685	+0.031	-076	-0718	685719	57-15
ICHK4	57-2/m	686.062	2217	453	13266	466	-40%	-2719	-6300	+1305	£209	-0695	+003/	•0.716	2718	685.342	37-12
KA-UKS	46-83	584.812	- 7/2/	•938	+805	+0.500	+0.031	+0619	-6730	+120!	+aari	10580	+20:/	+0415	+267	584195	48-8
/C5-UC6	45.8 4	584625	7121	938	+5059	-0500	-0051	-0.609	6730	·1281	601	+0.54	-0031	-0615	05/7	500.008	42-8
JC6-UC7	45.2	578.000	0	0	0	0.000	0	ō	0	0	0	0	0	0	a	578 000	18-2
	48-E	578,000	0	0	0	0000	Ī.	0000	0	0	1 3	-	C00C	0,000	0	578.000	
0-MC7		1105625	-2/73	-465	26.1	0704	006		_		-5614	-0700	-0016	-07/6	cns	1107.343	
KI-UC2	92.5 2	1109 750	- 3666			0707		_	-3400		•	2696				1110 265	
		1109.750										1036				1108 588	
4C3-1C4		1106.675		+618				+1.467				1093				1105.461	92 1
C4-KC5	70 / 74			-721		-0546	-		-5770		+T	0543			0524	841.981	20.12
VC5-VC6	20	643094	5.53	- 672		0549	anic					0557	_		*****	843.658	70-3
K6.KC7	70-3/2		5/17	+ 682		-0530						4.5	_	-	-	842 204	70-2
K748	70-174			+ 633		280			-							840.579	
VCHU2				- 51		+'-	40031	$\overline{}$	_								70-0
			- 519		•	C 300		0.568		- 65	× 567					110762	92-3
	92 23	APPENDING HA	-227	- 58		0349	-006		-426	- 7/	- 297					1106.980	
165-166	70 - 15%	861.437	-410	- 49		0299		0299		-67	-457	0.298				841.735	70-17
C6-MC7	70-194	841.437		- 29		0229		1295	336	- 67	-405				*****	841.731	70-15
KHKI		1153 125	157	. 0		AL IS			· 157	0	157					1153.260	96-1
K3K3	33 0 24	208 687		_0	-103	000		C064	103	0.	- 103	-000			0054	108 751	59-0
- + +		1415 000	-672			-0724		-0740	+632	-#1		0.722		D: 4 41		1414.261	117-10
C5 HC5	59-0-		- 69	0	- 89	-0012	205	-2050	89	0	- 89	2002	2016	0058	-050	708,120	59 - 0
KE-116	102-4	1226.00	• 952	-142	11/24	-3612		2652.	924	+ 156	+ I120	6.50		-0630	4657	1227.369	102-3
C2 (C2	148-3	1779000	1346	+ 165	1511	-1021		1027.	4207	+222	1603	+1.615	٠	·NOE	+1C21	1777.579	148-15
C7-14C7	45.5	\$81,187	- 25		- 45	-0935		-6035	- 35	. 0	- 45	-2035		-0.035	-2535	561.222	48-5
crici	73-11%	507 506	5.0	-152	-662	-0.42		£42!	476	-152	633	-04-6		12436	44.5	£57,492	73-77
123-163	73-117	£57.536	.5%	:52	+652	20:5		-6415	+465	+162	+627	C399		2395	.0407	657499	73-11
C51C5	5: - 5				-52!	×626		-0.26	*****	+144	502		· · · - <u>- </u>	0.237	·** - 1 / **	612.915	51-0-
K7-4C7	51.1 32	613 156			+532	-6252		0252	.369	-166		-22/3	~~~	0243	16268	612.903	51-0
10 HC1	59 3 %		c	0	0	0,000		000		0	5	GOOC	<u>-</u>		000	7/1.906	59.5
·					• -												
102-403	55-03-	660969	0	0	0	0000		0000	0	0	0	0.000		0.000	3000	660.969	55.07

GENERAL NOTES

The average deformation for the two trusses was used in calculating the comberned the members.

Comberned lengths were computed for Dead Load plus one-half Live Load stresses. (#11.*2020 this per lineal fit on the south truss and 1480 this per lineal fit on the north truss).

Modulus of elasticity of 29.000.000"/b" was used for the Eye-bors and 30.000.000"/b" for the built up members.

Sub hangers are comberned for Dead Load plus one-half floor-beam Live Load reaction.

FLOOR-BLAM LIVE LOAD REACTIONS

48 Fz	PANEL	
North Truss	South	Truss
55 <u>214</u> 269	.55 <u>.232</u> 287	Upper Dec Lower Dec Yotel
5 <u>5 A</u> 63 <u>244</u> 307	65 260 323	Upper Dec Lawer Dec Total

					5	เบร	PEI	NDE	D:	SPA	N						
	LENG	TH		Non	27H	TRUS	\$		<u> </u>	50	UTH	TRU	ss		Av	FABRIC I	EMSTH
Nember	FT - Ins.	INCHES	D. L. STA. RIPS	i L.L STR KIPS	Pit	Д	Aĸ.	ZΔ	DL STA MAS	MIL. STR KIPS	04.	4	PIN	ΣΔ	£3	/AICH/ES	FT-INS
150-151	48'-0	576 000	-25.49	-390	3239	-0.294		-0.283	-2689	+533	1,1222	-0263		×0.285	-0284	575.716	47'11"
L51-(52	48-0	\$76,000			13239	0.280		-0 284	-2659		-3222	·0.253		-0 223	-0.254	\$75.716	47-114
1,12-153	49 - 0	576,000	+2840	+590	• 3230	•0276		-0276	2630	•533	-32/3	0275	ĺ.	10275	·0276	575.724	\$7-1!
153-154	49 0		-2820		+5230	02.6		-0276	2630	-533	-32/3	+0.275		0 275	+0.276	575.724	45 11
<u> </u>	48-0	576.000	·4861	675	+555€	•0633	0001	-0464	· 4604	+921	-5525	-0430	-0031	·0.46/	+0.462	575.538	47-11
455-456	48-C	576.000	-4881	•675	+5558	·Q £33	-003:	0.454	·404	+921	-5525	10430	-0031	-4-6	+1457	575.539	47-11
USO USI	48 - 1/21	577.031	0	0	0	0000		0	0	. 0	Ø	6000		G000	0.000	577.03/	18-17
USI-US2	48-1/11	\$77.031	0	0	0	0.000		0	0	0	0	0.000		0000	0 000	577.031	18.1%
	49 - 1752		4123	-560	4697	-0.39		-0.461	3590	-776	-4656	-0458		0.450	-0.450	577.491	J8-17
US3-USA	46-1/50		4/23	-568	-4691	-0.46/		0.461	3590	-776	4000			0.49	-0.460	577.491	45.7
USB-USS	28-1/32		4123	-568	-4691	446/		0.451	-3000	-776	4666	0.48		-0.458	0.460	577 491	48-17
U <u>S5-US</u> 6	48-1'35	577.031	-4123	-568	-4691	-2461		0.461	300	776	4666	2458		0450	0450	577.49	15 1/2
:50 -1 251	67 - 11 14	815.656	-4028	-553	-4581	-8631		-0694	-3902	-755	-4557	-0620	L	2620	6522	816,278	
US-US2	60 - 176	8/7,125	3665	-501	-4166	-7595		-0.598	-3459	- 685	-6146	-0594		0.595	-0.596	817.721	65-15
JS2-WS3	60 - 1%	817.125	-2165	900	246	0.506		-0506	2062	+410	2452	+0503		250	r0504	816.601	
453-154	67 - 115	815.656	+1814	-252	+2066	-0475		+0478	-1711	- 343	+20X	-0475		·Q.475	12476	£15.180	67-11;
56·M55	67 -105	8/4.219	- <i>IG17</i>	-151	-1223	019/		0391	1010	206	- 1216	-0389		Q \$3	0.390	814.609	67 · 10
V55 US8	67 - 1156	815.687	- 721	102	- 823	2,229		-4329	-680	-139	-219	-0,27		0,327	4 325	816.015	68-0
151-151	40-1752	577.281	+ 357	134	• 521	-0232		0232	+ 158	-/23	+ 501	+0223		-0223	+0.228	577.053	48-13
VSI-L52	67 - 11%	815656	- 364	- 51	- 415	-0277		0.277	- 343	- 68	- 411	-0275		0275	-0276	815.932	67-11
ISI USI	48-5%	58/125	- 48	0	- 48	-0.037		-0.037	- 45	0	- 48	-0037		-0.037	-0037	591.162	48-55
152-152	94-4%	1156125	1931	1144	+1075	-059/		16.591	+873	-194	1067	0597		-0587	-0.689	1/55.436	96-37
JS3-NS3	48-1792	577.031	- 56	0	- 56	-000		-0.015	- 56	0	- 56	-0023	_	-000	-2003	577.074	45-17
153/53	48 - 17/4	577.291	·388	138	22	+4232		-0232	+359	163	_	-0224	_			577.053	
154-154	96 - / 5a		- 215	- 27	-242			0/13		- 27		-043				1153144	
J55-W55	48-1/50	577.031	- 57	0		2044		-0044		-0		004				577.075	
V55 U5	49-1/70		_		.533		GG16	×1253		1/43		0.228	1006			574.971	47-10
156-156			•936	-144				*0600		194		+0587		_		1151.394	
52-853	67- 11%		-35/	- 51	- 402			-0269		-68		-0266				815 924	
V35256	67 103		- 350	- 51	-401	025		-0267		-68		-0266				814.405	
	96-94		· 207	-28	- 235			-0,103		28		-0.03	\vdash			1161.353	
(20 430)		1103230			-235	2,03		~200	20/	20	275	CALC		2000	G#05	1001.323	20,24

2 Cambered for dead Load plus one half floorbeam five load reaction. * Length taken as 30°-0' for floorbeam dead and line load. full length taken for upper panel and post dead load.

	CORRECT;	
	APPROVED: Engineer of Dogs	STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS
	Bridge Engineer	SAN FRANCISCO-OAKLAND BAY BRIDGE
	Chief Engineer	SUPERSTRUCTURE-EAST BAY CROSSING
	Director of findic mortes Ownerson	CANTILEVER STRUCTURE
OARD OF		CAMBERED LENGTHS
NSULTING NGINEERS	T	5C,ACE +H 15ET 40 40 20 0 80 120

CONTRACT NO.7.

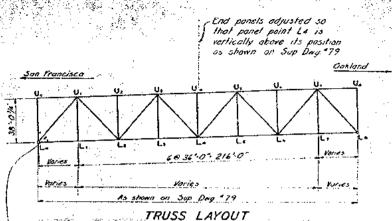
SUP DRAWING NO. 89A. JULY -1934

NORTH TRUSSES

	Si	PAN YB	1-YB2	2		1.		SPA	V YB	2 - 41	93				3	PAN	<i>YB3</i> -	Y84		ىدى <u>ىن ئېلىرىد.</u> ئىرىق			SPA	V YB4	-EI			雪鱼
Member	Stresses	Geometrie Length		3//	ombered Cambered Length Length	Hember :	Stresse	:	Geometric Length		Sty Comber				resses		constric Length Gre	34/65	Combene	Combered	Nember	5tre	5565	Geometric Legato		SL/AE Cambe	red Combere	
L. L.	ead Dive R	ins	Area	107.5	ins It and in		1 12 Live		ino	Arco	ins ins	ft and ins.		Dead	12 Live	Total :	ins Are	to ins.	103.	fl and ins	4 (200)	Dead /2	Live Total	ins.	Prea	125. ms	ft. and it	ins.
4.4.					: '	Tires .110	2 . /90	127	~32.000 J	90.5	.215 452.97 205 431.75	5 35 // %	2.60	+1120	- 194	13/4 43	32000 90	8 208	431.292	. 35 - // 'Xu	L. 12.2	+1140 +	197 - 1337	432.000	900	212 431.7	89 35-11 7	24
65-64	*					Li Li (232 Li Li (232	0 - 395	12715	do	141.6	-275 431.72 -275 431.72												101 +2741 101 +2741		141.8	.278 431.7 .278 431.7		
Lo Lo Lo Lo		-			<u>.</u>	L. L233				141.8	277 431.72					2751	do. 141	6 .284	431.720	35 11 %	40-65	12335 Y	00 2735	do		276 231.7	24 35 11 4	**
L. L.		:		÷	77.03	440 1112	0 - 193	1/3/3	432.000	908	208 431 79	2 35.11%	dill	11140	.197	1337 45	2.000 90	20 .211	431.789	35-11 31	4-47	1110 4	190 -1300	432.000	900	.206 431.7	94 35.11%	×4
U- U.	•		: :			U. U	, - .		453.187	622	- 453 18	7 37-9 %	u. is		+	- 42	3.500 62	721 T 211	463.500	38.7%	U.U.		- 	472.469	122	472.4	69 39 4 %	82
Us Us		-			Sou	UrUs -180	0 -310	-2178	do	116.6	.269 432.26 -268 432.26	9 36 0%	UrUs	-1800	-323	2203	do 1114	4 .272	432272	34.0%	U1. U3	-1890	26 -2216	do.		.272 432 2		
Us Us					.	Us-Us -248	0 -421	-2901	do	1543	.270 432.27 .270 432.27	0 36.034	U4:U5	-2500	-427	2927	do 154	3 .274	432.274	36 0 Be	Usus	2485 -	27 -29/2	do		.271 432.2		
U. U.						U. U 187 U. U 187	0 320	-2120	432.000	114.6	.271 432.27 .271 432.23	1 34-0%	U, U,	-1890 -1890	- 326 - 326	2216 43	do. 114 12.000 114	4 .273	432.273	34 0 %1.	U.U.	-1870 -1870	923 -2193 923 -2193	do 432 000	114.6	.270 432.2 270 432.2	70 36 0%	32
01.04					ves	Urus -			463.562		- 443.54	-			···· ' }				•									- i
L. U. U. L.					: \$	U.L. 1110.	0 - 269 5 • 187	1829	643.428 628.685	103.3 57.6	379 643.80	7 53.7%	Litte	-1500	- 273 • 188 •	1853 65 1268 62	10.732 103 18.485 87	3 389 8 304	651.121	54-3% 52-4%	U.L.	-1503	74 -1857 185 -1277	457.151	103.3	393 457.5 304 428.3		
L. Us Us La				-	. <i>am</i> .	U. 20 - 22				+0.9 37.0	149 42895	4 32.4% 6 52.4%	4:46	- 670	-112	182 268	da 66	0 269	428.954 428.534	52 4 1/2	Urts	- 660 -	(- 72 250	do		.246 6289		
La Us Us Le				· ·	; G "	U. 16 - 22				37.0	149 628.53 145 628.54 266 628.75	0 52-4%	Lette	- 220	- 36	254	do 37	0 145	628.540	52 4 74	Le Us	- 475	38 1 248	do.		151 6205	34 32 4 %	<i>/</i>
L U7. U7-L0						Ur LA - 157	-185	11283 -1844	428 685 630 777	67.8	306 428.57	9 52 4%	4.07	11100	185 .	1285 42	8685 37	8 .306	628.379	52-4 74	4.17	11110 11	88 11298	628.685	87.8	.310 6283	75 52.4 %	a
U.L.		•		:		4-2 6	,	. ;	:	,-	.039 454.78						4.750 35		1	38-0 %						.039 456.21		1
U. L.			i i	· .		U.L. 17.	24				114 454 63			175			do 35 do 35	5 .114	456.434	38.076	44	-175 -	90 - 245		35.5	.063 456.6	36 38-0%	6
Vola			: :	:		15 to 191	- 74	-155		35.5	172 454 62. D67 456.81	300%	115.63	1 191	194	155	do. 35	5 .122	454.628	38-0%	Us'Ls	19/	94 + 285 24 - 155	do.	35.5	122 456.4	28 38 0 %	8
U. Le	terms of			-		U.L 122					.122 456.62			- 171			do. 35 do 35	5 ,122	456.628	38 0 %	Wite	1191 1	94 - 285 24 - 146	da.	35.5	122 456.6	28 35-0%	6
Un Lo						Urls - 175			2.7	35.5	114 456.63	58.078	4741	+ 175	. 20	245 4	do . 35.	5 114	456.636	38-0%	Urla	+175 -	90 1265	do 45 6 . 750	35.5	114 456 6.	36 38-0%	9

SOUTH TRUSSES

SPAN YBI -YB2	SPAN YB2 -YB3	SPAN YB3-YB4	SPAN YB4 -EI
Strasses Geometric St. Combared Cambared Hember Deod Ective Total ins Area ins ins. If and ins.	Number Length Gross LAE Length Length Hends	Stresses Geometric: St./ Combered Combered be Length Grass /AE Length Length Length I Dead 'Is Live Total ins Area ins. Ins. It and ins	Stresses Guardrio SI, Combered Combered Member Length Gross IAE Length Length Dood & Live Total ins. Area ins. ins. It and in
Lo-Li 475 -170 : 845 321/25 63.9 141 320384 26-9 Li-Li 475 -170 : 845 432000 63.9 170 431,810 35-11 % Li-Li 1750 442 2132 do 1204 242 431/38 35-11 %	Let., 1846 1217 1013 401.438 64.8 169 401.729 33-5 45 Let. Litz 1846 1217 1013 432000 64.8 182 431.818 35:1174 Litz 1114 1875 4804 1324 1	. 800 206 1006 379 350 84.8 150 379 700 31 7 15 800 206 1006 432 660 84.8 171 431.829 35 11 %	L-L. 830 -213 1/043 386.183 84.8 159 388.029 32-4 1/2 LrL 830 -213 1/043 432.000 84.0 177 431.823 35-11 92
4-65-1750 442 12192 do 1204 242 151 738 35-1134 4560 11750 1442 12192 do 1204 242 451 738 55-1134	Lita v1875 1486 12361 do 1358 230 431,750 35-11 14 Lita Lita v1860 463 2343 do 1358 248 431,753 35-11 14 Lita Lita v1860 463 2343 do 1358 248 431,752 35-11 14 Lita Lita v180 463 2343 do 1358 248 431,752 35-11 14 Lita Lita v180 263 2134 do 1368 248 431,752 35-11 14 Lita	4 1850 4850 12330 do 135.8 .247 431.753 35.11 14 4 1840 4852 23342 do 135.8 248 431.752 35.11 14	1514 1/850 1463 12313 do. 135.8 251 431.749 35-11 % 1414 1/900 1464 12386 do. 135.8 252 431.748 35-11 %
4.4 - 312.938 62.2 - 312.938 74.0%	Well 401.438 42.2 - 401.438 35-572 Will	379.250 62.2 - 379.250 31.7 W	LTLA : 870 :225 :1075 413.125 84.8 177 412.948 34.4 74 U-U - 368.166 12.2 - 368.166 32.4 78
U+Us -1885 -476 -2361 do. 1285 .264 437.264 56-014	Us Us -1490 - 386 -1876 do 1049 . 253 432.253 36 0 % Us Us Us Us -2000 - 519 -2519 do 1435 253 432.253 36 0 % Us Us	4 -1460 - 377 -1837 do 1069 .247 432247 34-0 4 4 -1980 - 315 -2495 do 1435 .250 432.250 36-0 4	U-U - 1490 - 379 - 1849 432000 104.9 252 432.242 34.0 % U-U - 1490 - 379 - 1849 do 104.9 252 432.252 34.0 % U-U - 2020 - 519 2539 do 143.5 254 432.254 34.0 % U-U - 2020 - 519 - 2539 do 143.5 254 432.254 34.0 %
U-U-1350 -340 -1490 de 925 .259 432.259 34-074 U-U-1350 -340 -1490 432.000 11.5 .259 432.259 34-074 U-U-14 - 321.125 42.2 - 321.125 24-976	Ur Uk -1470 -379 -1849 do 1069 249 432 249 36-0 14 Uk Uk	4 -1470 -380 -1850 do. 1049 .250 432.250 34-0 % 4 -1470 -380 -1850 432.000 1049 .250 432.250 34-0 %	UNU -1520 -386 -1906 do 1069 257 432.257 34-0 14
U. 1. 1 980 - 248 11228 428485 628 193 438392 52 4 % 12 Us - 594 - 148 - 738 do 409 254 428939 52 4 %	U.Lz + 960 + 264 + 1184 + 628488 + 87.8 - 282 + 628409 + 52-4% + U.Lz - Ls-Ur + 348 + 146 - 704 + do + 609 + 243 + 288928 + 52-4% + Ls-Us	4 + 750 - 247 +1177 628485 87.8	
2 · U · 200 · 50 · 250 · 60 370 141 428.544 52 4 % - U · L · 590 - 148 - 738 · de 409 254 428.939 52 4 %	L. U. 4 200 + 57 + 252 40 310 142 628543 52-4 1/4 L. U. U. 4 575 -151 - 726 40 605 250 628935 52-4 1/2 U. L.	- 560 -147 -707 do 60.9 244 628.929 52.4 %	14-U1 + 178 + 47 + 225 do. 37.0 .127 428.558 52-4 1/4
Wris -1180 - 292 - 1414 518338 929 299 538230 44-439 L4-10 - 54 - 24 - 80 454873 355 .034 454857 38-0%	11.14 -1770 -324 -1594 593 714 93.9 336 596 652 49.4 49. 49.4 464 74 - 24 - 98 456,750 355 042 486 792 38.0 48.4	- 1280 - 525 - 1405 599.445 93.9 .541 599.604 47-11% 74 - 24 - 78 434.756 .55.5 .642 154.792 36-0 %:	41.40 -1298 -335 -1635 613.666 93.9 356 616.224 51-4 80 444 - 74 - 24 - 98 456.750 35.5 042 456.792 38-0 151
U+L-114 24 -140 do 35.5 040 434.810 38.0% U+L-134 - 98 1232 do 35.5 00 454.50 38.0% U+L-122 - 24 -144 do 35.5 04.3 454.813 38.0%	L. L. + 152 100 1252 do 35.5 108 434442 38-015 U.L. U.L. + 124 24 148 do 355 063 454813 38-015 Url. Url. + 155 - 94 1249 do 355 107 46443 38-076 Url. Url. + 155 - 94 - 151 do 355 005 434615 38-076 Url. Url 127 24 - 151 do 355 065 434615 38-076 Url.	2 - 124 - 24 - 148 do. 35.5 064 456.914 36.074 4 - 127 - 24 - 121 do. 35.5 107 456.43 38.076 4 - 127 - 24 - 151 do. 35.5 065 454.615 38.076	Usls - 154 - 24 - 148 40 35.5 064 454814 30 0 % Usls + 153 - 94 - 249 do 35.5 107 456 643 38 0 %
U11. 114 24 -140 do 355 OLD 456810 38 0% U11. 119 -98 -217 do 355 093 456457 38 0%	U(4) -153 · 94 · 289 do 35.5 · 107 456443 38-0%; U(4) U(4) · 124 · 24 - 148 do 35.5 · 063 456813 38-0%; U(4) U(4) · 152 · 100 · 1252 do 35.5 · 108 456442 38-0%; U(4) U(4) - 74 · 14 · 98 434750 35.5 · 042 454792 38-0%; U(4)	- 124 - 24 - 148 do. 355 .014 45L814 38.0% 7 - 152 - 100 - 252 do. 35.5 .108 454.442 38.0 %	Usts +153 + 26 + 249 do 355 107 456.443 38 0 %; Usts +124 - 24 - 148 do 35.5 064 456.84 38 0 %;



90° ercept in spon YBI-YB2 where Ualo

is vertical

Note: In spon YB3-YB4 vertical curve to be laken up in Thor system

NOTES

Live Load: 1/2 Live = 2000 lb per ft. along South Truss and 1500 lb per ft.
along North Truss, except for verticals where the Live Load
is 1/2 the Noorbeam reaction

- E: Value of E taken as 30,000,000 fm' for all members + Tension
- Compression

Combered Length- The combered length as given in feet and inches to be used for fabrication

2.5	CORRECT
· ·	Cognical of Proper
	APPROVED:
•	Bridge Lagran
	Chief Comme
	D. WAT JAME HALL
	Characa
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DEPARTMENT OF PUBLIC WORKS

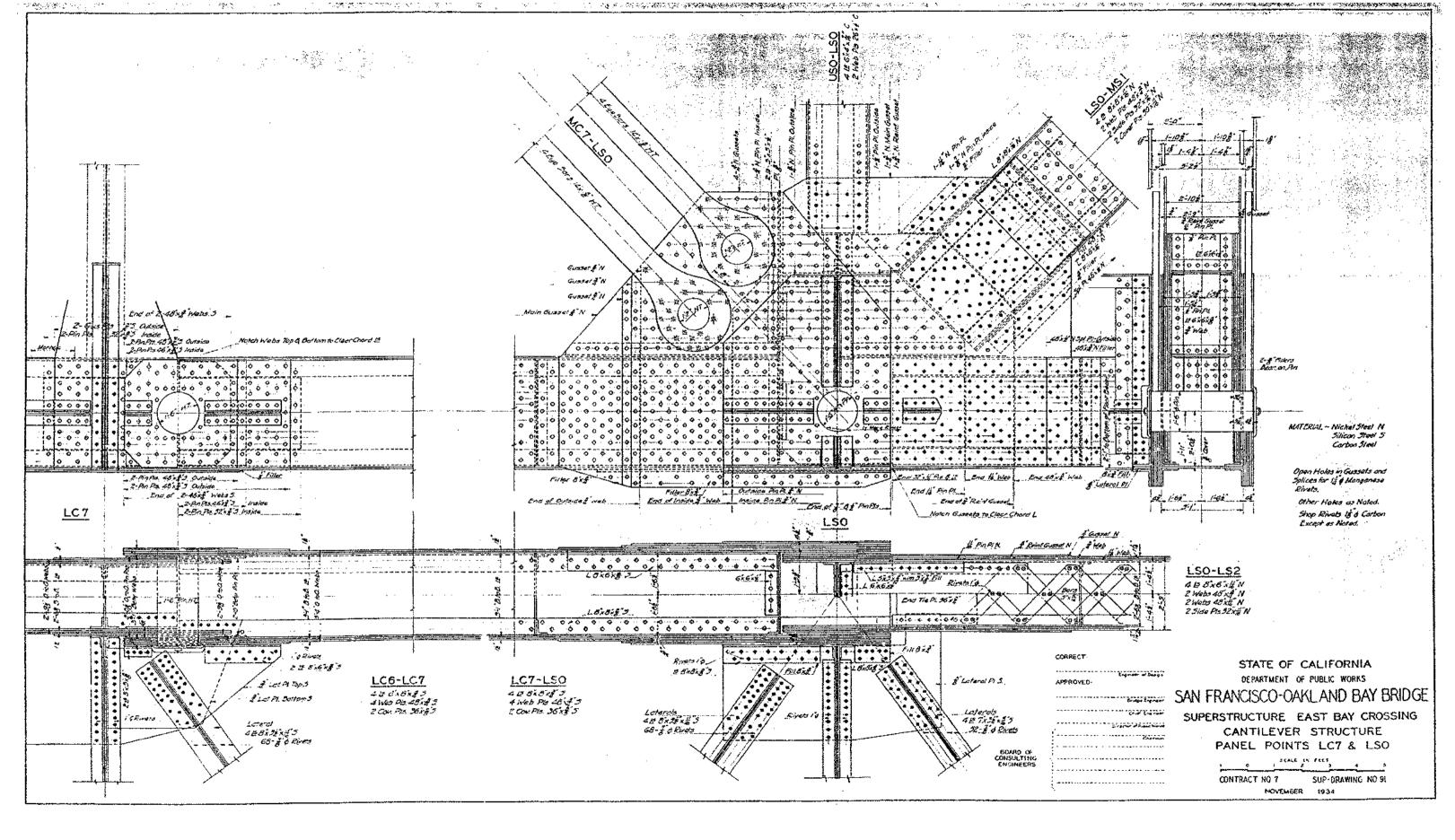
SAN FRANCISCO-OAKLAND BAY BRIDGE

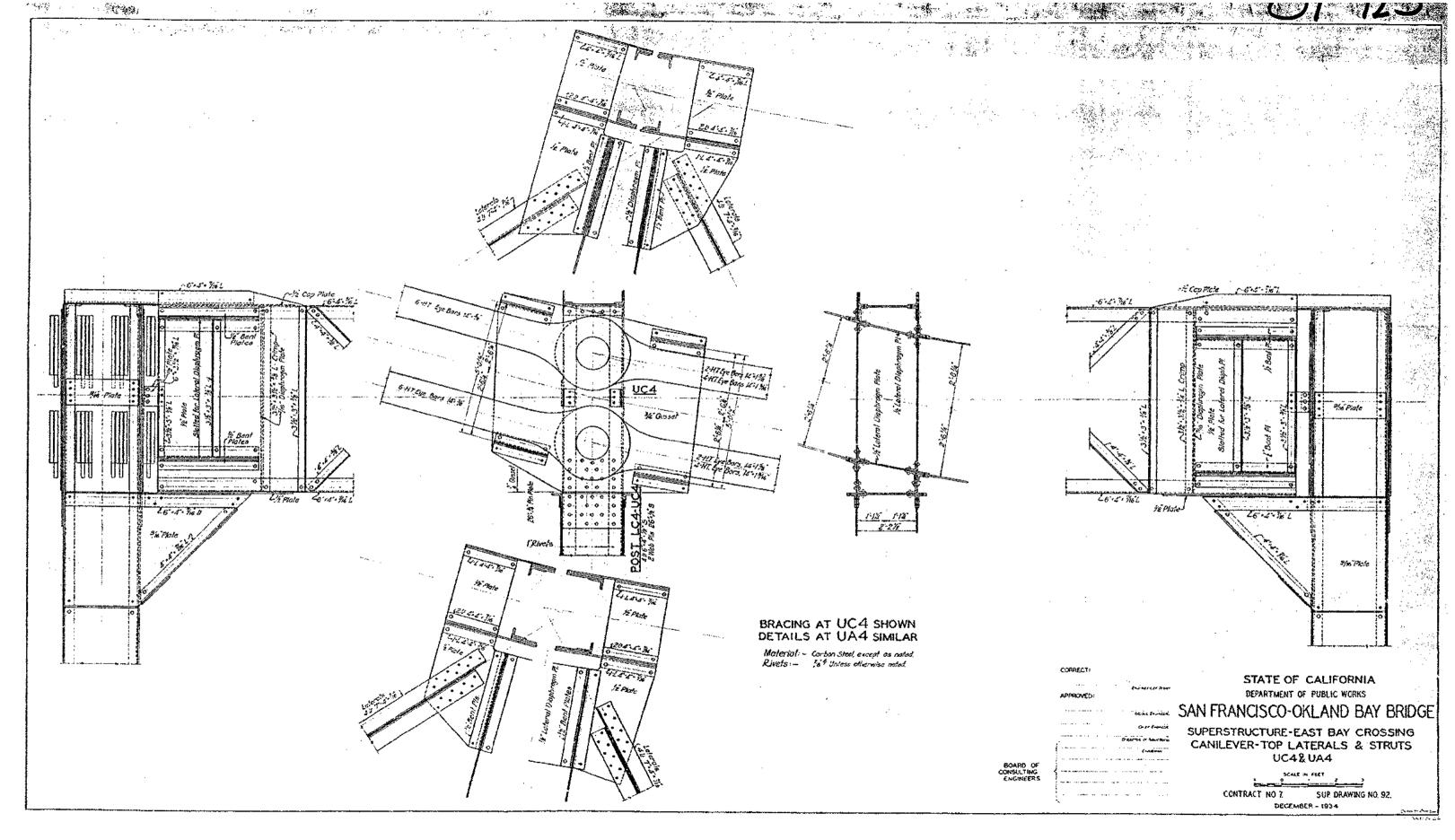
SUPERSTRUCTURE-EAST BAY CROSSING 288 FT. SPANS-YB I TO E1 CAMBERED LENGTHS

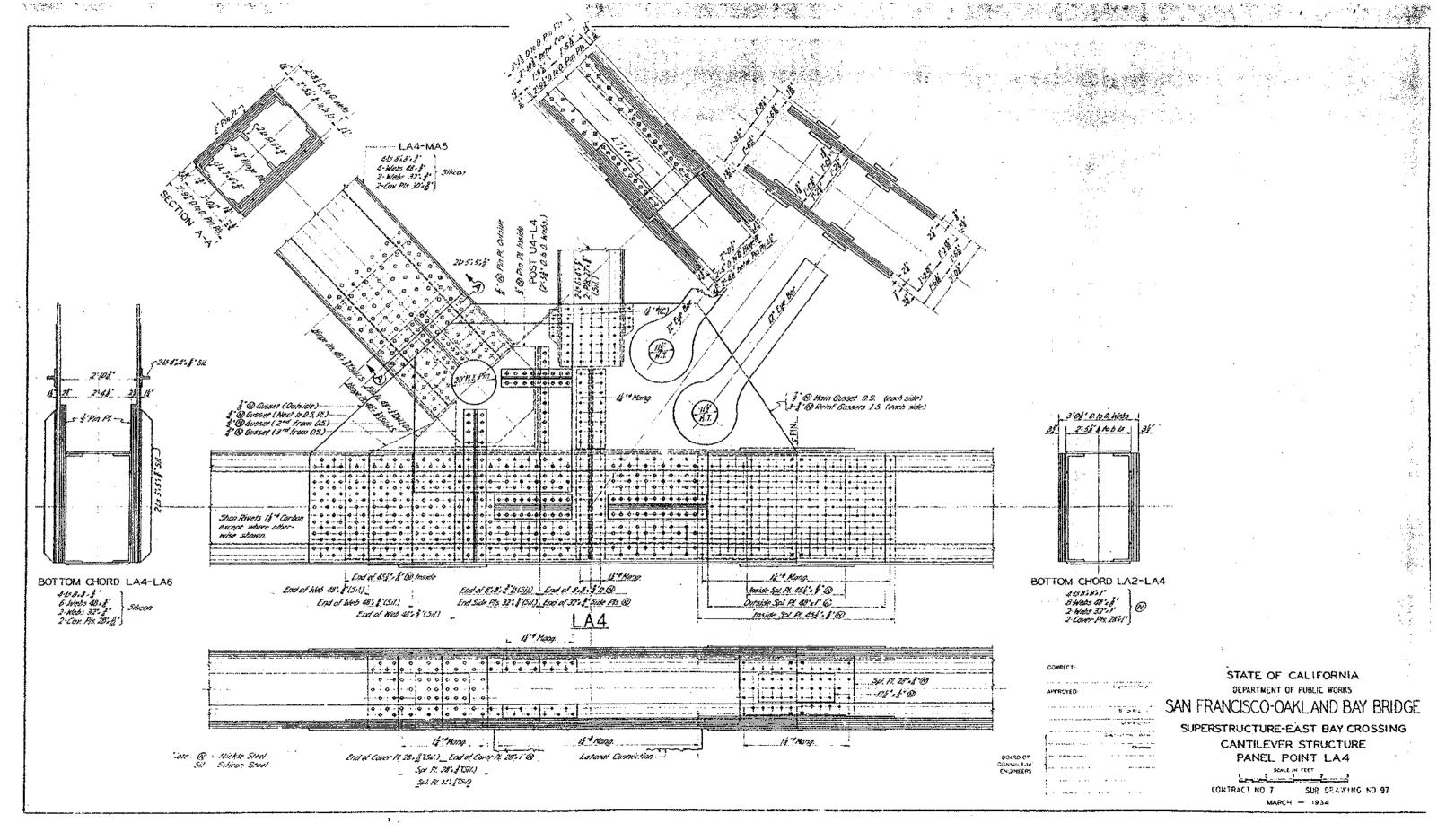
CONTRACT NO.7

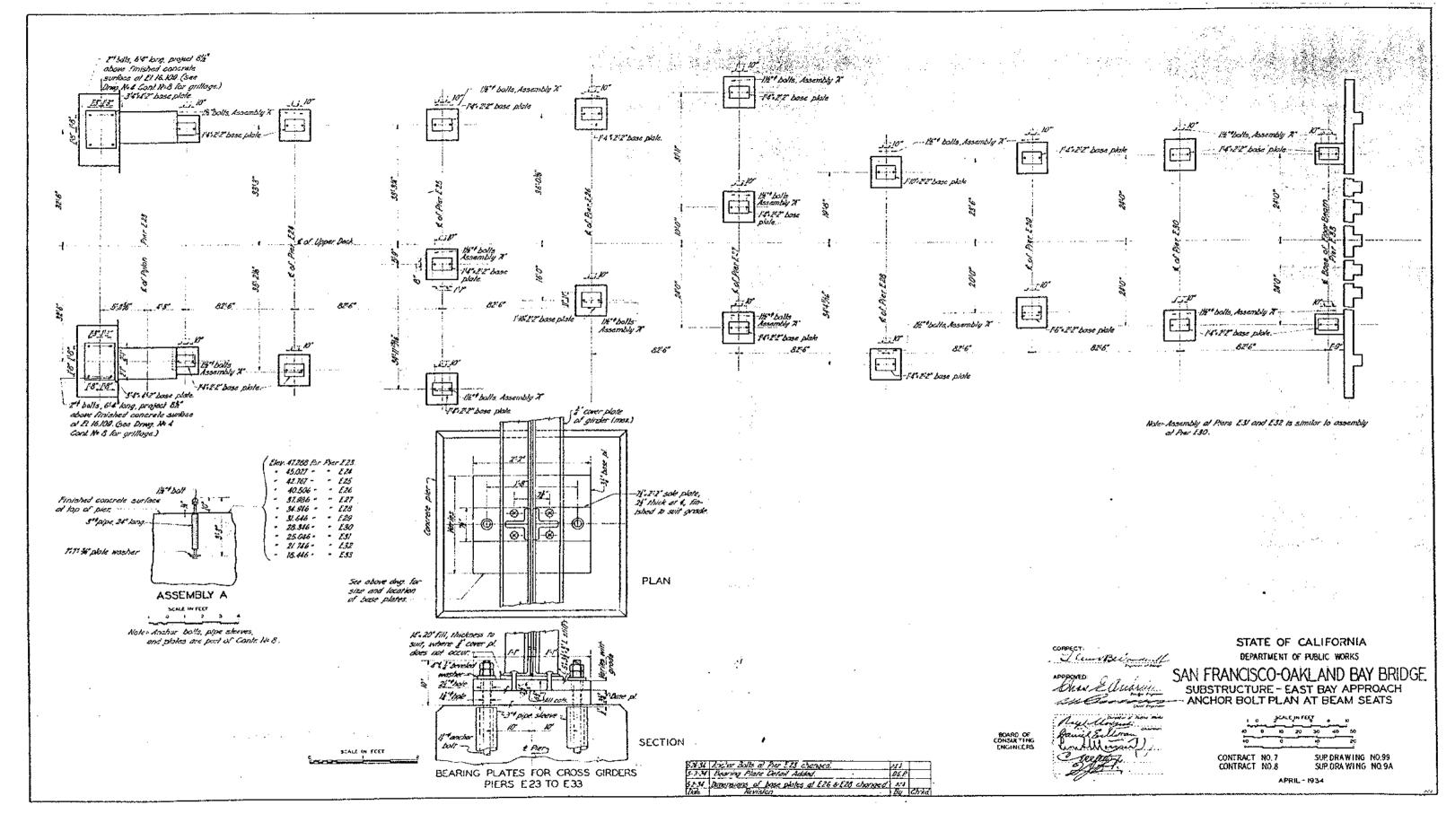
SUP DRAWING NO. 90

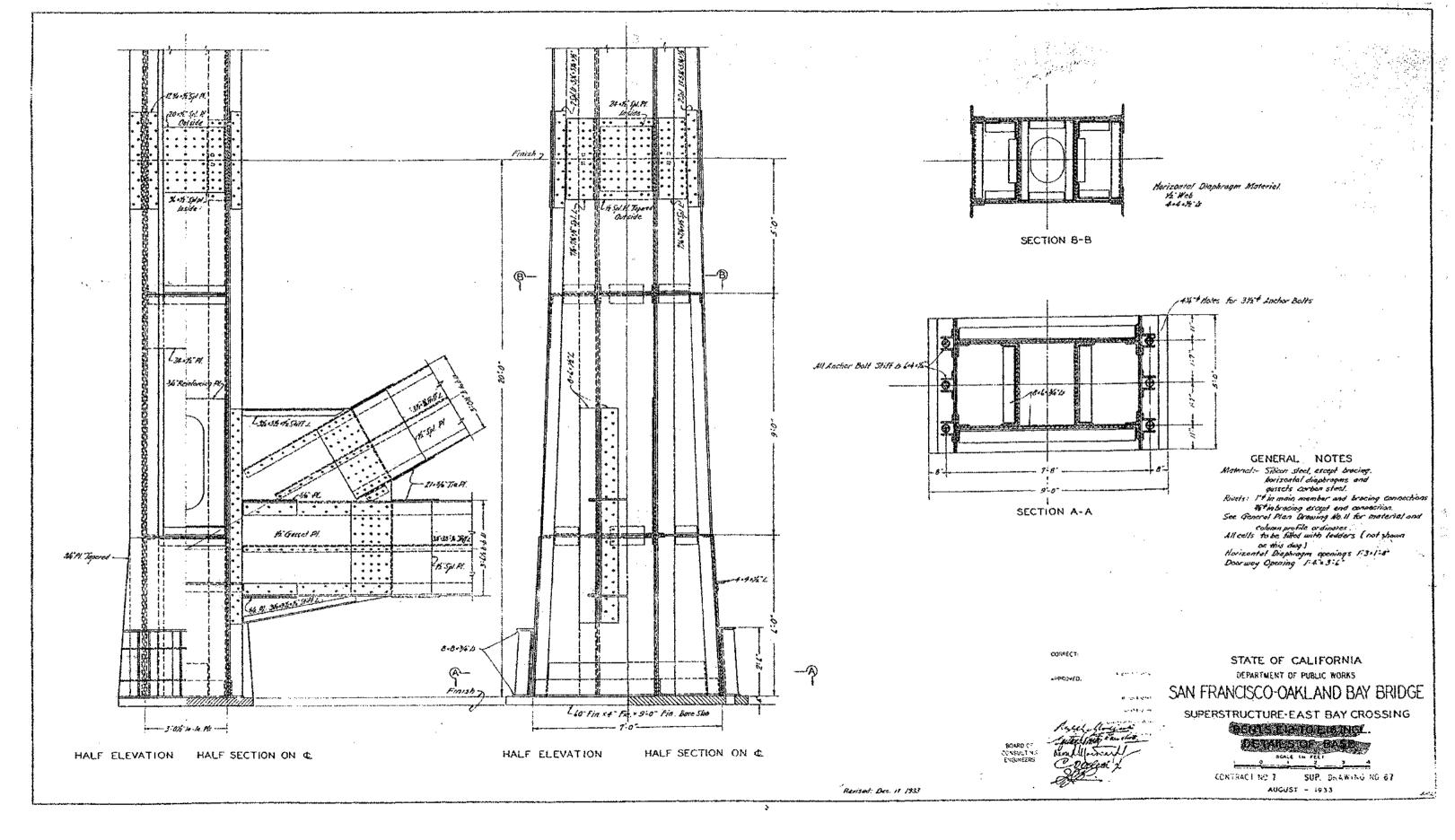
FEBRUARY - 1934

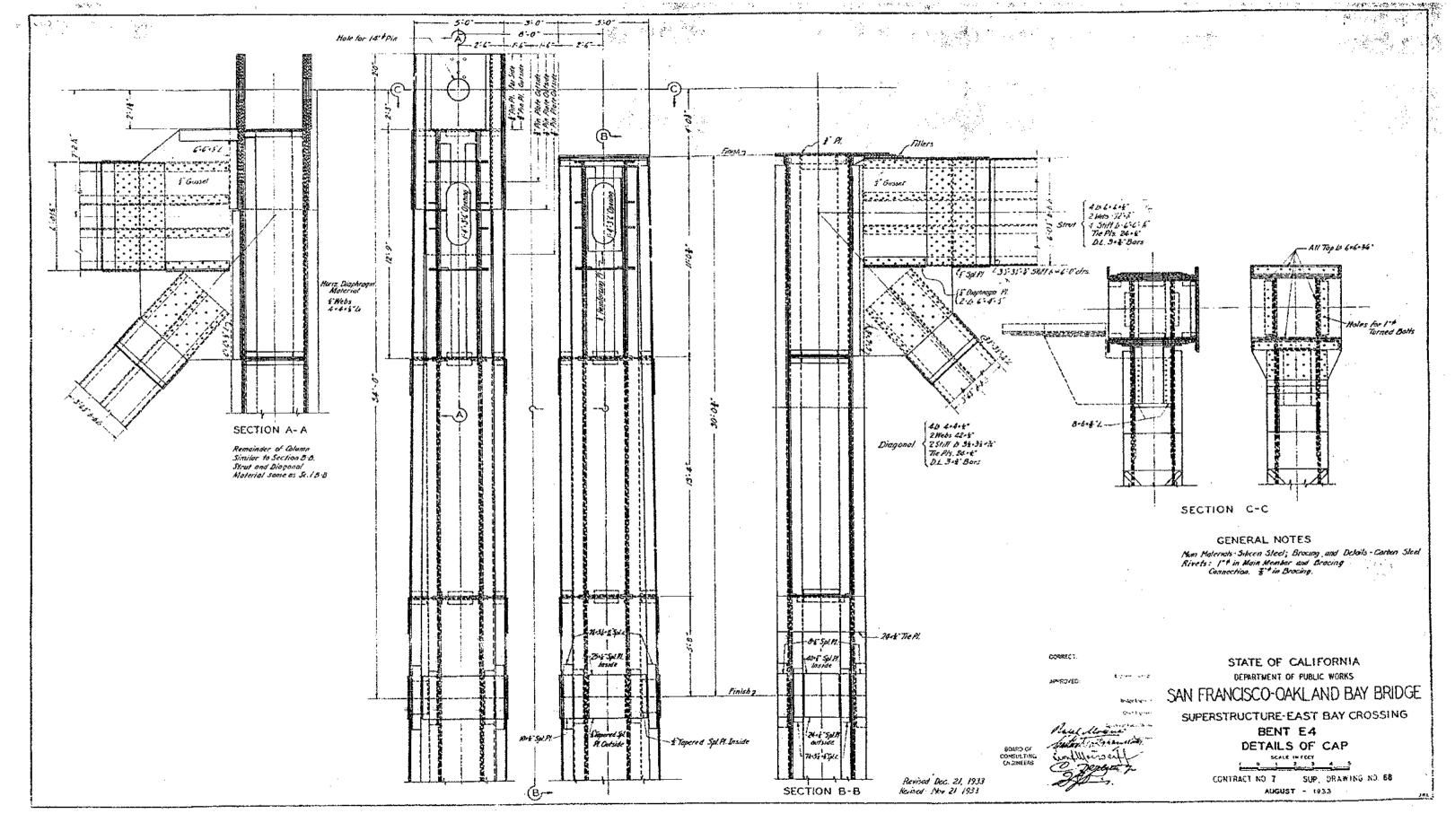


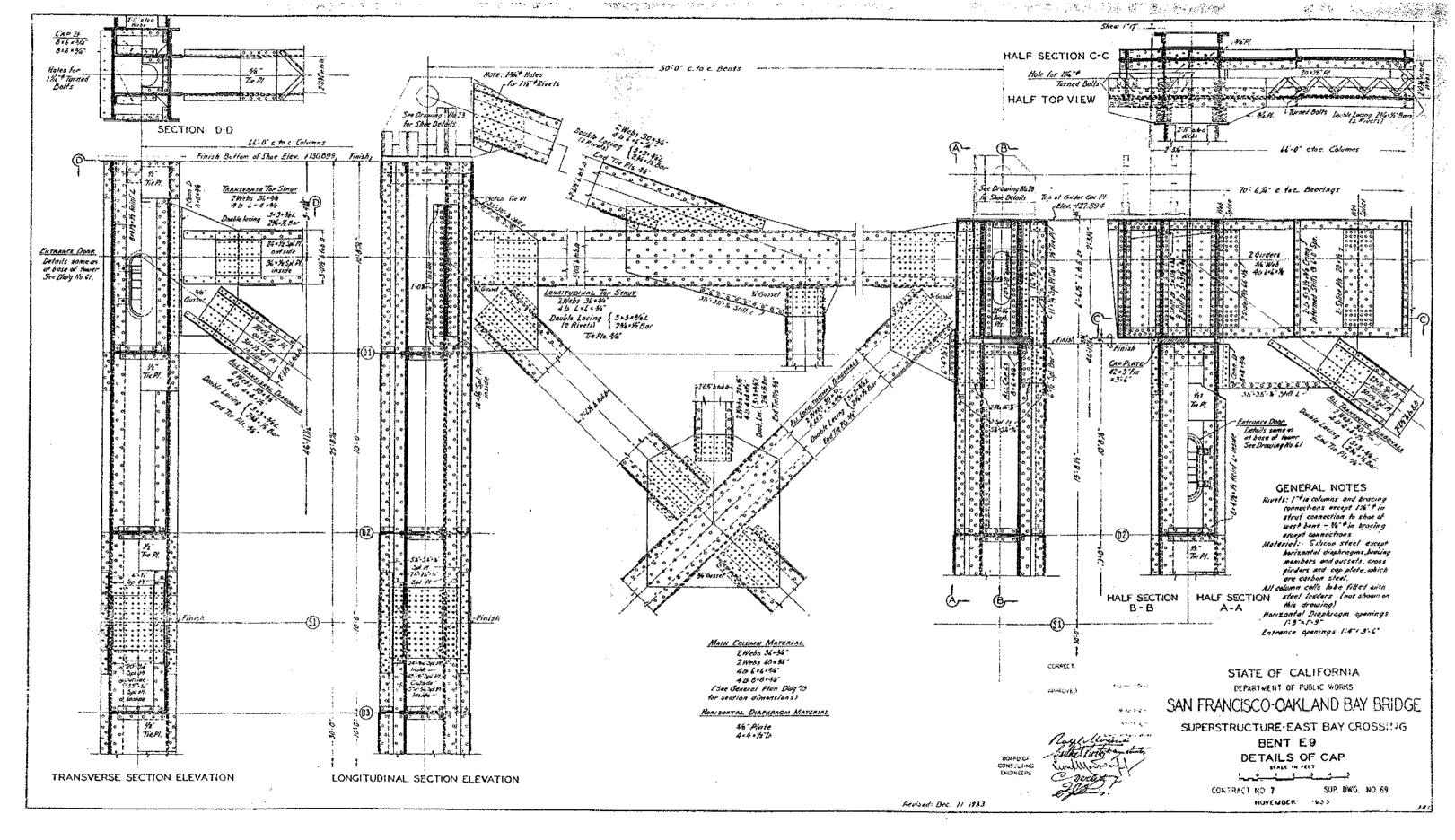


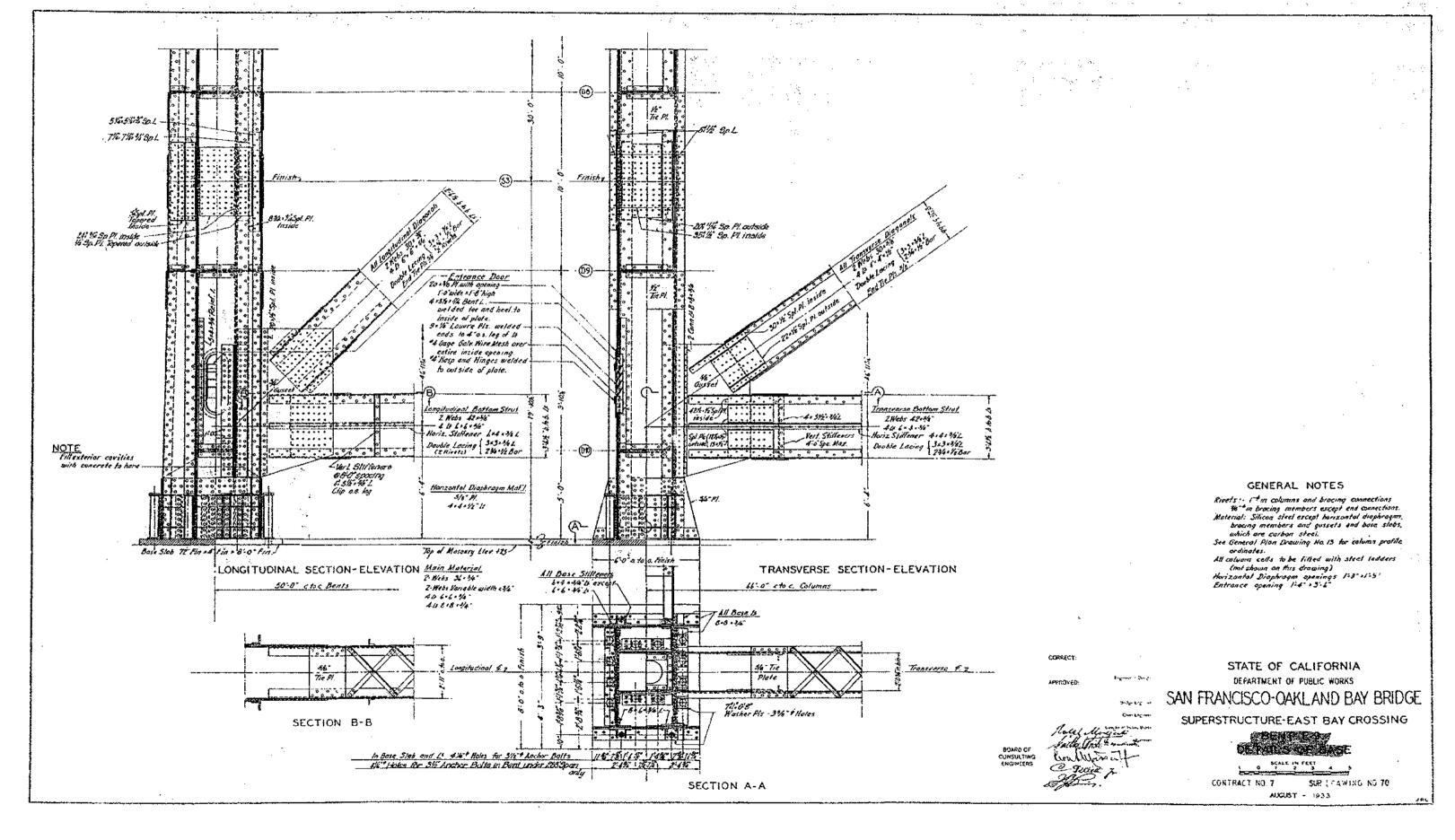


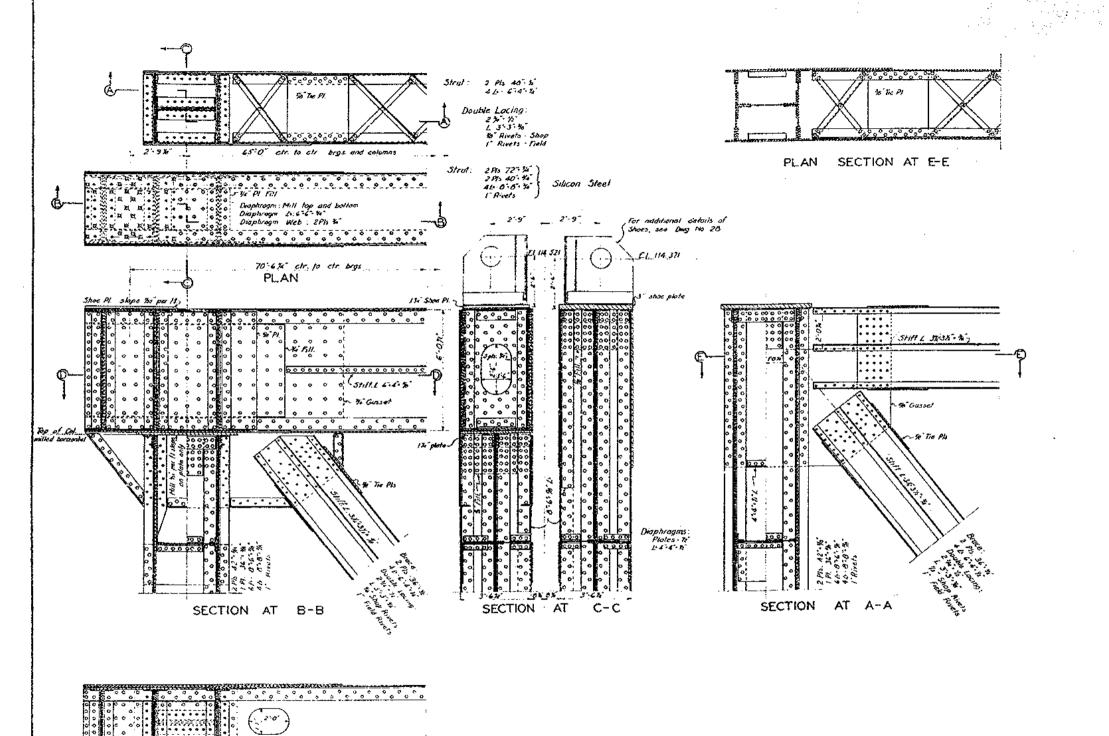












PLAN SECTION AT D-D

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SAN FRANCISCO-OAKLAND BAY BRIDGE SUPERSTRUCTURE-EAST BAY CROSSING

STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS

CAP DETAILS FOR BENT E- II

CONTRACT NO 7

OCTOBER - 1933

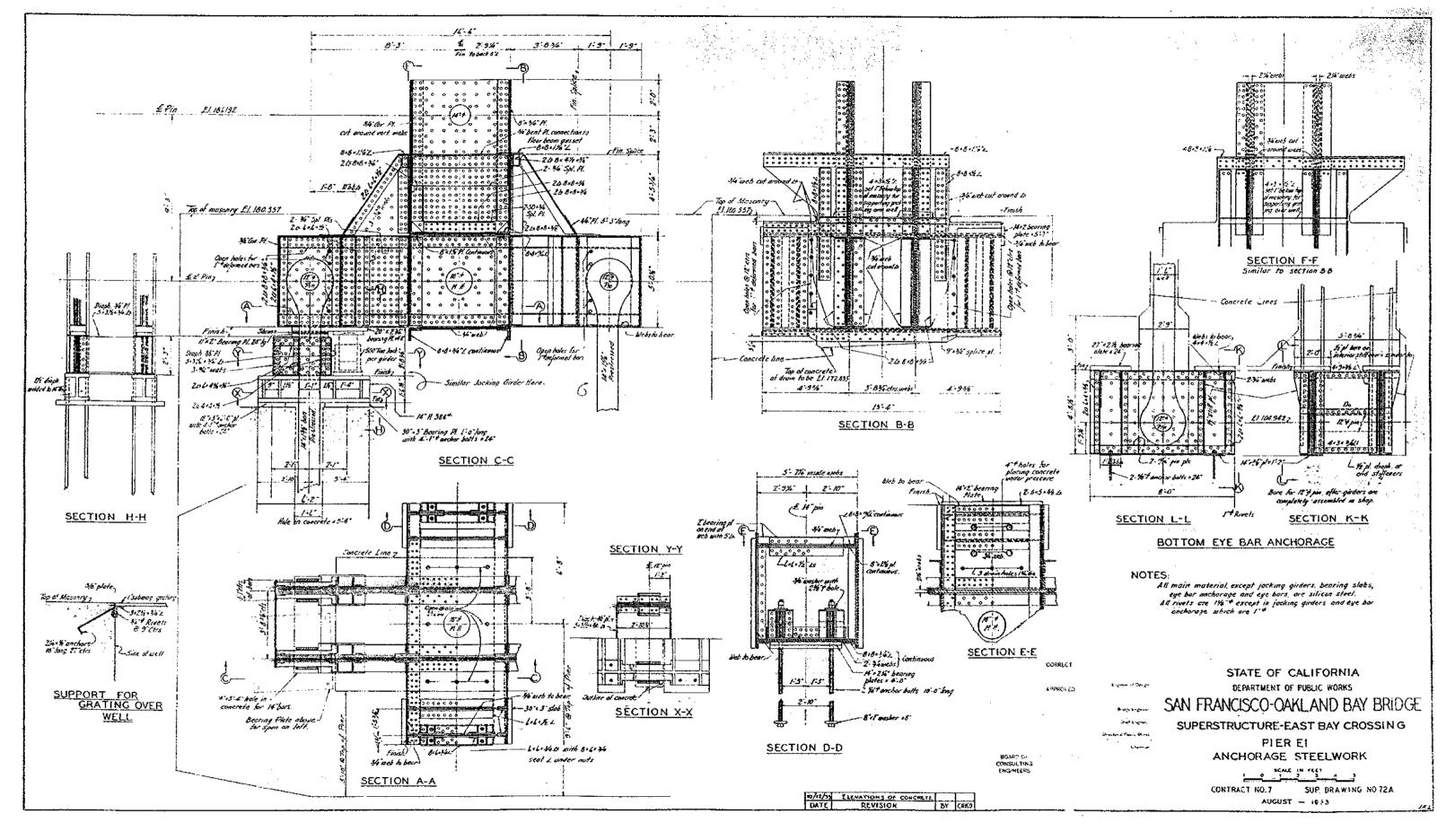
Revised Dec 11 1933

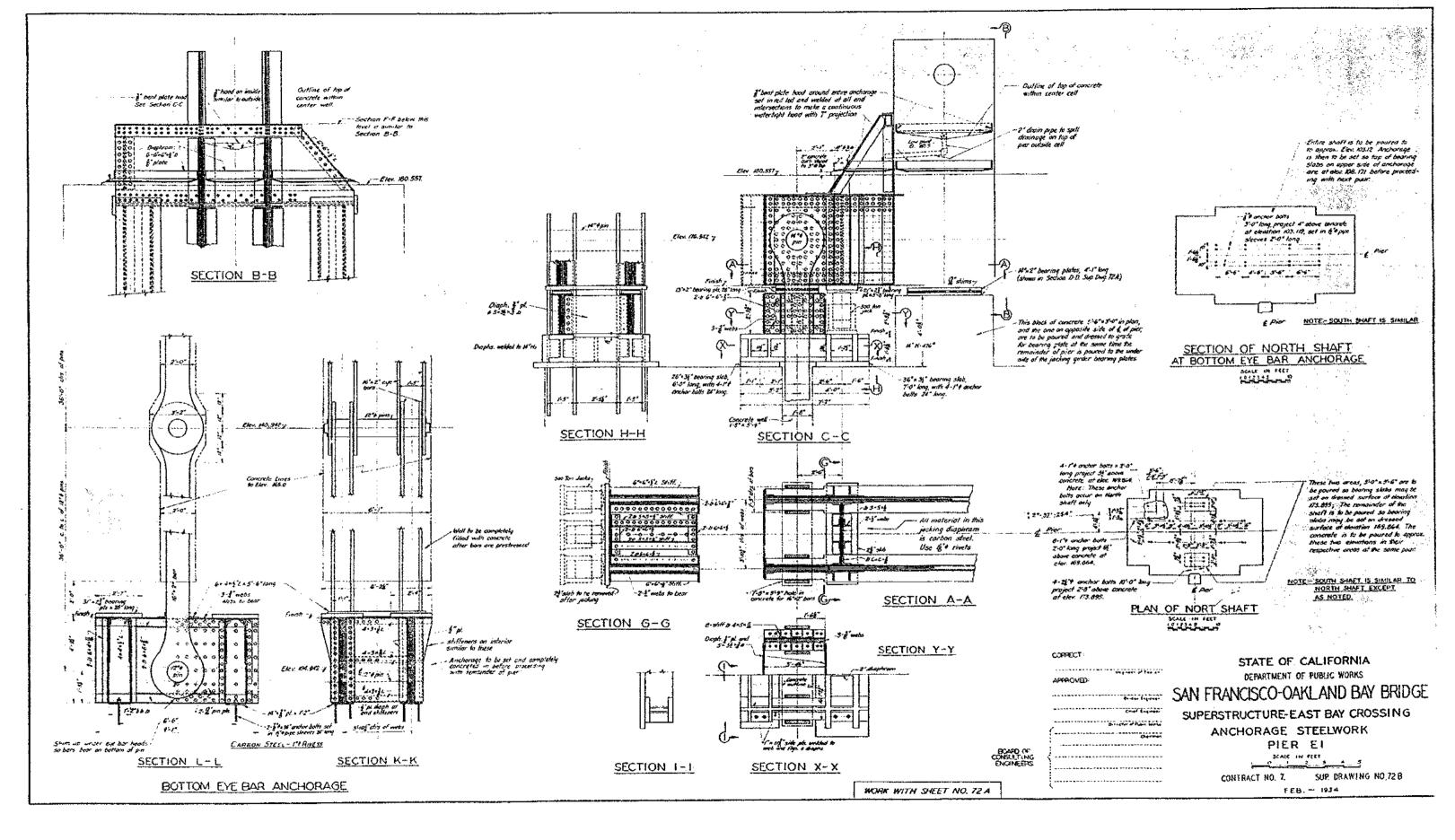
For General Drawing, see Sup. Dwg. No. 8

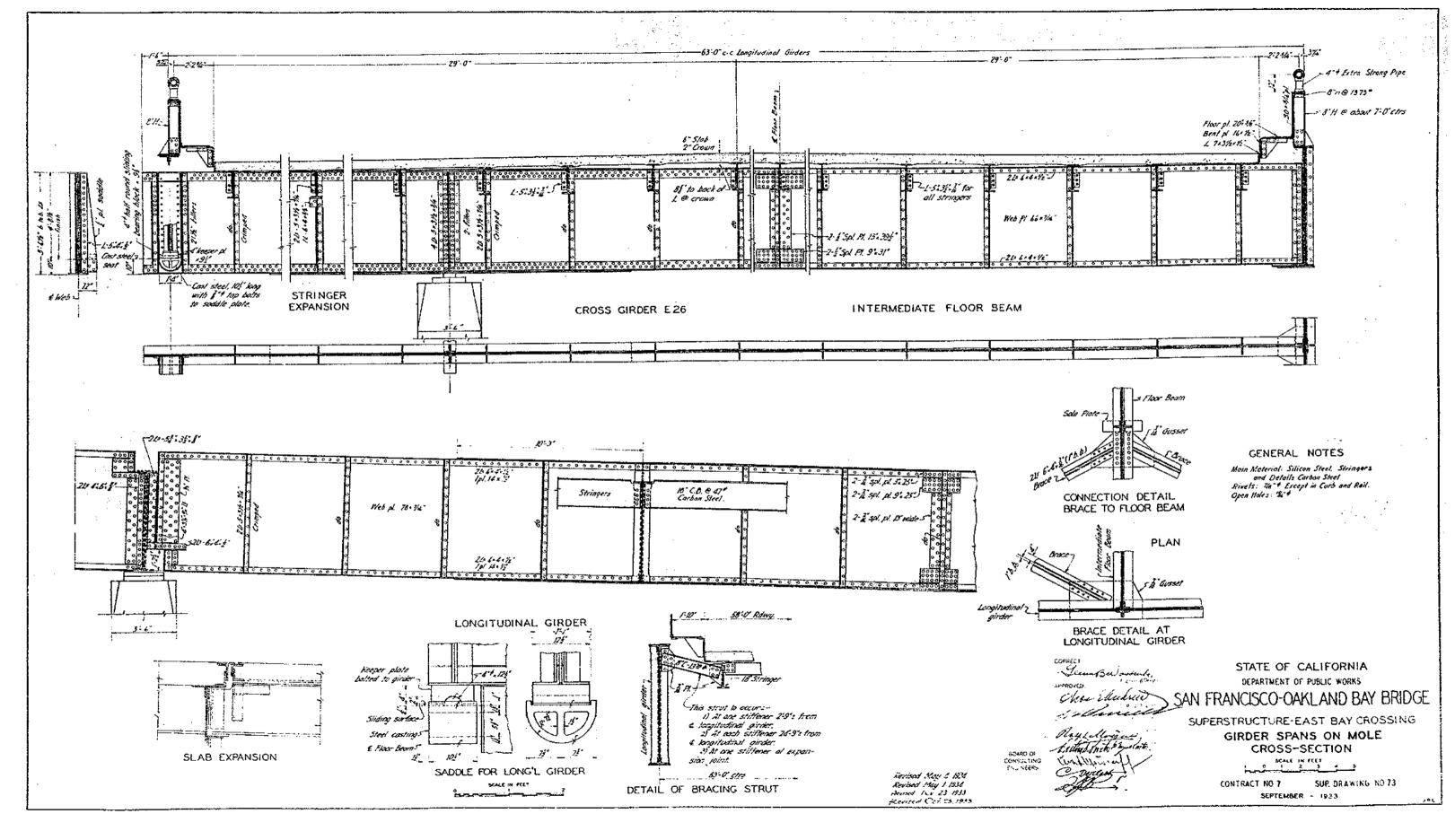
NOTES Moin Column material, Silicon Steel

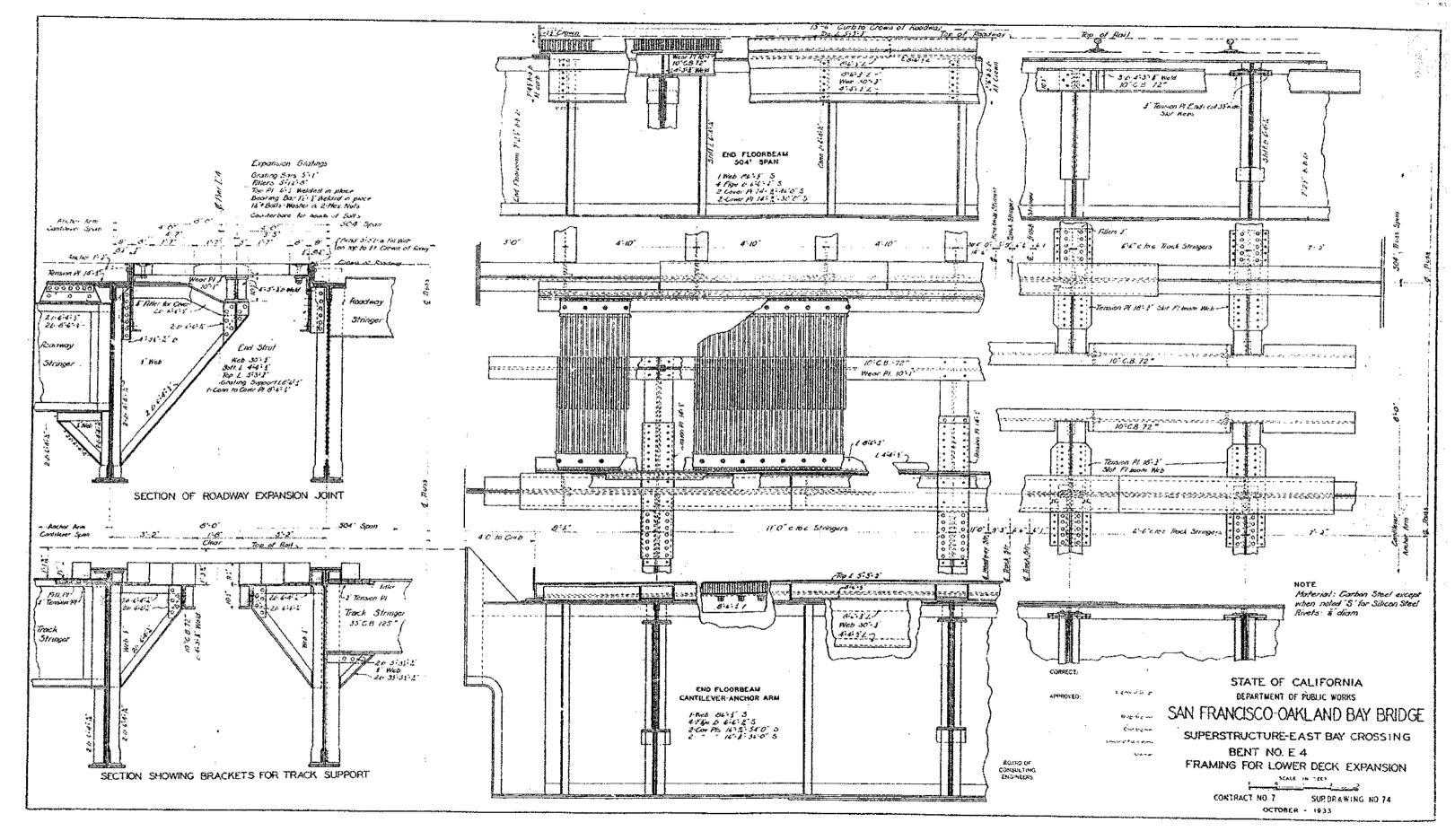
Gussets, struts, and broking, Carbon Steel. Te 1 15

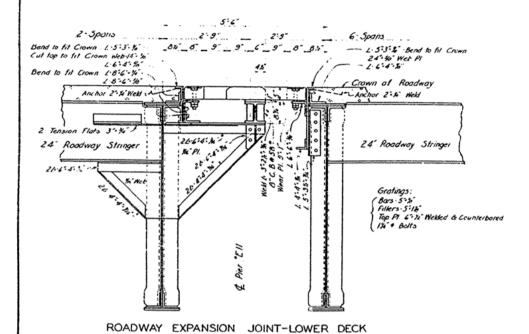
SUPDRAWING NO 71



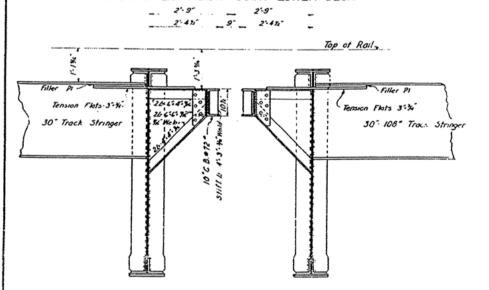




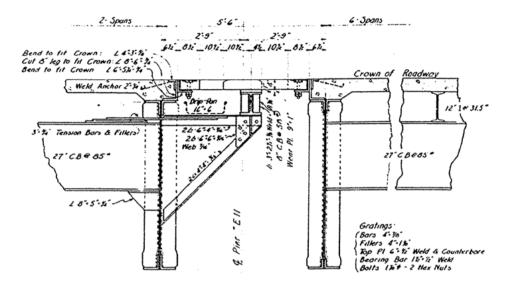




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The Comment

ROADWAY EXPANSION-UPPER DECK

CORRECT:

transcription

and the late that the

Charles me

BOARD OF

STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS

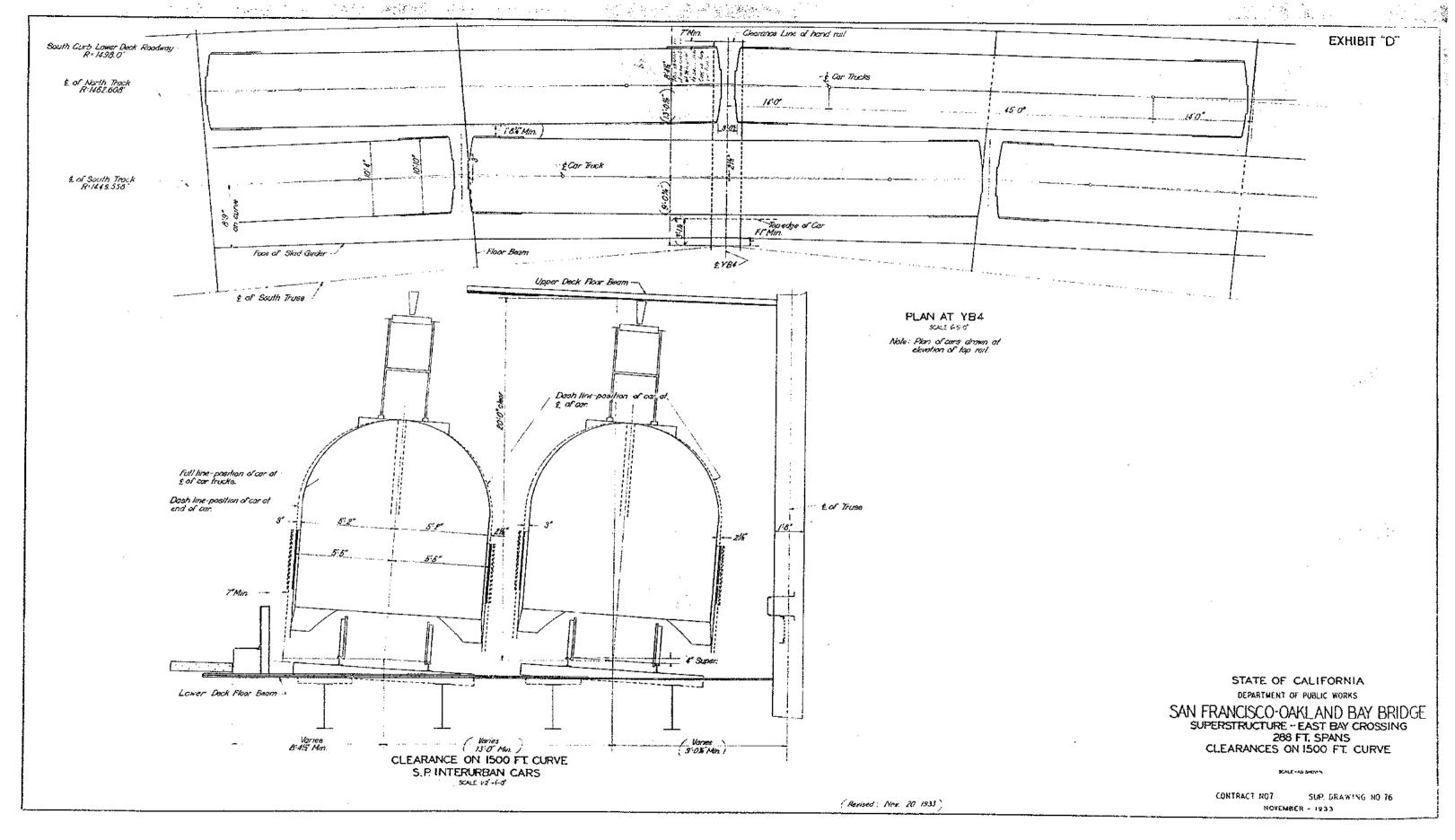
SAN FRANCISCO-OAKLAND BAY BRIDGE

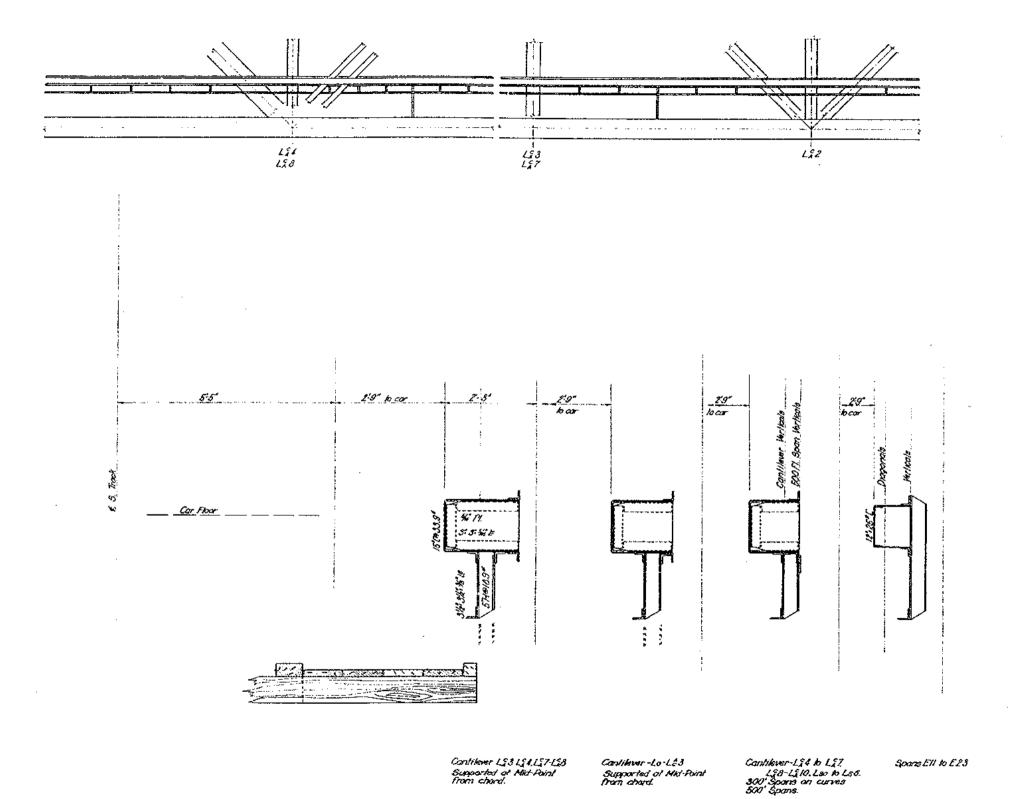
SUPERSTRUCTURE-EAST BAY CROSSING

EXPANSION AT BENT EII FRAMING FOR UPPER & LOWER DECKS

CONTRACT NO 7 SUP DRAWING NO 75

HOVEMBER - 1933





CONRECT

APPROVED

19、1数1.10分子20分支数

Charlenger

SAN FRANCISCO-OAKLAND BAY BRIDGE SUPERSTRUCTURE - EAST BAY CROSSING TYPICAL RAILING SECTIONS

STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS

BOARD OF CONSULTING ENGINEERS

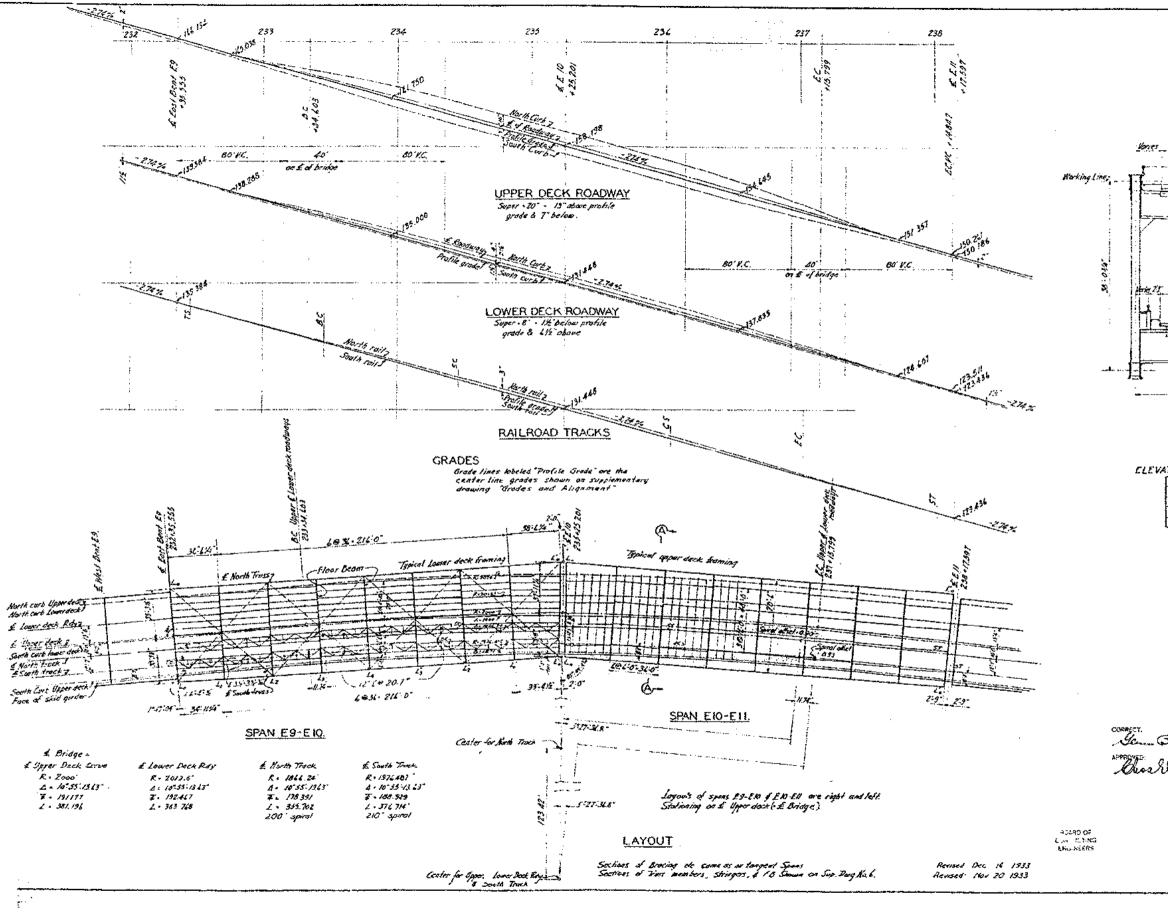
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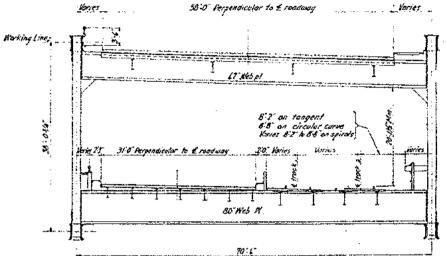
CONTRACT NO7

SUPURAWING NO 77

A Section of the second

SEPTEMBER - 1933





SECTION A-A

ELEVATION OF & OF LOWER CHORD AT & OF PIN

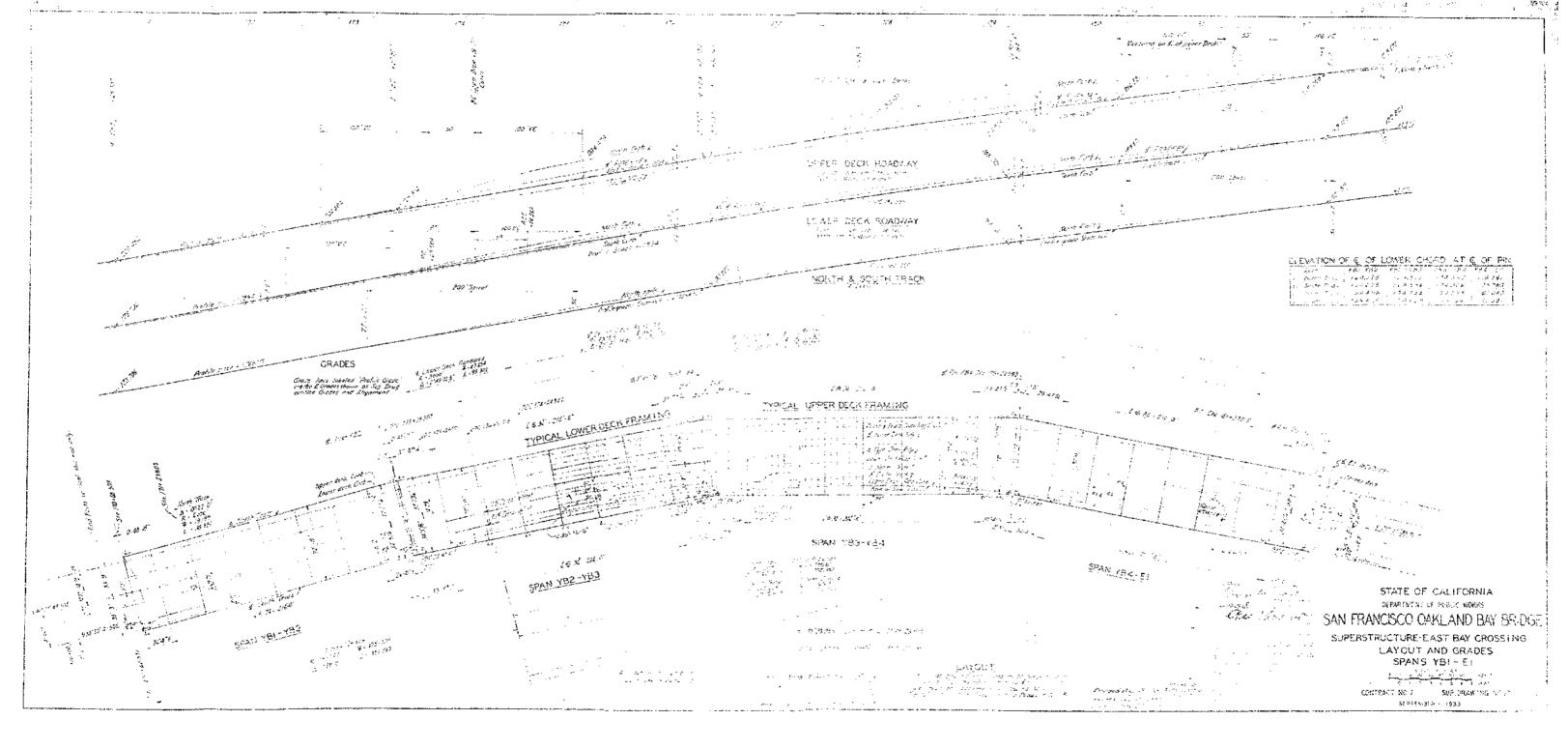
-	Span	C9 - E10	£10-£11
1	La North Truss	/30,373	122.438
1	La South Trusa	130.330	122.296
1	Le North Truss	122.340	114.446
	L. South Truss	122.510	114.409

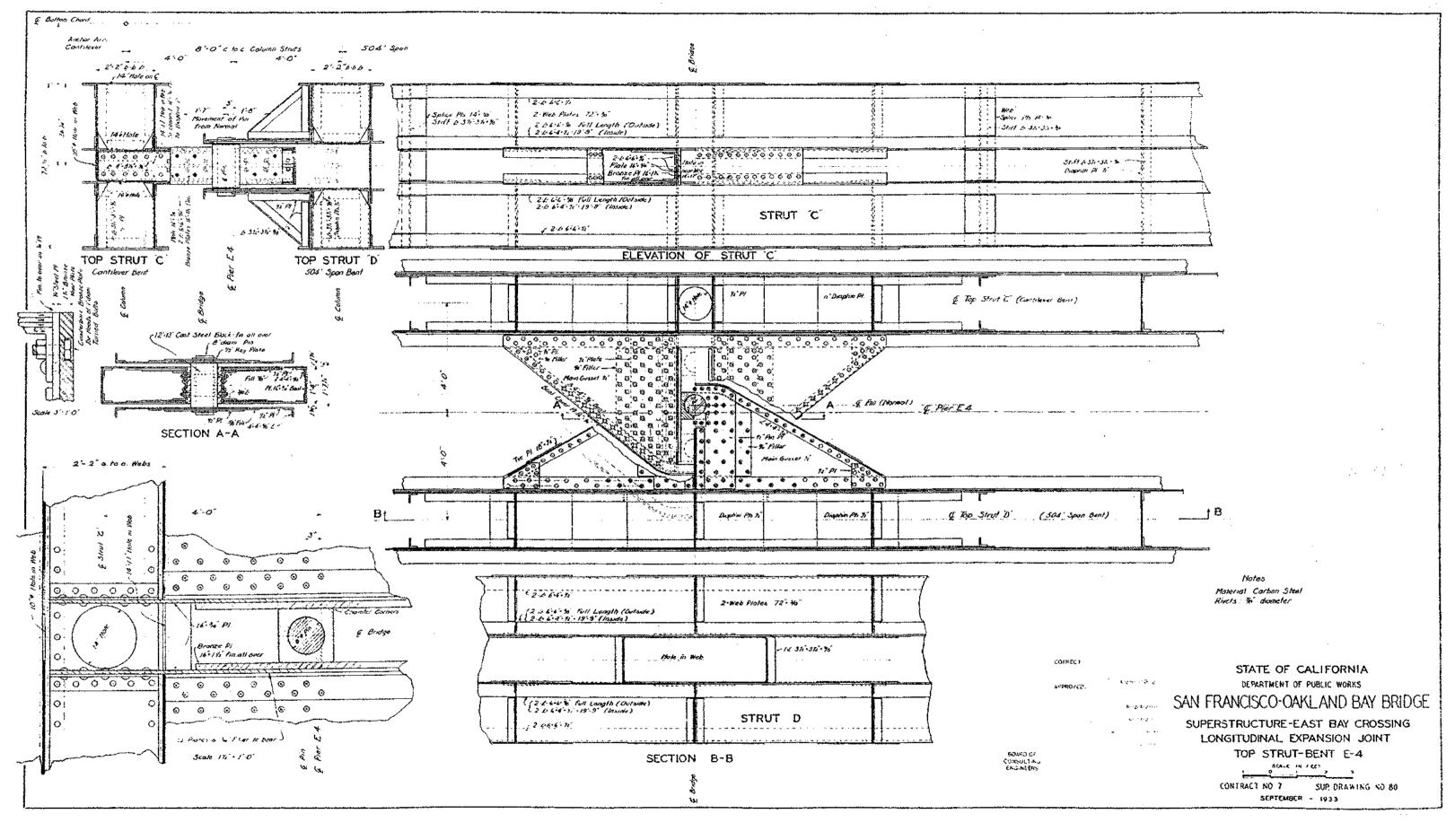
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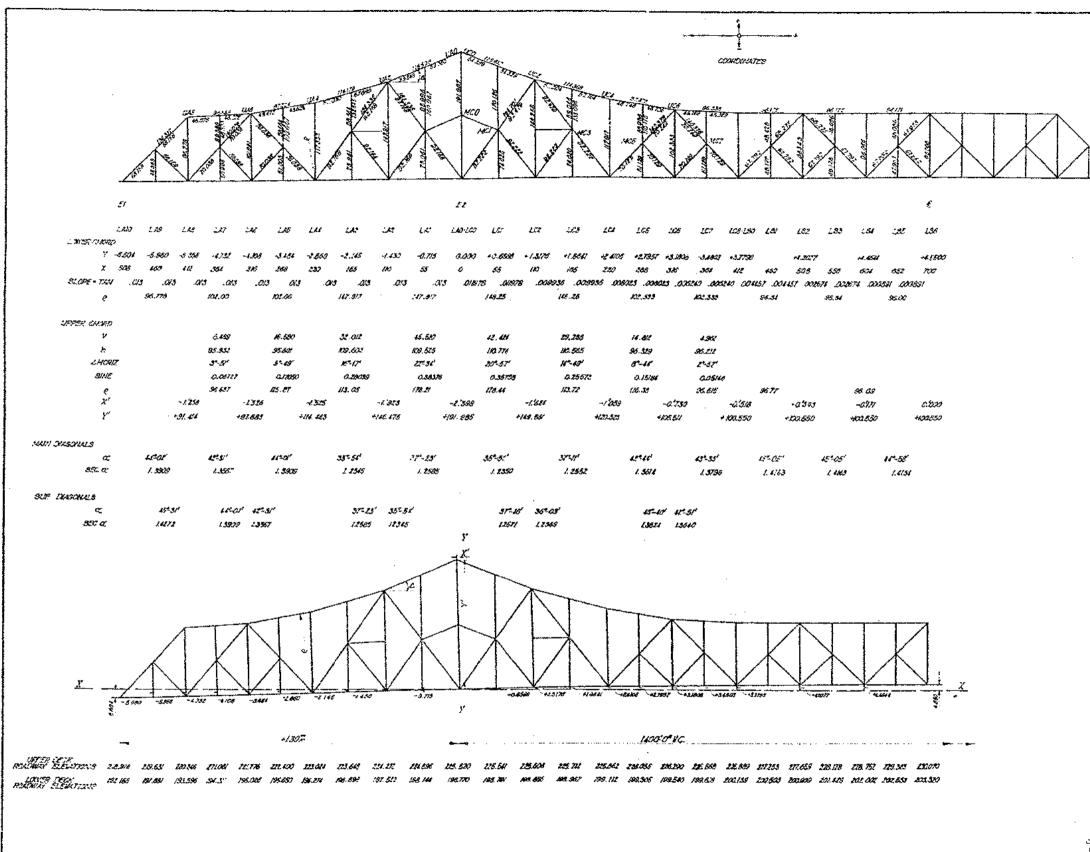
STATE OF CALIFORNIA DEPARTMENT OF PUBLIC WORKS SAN FRANCISCO-OAKLAND BAY BRIDGE SUPERSTRUCTURE-EAST BAY CROSSING LAYOUT AND GRADES SPANS E9-EIO & EIO-EII.

CONTRACT NO T SUP, DRAWING NO.78

SEPTEMBER-1933







Continuies given are for geometric centers. Dead load plus uniform line load of 2020 pounds per foot of trues.

This loading for earth trues. Make north trues line some.

53

CORRECT

APPROVED

territory design

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SAN FRANCISCO-OAKLAND BAY BRIDGE SUPERSTRUCTURE ~ EAST BAY CROSSING GEOMETRIC CENTERS

CANTILEVER SPAN

CONTRACT NO 7

SUP CRAWING NO.81

OCTOHER - 1933

